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NASA CONTRACTOR  
REPORT



NASA CR-132732-2

(NASA-CR-132732-2) ADDITION OF FLEXIBLE  
BODY OPTION TO THE TOLA COMPUTER PROGRAM.

N85-27856

PART 2: USER AND PROGRAMMER DOCUMENTATION

(NASA) 205 p HC A10/EF A01

CSCL 01C

Unclas

G3/05 21527

# ADDITION OF FLEXIBLE BODY OPTION TO THE TOLA COMPUTER PROGRAM

## Part II - User and Programmer Documentation

By *I. W. Dick and B. I. Benda* FOR FAI



*APRIL - 1985*

Date for general release:

Pre  
MCD

St. Louis, Missouri 63166 (314) 222-0792

for Langley Research Center



**NASA CR-132732 -2**

**ADDITION OF  
FLEXIBLE BODY OPTION  
TO THE  
TOLA COMPUTER PROGRAM**

**Part II - User and Programmer Documentation**

*By J. W. Dick and B. J. Benda*

Prepared Under Contract NAS 1-13259

*by*

**MCDONNELL DOUGLAS ASTRONAUTICS COMPANY — EAST**

St. Louis, Missouri

*for*

**NATIONAL AERONAUTICS AND SPACE ADMINISTRATION**

# ABSTRACT

User and programmer oriented documentation for the flexible body option of the Takeoff and Landing Analysis (TOLA) computer program are provided in this report. The user information provides sufficient knowledge of the development and use of the option to enable the engineering user to successfully operate the modified program and understand the results. The programmer's information describes the option structure and logic enabling a programmer to make major revisions to this part of the TOLA computer program.

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## 1. INTRODUCTION

The purpose of this report is to summarize the flexible body option of the airplane Takeoff and Landing Analysis (TOLA) computer program and explain how to use this option in conjunction with the overall program. The flexible body option was developed by McDonnell Douglas Astronautics Company-East under NASA Contract NAS1-13259 for investigation of aircraft response in a ground operating environment.

The original TOLA computer program developed by Air Force Flight Dynamics Laboratory personnel provides a complete simulation of the takeoff and landing of a rigid airplane. The flexible body option provides the additional capability of predicting the total motion of specified points on the aircraft including elastic airframe effects.

It should be emphasized that the flexible body option is but a part of the overall TOLA computer program. Successful operation of the program depends on proper input of all required data and interpretation of the resulting output. Much of these data are associated with the existing rigid body version of TOLA. It is not the purpose of this document to define these data, for this is done in Reference 1. The user should not attempt to execute the TOLA computer program without first becoming familiar with the information contained in this reference.

Programming information on the structure and flow logic of the flexible body option is also contained in this report. Additional information on the structure of the entire TOLA computer program is given in Reference 2.

## 2. PROGRAM DEVELOPMENT

2.1 Program Description and Capabilities - The flexible body option version of TOLA provides the capability to predict the total motion of an aircraft in the ground operating environment including airframe elastic effects and landing gear dynamics. It can simulate any conventional aircraft having up to five landing gears and four engines with the airframe considered either rigid or flexible. In the flexible airframe option, the flexibility is represented by superposition of the free-free vibratory modes on the rigid body motion. From one to twenty modes may be included to represent this airframe flexibility. The dynamic effects of a maximum of five independent landing gears can also be simulated. The landing gear modelled in the program is a double air chamber oleo strut with balloon tires, similar to that used on the C-5 aircraft (Figure 2-1). Each of the struts must lie in a plane parallel to the aircraft plane of symmetry, but the strut axis may be non-perpendicular to the longitudinal aircraft axis.

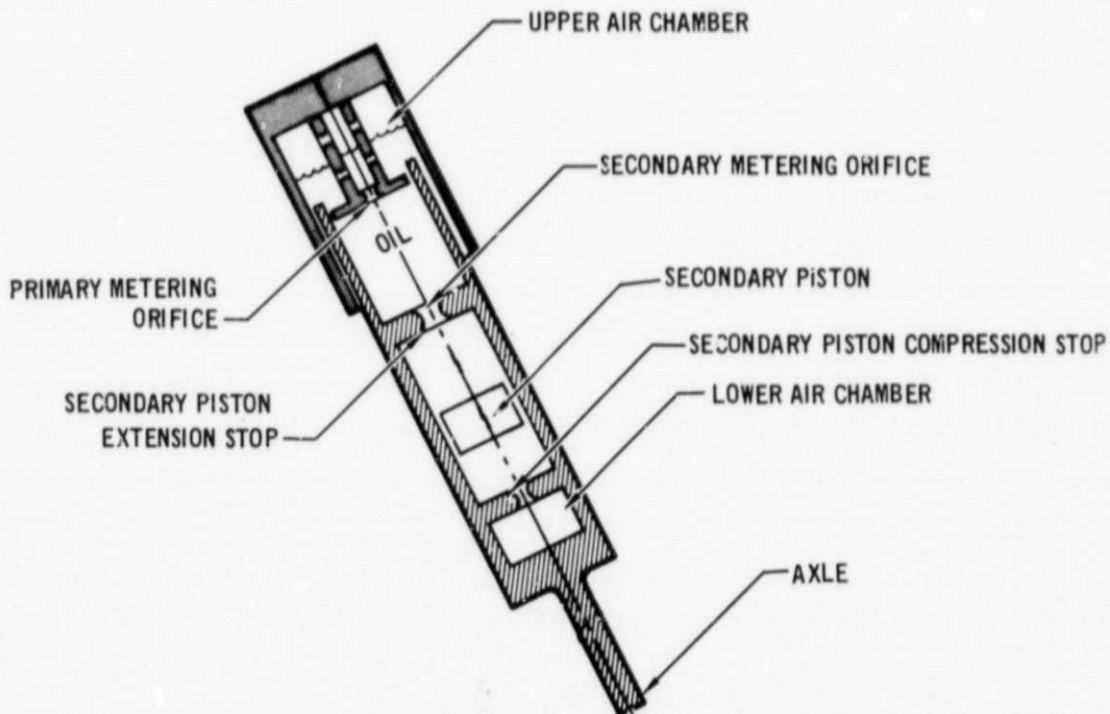


FIGURE 2-1 LANDING GEAR STRUT CONFIGURATION

The simulated aircraft, as represented by the airframe rigid and flexible body equations of motion and the strut, strut secondary piston and wheel equations of motion, may be subjected to time varying forces. The forces considered in the problem include engine thrust, aerodynamic loads including ground effects, drag chute forces, landing gear tire-ground reaction and braking forces. These forces may be varied and/or staged within the aircraft's capability by the maneuver logic and autopilot simulation.

The function of the autopilot simulation is to specify the timing and magnitude of the aircraft's control system inputs required for the desired aircraft performance during glide slope, flare, landing roll and takeoff roll. The maneuver logic utilizes information on the state of the aircraft obtained from solution of the airplane equations of motion to compute state errors. If necessary, it defines maneuvers required to maintain proper aircraft attitude by specifying parameters such as angle of attack, roll angle, thrust level and braking values. The maneuver logic also controls the staging of such events as spoiler activation, kill power, thrust reversal, drag chute deployment and brake activation in both normal and unusual takeoff or landing situations. The unusual situations include engine failure, brake failure or tire blow-out.

2.2 Development of Equations of Motion - To determine the response of an aircraft under any of the conditions described above, the equations of motion for that aircraft must be solved. As complex as the various options in the TOLA computer program may seem, they simply calculate their particular influence on these equations. The flexible body option is no exception. To understand this option and its effect on the overall program, its contributions to the existing equations of motion must first be understood. Since the equations which define the effects of a flexible airframe cannot be uncoupled from the overall problem, this section will give a general development of the total aircraft equations of motion including flexibility effects.

In developing the airplane equations of motion, the airplane main body is defined as the airplane less its landing gears. As such, the airplane is represented by  $K+1$  bodies. The aircraft main body is considered the  $0^{\text{th}}$  body while a typical landing gear is considered the  $k^{\text{th}}$  body with  $K$  being the total number of gears. Although the landing gears are considered rigid, they are allowed to move relative to the main body.



The coordinate systems used in the development of the equations of motion are shown in Figure 2-2. The inertial coordinate system  $(X_g, Y_g, Z_g)$  is fixed relative to the earth's local acceleration gravity vector. The body coordinate system  $(X_o, Y_o, Z_o)$  moves with the airplane and is fixed at the center of mass. The strut coordinate system  $(X_k, Y_k, Z_k)$  moves with the airplane and is located relative to the body coordinate system by the vector  $(\bar{R}_k)_o$  and the angle  $\Theta_k$ . This axes system is aligned such that the direction of gear movement is along the  $Z_k$  vector.

The dynamic motion of the main body is described using the normal mode method. In this method the main body motion is approximated by the combination of a limited number of vibratory modes plus the six rigid body modes. The main body's flexibility is represented by its free-free (unrestrained) vibratory modes. The rigid body modes are assumed to be the three translational displacements defining the airplane center of mass and three angular displacements defined in the body coordinate system.

In developing the airplane equations of motion, expressions defining the motion of an arbitrary point located on the landing gear and/or main body were obtained. These were used to evaluate the kinetic and potential energy of the airplane. The equations of motion were obtained by applying the Lagrangian equations to these energy expressions.

Using Figure 2-3, the total displacement of a point  $i$  is defined as

$$\bar{\rho}_{ki} = \bar{R} + (\bar{R}_k)_o + \bar{r}_{ki} \quad (2-1)$$

- $\bar{\rho}_{ki}$  = position vector of point  $i$  relative to the inertial coordinate system.
- $\bar{R}$  = position vector of reference point on main or  $0^{th}$  body relative to inertial coordinate system.
- $(\bar{R}_k)_o$  = position vector of  $k^{th}$  body reference point relative to the body coordinate system.
- $\bar{r}_{ki}$  = position vector of point  $i$  relative to the strut or  $k^{th}$  body coordinate system.
- $k$  = Subscript defining a specific body. The airplane minus its gears is the  $0^{th}$  body ( $k = 0$ ). A typical landing gear is the  $k^{th}$  body ( $k = 1, 2, 3 \dots K$ ).

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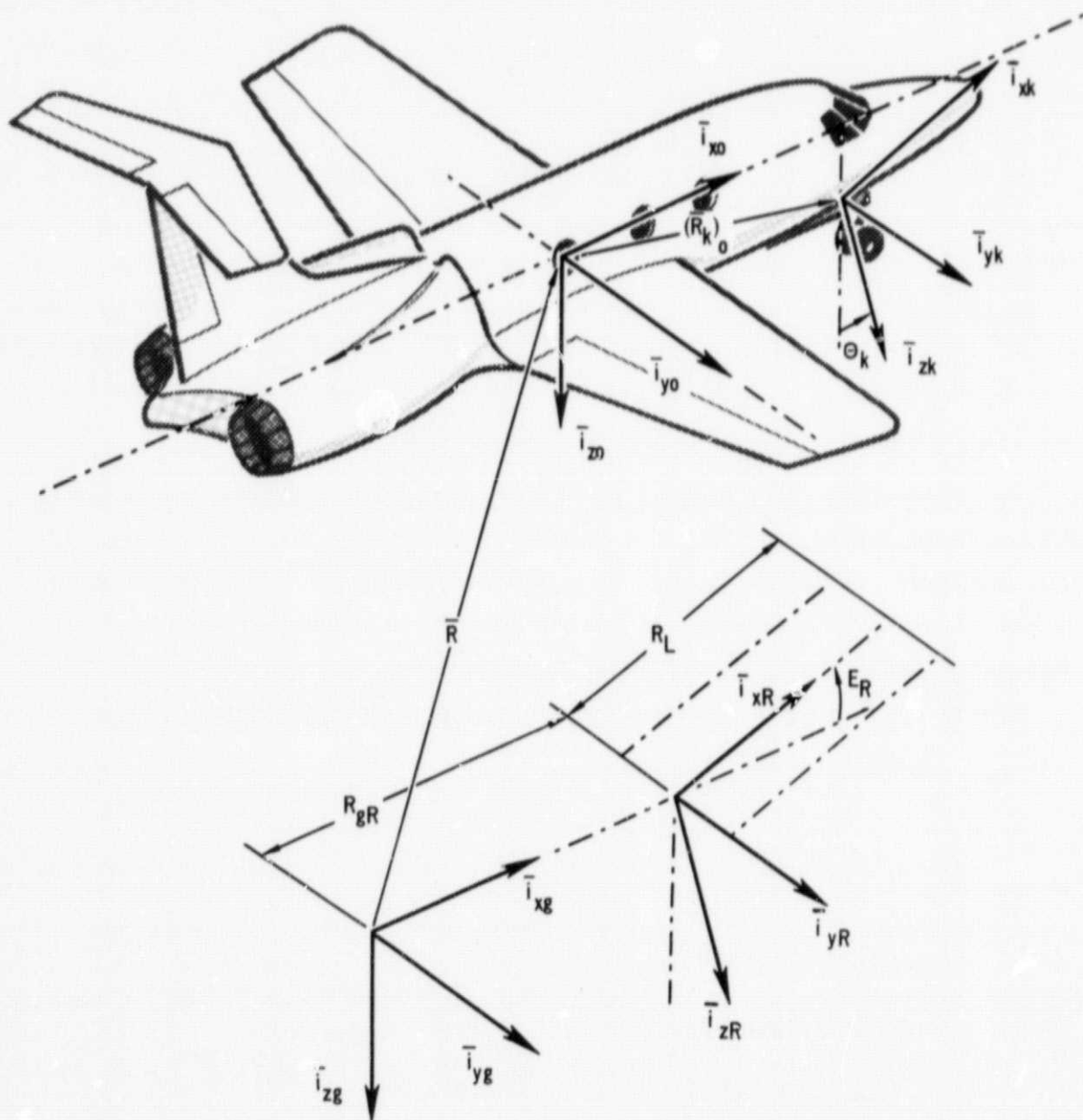


FIGURE 2-2 COORDINATE SYSTEMS

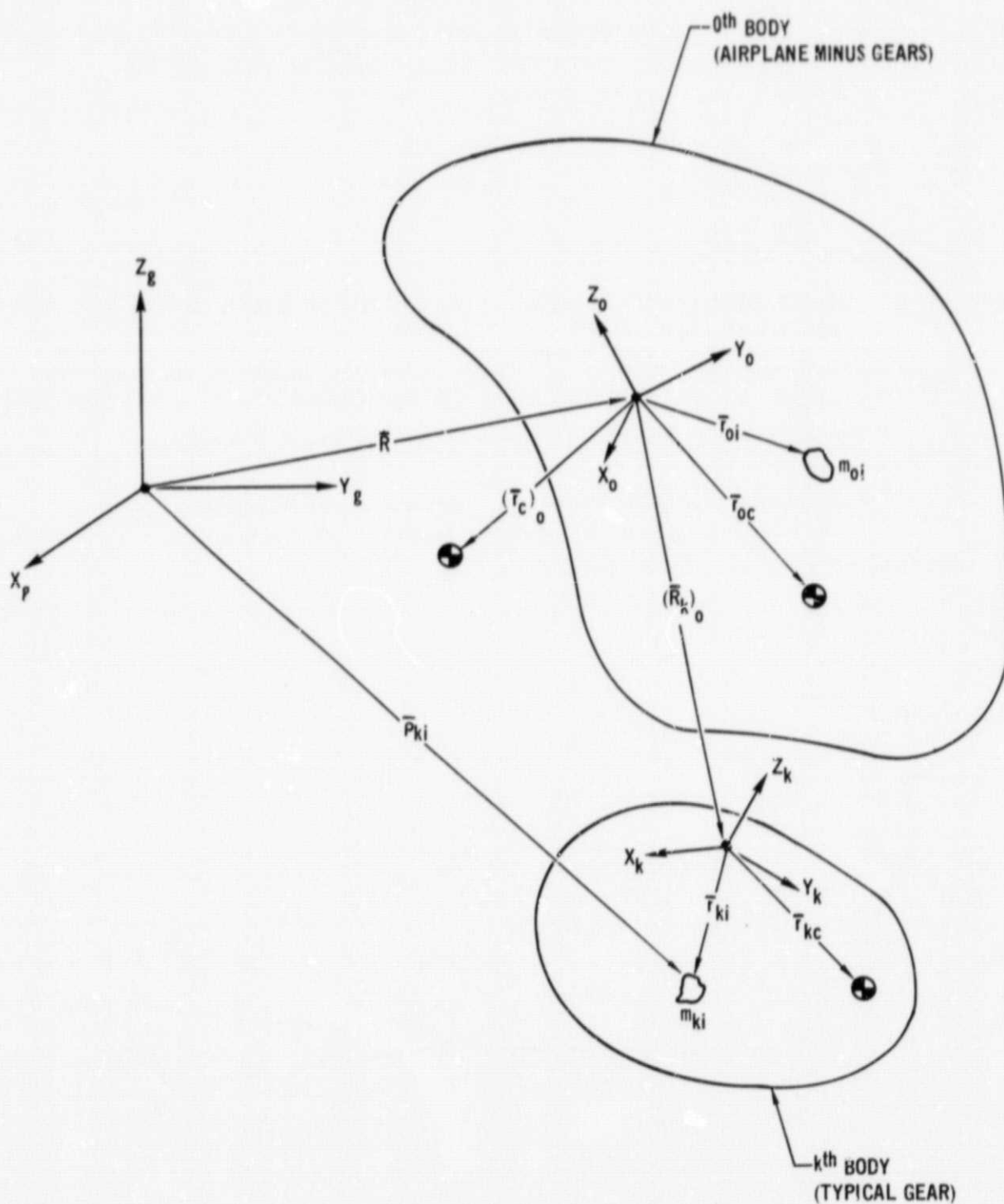


FIGURE 2-3 POSITION VECTORS

It is assumed that the position vectors  $(\bar{R}_k)_o$  and  $\bar{r}_{ki}$  used to locate point i in equation (2-1) can be separated into terms which vary with time and terms which remain constant with time. Thus, these vectors may be written

$$(\bar{R}_k)_o = \bar{R}_{ks} + \bar{R}_{ke}(t) \quad (2-2)$$

$$\bar{r}_{ki} = \bar{r}_{kis} + \bar{r}_{kie}(t)$$

where  $\bar{R}_{ks}$  = undeformed position of  $k^{\text{th}}$  body reference point in the body coordinate system

$\bar{R}_{ke}(t)$  = deformed position of  $k^{\text{th}}$  body reference point in the body coordinate system measured from the undeformed position of that point

$\bar{r}_{kis}$  = undeformed position of point i in the strut coordinate system.

$\bar{r}_{kie}(t)$  = deformed position of point i in the strut coordinate system measured from the undeformed position of that point

These position vectors are shown in Figure 2.4.

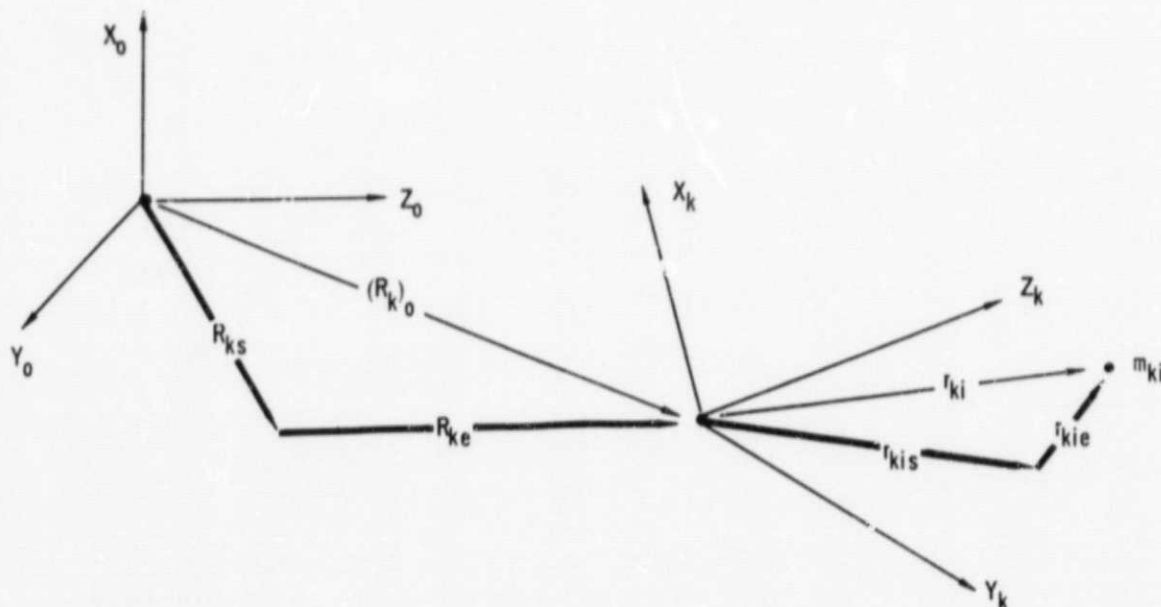


FIGURE 2-4 POSITION OF POINT i RELATIVE TO BODY COORDINATE SYSTEM

Since it is assumed that the elastic deformation of the airplane main body can be represented by the superposition of a limited number of vibratory modes, the terms of  $(\bar{R}_k)_o$  and  $\bar{r}_{ki}$  that vary with time may be written as

$$\bar{R}_{ke}(t) = \sum_{n=1}^N \phi_n^{-k} q_n(t)$$

and for  $k = 0$

(2-3)

$$\bar{r}_{oie}(t) = \sum_{n=1}^N \phi_n^{-1} q_n(t)$$

where  $N$  = number of vibratory modes included

$\phi_n^{-1}, \phi_n^{-k}$  = magnitude of  $n^{\text{th}}$  elastic mode at points  $i$  and  $k$  respectively.  
( $k$  used as a superscript refers to attachment point of  $k^{\text{th}}$  body,  
 $k = 1, 2, 3 \dots K$ )

$q_n$  = generalized coordinate associated with the  $n^{\text{th}}$  mode. These are a function of time.

Combining the above equations gives the final form for the location of a point  $i$  (Figure 2-3) as

$$\bar{r}_{oi} = \bar{R} + \bar{R}_{ks} + \sum_{n=1}^N \phi_n^{-k} q_n(t) + \bar{r}_{kis} + \sum_{n=1}^N \phi_n^{-1} q_n(t) \quad (2-4)$$

The kinetic energy of the  $K+1$  bodies,  $T$ , is obtained by summing the kinetic energy of all points  $i$  in the system having mass  $m_{ki}$

$$T = \frac{1}{2} \sum_{k=0}^K \sum_{i=1}^I m_{ki} \dot{\rho}_{ki} \dot{\rho}_{ki} \quad (2-5)$$

where  $K$  = total number of landing gears

$I$  = total number of mass points

$\dot{\rho}_{ki}$  = time derivative of the displacement vector

The potential energy,  $U$ , due to the strain energy of the main or  $0^{\text{th}}$  body is

$$U = \frac{1}{2} \sum_{n=1}^N \omega_n^2 m_n q_n^2 \quad (2-6)$$

where  $\omega_n$  = the natural frequency of the  $n^{\text{th}}$  free-free mode

$m_n$  = generalized mass of  $n^{\text{th}}$  elastic mode

The airplane's equations of motion were obtained by using the Lagrangian equations and the energy expressions of (2-5) and (2-6). The Lagrangian equations may be written

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \dot{q}_p} \right) - \frac{\partial T}{\partial q_p} + \frac{\partial U}{\partial q_p} = Q_p \quad (2-7)$$

where  $q_p, \dot{q}_p$  =  $p^{\text{th}}$  generalized coordinate and generalized velocity respectively

$Q_p$  = generalized force or moment in  $p^{\text{th}}$  mode

The resulting rigid body translational, rigid body rotational, and the flexible body equations of motion are given in Equations (2-8), (2-9), and (2-10) respectively.

Certain simplifying assumptions were made in the equations of motion. These assumptions were consistent with those made in the existing TOLA formulation. In the rigid body equations, the Coriolis acceleration terms for the landing gear struts were neglected mainly because the rotational velocities of the aircraft are small at landing relative to strut acceleration terms retained. Also, in the rigid body rotational equations, terms involving the variation of the inertia or inertia derivative tensors resulting from changing position vectors of the strut masses are small. The changes in the

# RIGID BODY TRANSLATIONAL EQUATIONS

$$\begin{aligned} \bar{F}_T = M_T \ddot{\bar{R}} - \sum_{k=1}^K m_k \ddot{S}_k [A_{k31} \bar{i}_{x0} + A_{k33} \bar{i}_{z0}] + \sum_{n=1}^N \sum_{k=1}^K m_k \ddot{q}_n [\phi_{xn}^k \bar{i}_{x0} \\ + \phi_{yn}^k \bar{i}_{y0} + \phi_{zn}^k \bar{i}_{z0}] \end{aligned} \quad (2-8)$$

# RIGID BODY ROTATIONAL EQUATIONS

$$\begin{aligned} \bar{M}_O = \bar{I} \cdot \dot{\bar{\omega}} + \bar{\omega} \times [\bar{I} \cdot \bar{\omega}] + \sum_{k=1}^K m_k \ddot{S}_k [-A_{k11} R_{ksy} \bar{i}_{x0} + (A_{k13} R_{ksz} \\ + A_{k11} R_{ksx}) \bar{i}_{y0} - A_{k13} R_{ksy} \bar{i}_{z0}] \\ + \sum_{n=1}^N \sum_{k=1}^K m_k \ddot{q}_n \left\{ [R_{ksy} \phi_{zn}^k - (R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{yn}^k] \bar{i}_{x0} \right. \quad (2-9) \\ + [(R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{xn}^k - (R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{zn}^k] \bar{i}_{y0} \\ \left. + [(R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{yn}^k - R_{ksy} \phi_{xn}^k] \bar{i}_{z0} \right\} \end{aligned}$$

Symbols are defined on the following page

# RIGID BODY EQUATIONS OF MOTION

$F_T$  = total applied force acting on K+1 bodies

$M_T$  = total mass of K+1 bodies

$m_k$  = mass of the  $k^{th}$  strut

$\ddot{S}_k$  = acceleration of  $k^{th}$  strut mass

$A_{k11}, A_{k13}, A_{k31}, A_{k33}$  = direction cosines relating strut coordinate system to  $0^{th}$  body coordinate system

$\bar{M}_O$  = total moment of all applied forces on K+1 bodies about  $0^{th}$  body center of mass

$\bar{I}$  = inertia tensor for the K+1 bodies about  $0^{th}$  body center of mass

$\bar{\omega}$  = angular velocity of  $0^{th}$  body in body coordinate system

$R_{ksx}, R_{ksy}, R_{ksz}$  = X, Y, Z components of strut attach point position vector

$r_{Fk}$  = distance from strut attach point to extended position of axle

$S_{kc}$  = distance from strut axle to strut center of mass



# FLEXIBLE AIRFRAME EQUATIONS OF MOTION

FOR  $S = 1, 2, 3, \dots, N$

$$\begin{aligned}
 & m_s \ddot{q}_s + \omega_s^2 m_s q_s + \sum_{n=1}^N \sum_{k=1}^K m_k [\phi_{xs}^k \phi_{xn}^k + \phi_{ys}^k \phi_{yn}^k + \phi_{zs}^k \phi_{zn}^k] \dot{q}_n \\
 & + \sum_{k=1}^K m_k [(\ddot{Y} - A_{k31} \ddot{S}_k) \phi_{xs}^k + \ddot{Y} \phi_{ys}^k + (\ddot{Z} - A_{k33} \ddot{S}_k) \phi_{zs}^k] \\
 & + \dot{\omega}_x \sum_{k=1}^K m_k [R_{ksy} \phi_{zs}^k - (R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{ys}^k] \quad (2-10) \\
 & + \dot{\omega}_y \sum_{k=1}^K m_k [(R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{xs}^k - (R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{zs}^k] \\
 & + \dot{\omega}_z \sum_{k=1}^K m_k [(R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{ys}^k - R_{ksy} \phi_{xs}^k] = Q_s
 \end{aligned}$$

$Q_s = Q_s^T + Q_s^{DC} + Q_s^A$  = Generalized forces associated with  $s$  th mode due to engine thrust, drag chute deployment and aerodynamic pressure respectively

Symbols are defined on the following page

# FLEXIBLE AIRFRAME EQUATIONS OF MOTION

$m_s, q_s, \omega_s$  = Generalized mass, generalized coordinate and natural frequency respectively associated with the  $s$  th elastic free-free mode

$$Q_s^T = \phi_{xs}^1 T_{x1} + \phi_{xs}^2 T_{x2} + \phi_{xs}^3 T_{x3} + \phi_{xs}^4 T_{x4}$$

$T_{x1}$  through  $T_{x4}$  = Engine thrust forces

$\phi_{xs}^1$  through  $\phi_{xs}^4$  = Magnitude of  $s$  th mode shape at point force application

$$Q_s^{DC} = \phi_{xs}^{DC} F_{cx} + \phi_{ys}^{DC} F_{cy} + \phi_{zs}^{DC} F_{cz}$$

$F_{cx}, F_{cy}, F_{cz}$  = Forces due to deployment of drag chute

$\phi_{xs}^{DC}, \phi_{ys}^{DC}, \phi_{zs}^{DC}$  = Magnitude of  $s$  th mode shape at point of force application

$$Q_s^A = -B_s^1 \phi_{xs}^A a + B_s^2 \phi_{ys}^A y - B_s^3 \phi_{zs}^A n_f + B_s^4 \theta_{xs}^A l + B_s^5 \theta_{ys}^A m + B_s^6 \theta_{zs}^A n$$

$a, y, n_f$  = Aerodynamic forces;  $l, m, n$  = aerodynamic moments

$\phi_{xs}^A, \phi_{ys}^A, \phi_{zs}^A$  = Magnitude of  $s$  th mode shape at point of force application

$\theta_{xs}^A, \theta_{ys}^A, \theta_{zs}^A$  = Slope of  $s$  th mode shape at point of moment application

$B_s^1$  through  $B_s^6$  = Participation factors for  $s$  th mode

gear positions are very small compared to the overall airplane dimensions, therefore the variation of the inertia terms due to gear position changes are small and were neglected. The flexible airframe equations of motion were also simplified by neglecting terms analogous to those neglected in the rigid body equations. Coriolis and centripetal type accelerations of the strut masses were considered small, again mainly because the rotational velocities of the aircraft are small relative to the strut acceleration terms retained. Rigid body "tangential" type acceleration terms that vary with changing position vectors were neglected; however, all others were retained.

Reference 3 gives a more thorough derivation of the total aircraft equations of motion. In addition, topics such as the determination and implementation of elastic airframe effects on strut equations of motion are also discussed. The reader will find additional information on these and other aspects of the flexible body option version of TOLA presented in Reference 3 that will aid his understanding of the program operation.

### 3. PROGRAM DESCRIPTION

3.1 Program Structure - The equations describing the motion of points on a flexible airframe are formulated and solved in subroutine FLEX1. This subroutine can determine the response at twenty points on an airframe whose stiffness characteristics are defined by the modal deflections and natural frequencies for a maximum of twenty modes. A matrix approach was used to simultaneously formulate and solve all flexible body equations of motion at a particular point in time.

The basic structure of TOLA has been retained. It still consists of three OVERLAY segments. OVERLAY (TOLA, 0, 0) consists of the executive subprogram TOLA. Through its call to subroutine EXE, it calls the other two overlays and controls the execution of the complete program. TOLAN1 is the executive subprogram in OVERLAY (TOLA, 1, 0). It reads the input data and checks to determine if the proper amount of input data has been supplied. TOLAN2 is the executive subprogram in OVERLAY (TOLA, 2, 0). It provides the autopilot and phasing functions. A diagram showing the general structure of the revised TOLA program is given in Figure 3-1. This diagram is not intended to be a comprehensive programming chart, but shows the general flow of the flexible body option logic. A listing of the TOLA computer program is given in Appendix A.

Subroutine FLEX1 is located in OVERLAY (TOLA, 0, 0). The format used in structuring this subroutine closely follows that of existing subroutines so as to make it compatible with the logic used in the TOLA program. This structure enables calls to entries in FLEX1 to be placed in the EXE and OPT1 subroutines at those points where calls are made to other subprograms that perform similar functions.

All input data associated with the flexible body option are stored in COMMON/DIRCOM/. Those data calculated within the subroutine and passed to other parts of the program are stored in COMMON/FLXOP/. This use of common simplifies the communication between subroutines.

3.2 Program Operation - An understanding of program development in itself will not result in smooth program operation. Successful operation of the TOLA computer program with the flexible body option depends on proper input of all required data. Much of these data are associated with the existing rigid body version of TOLA. It is not the purpose of this document to define

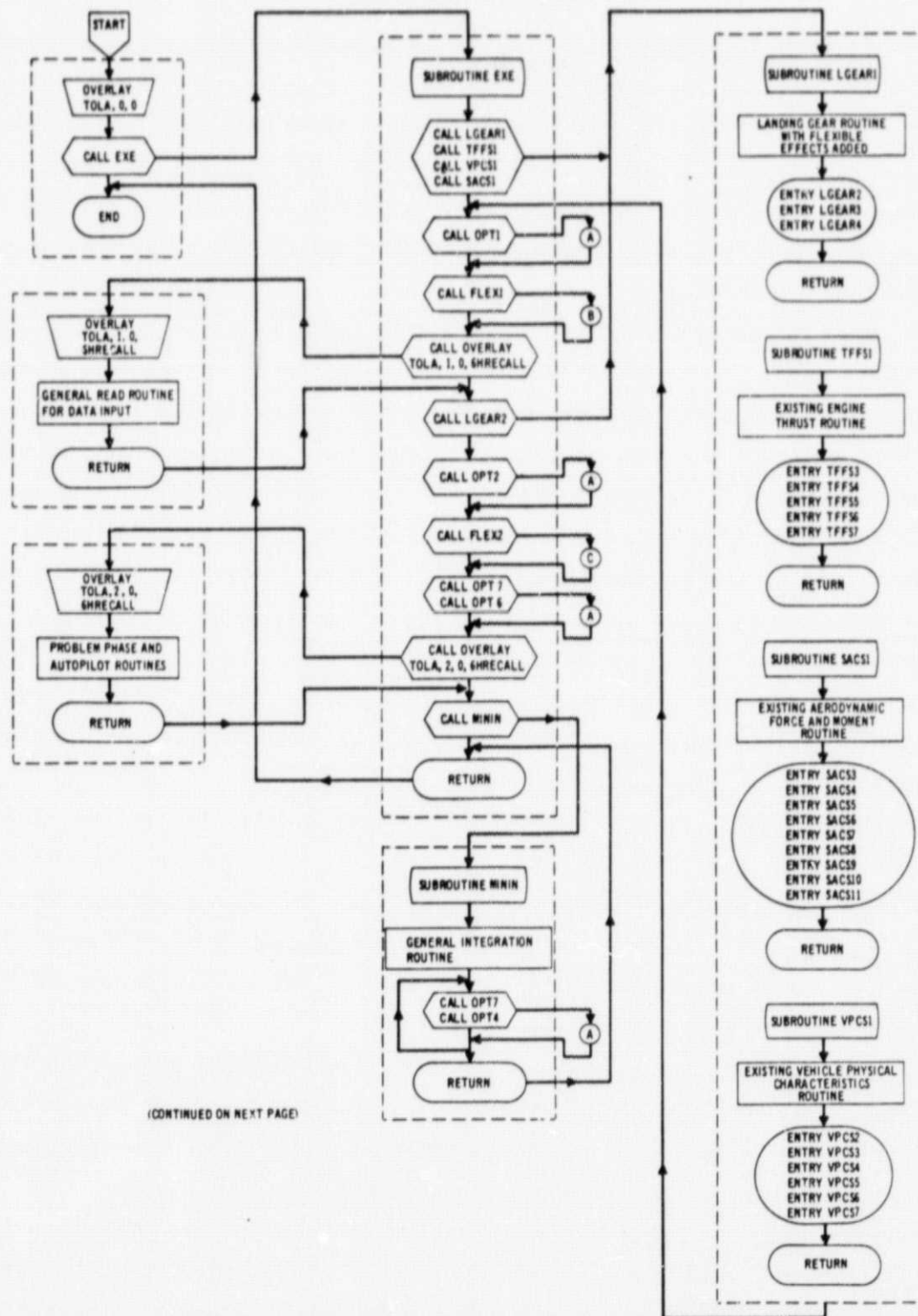


FIGURE 3-1 FLOW DIAGRAM FOR TOLA COMPUTER PORGRAM FLEXIBLE BODY OPTION

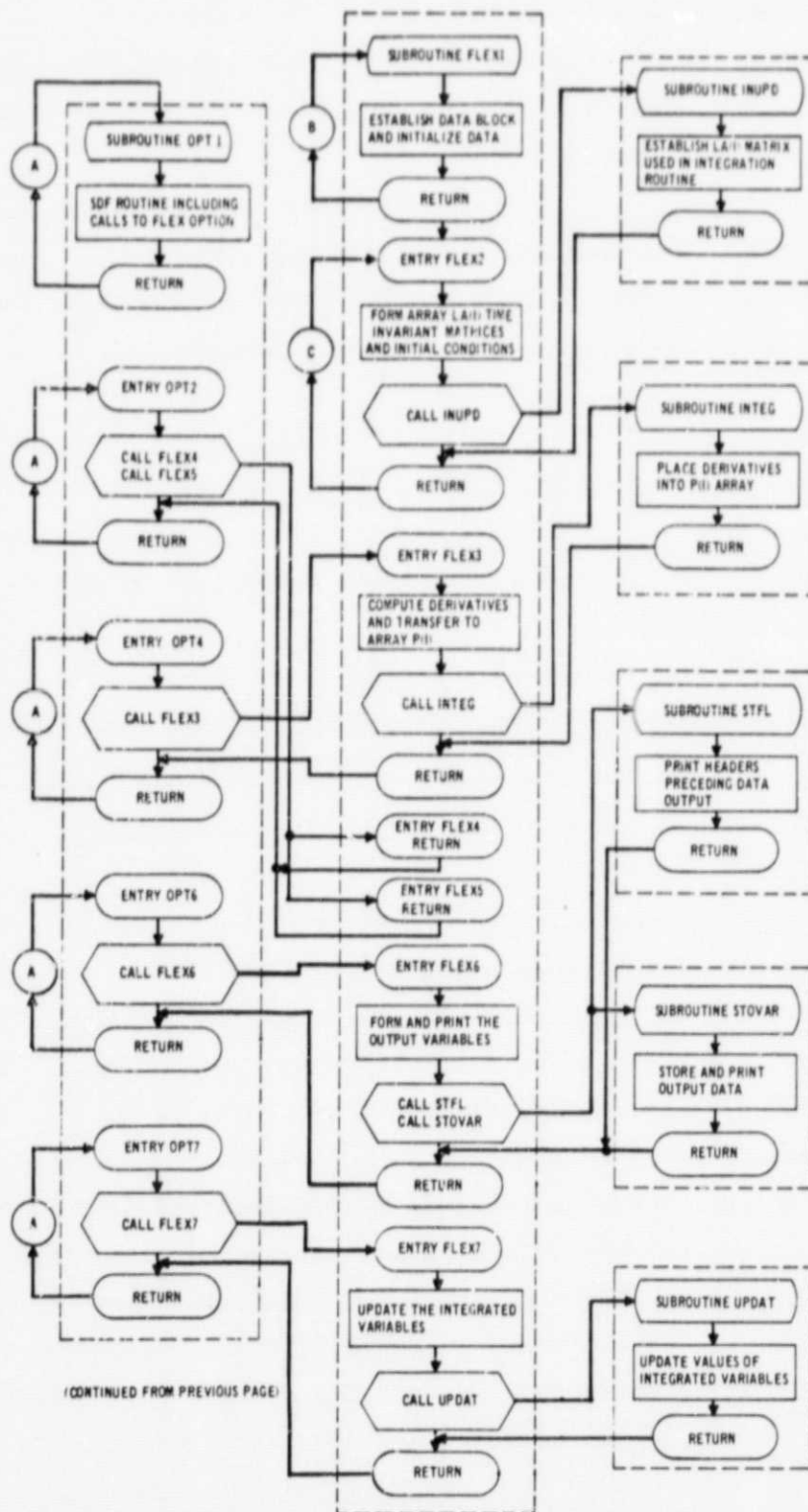


FIGURE 3-1 FLOW DIAGRAM FOR TOLA COMPUTER PROGRAM FLEXIBLE BODY OPTION (Continued)



3.2.1 General Input Data Format - The input data associated with the flexible body option are read into the program by the existing input routine (READ). As a result, it must follow the same general format as the rigid body data. The input must follow the following format:

Card Columns	1-6	7	8-10	11	12-66	67-72	73-80
Field Number	I	II	III	IV	V	VI	VII

Field number I contains the alphanumeric variable name of the data contained in Field V. Example:

STATEMENT NUMBER		FORTRAN STATEMENT																																													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	
I N D E X																																															

Field number II is not used.

[illegible]





INPUT INDICATOR/ VARIABLE	COORDINATE SYSTEM(1)	INDICATOR OR VARIABLE DEFINITION
INDFLX		INDICATOR DEFINING OPTION INDFLX = 0 - RIGID AIRFRAME INDFLX = 1 - FLEXIBLE AIRFRAME
NMODE		INDICATES NUMBER OF MODES INPUT (20 MAXIMUM)
GMASS1(I)		GENERALIZED MASS OF I TH ELASTIC MODE
GFREQ(I)		FREQUENCY OF I TH MODE (RADIAN/SEC)
SXMOD(I)	BCS	X MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
SYMOD(I)	BCS	Y MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
SZMOD(I)	BCS	Z MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
TXMOD(I)	BCS	X MODE SHAPE FOR ENGINE THRUST APPLICATION ATTACHMENT POINTS IN I TH MODE
ARMODE(I)	BCS	X,Y,Z, $\theta_x$ , $\theta_y$ , $\theta_z$ COMPONENTS OF MODE SHAPE FOR AERODYNAMIC FORCE AND MOMENT REFER- ENCE LOCATION IN I TH MODE
PF(I)		PARTICIPATION FACTORS OF GENERALIZED AERODYNAMIC FORCES AND MOMENTS IN I TH MODE
SKC(K)	SCS	DISTANCE BETWEEN K TH STRUT AXLE AND STRUT CENTER OF MASS
DCMODE(I)	BCS	X,Y,Z COMPONENTS OF MODE SHAPE FOR DRAG CHUTE ATTACHMENT POINT IN I TH MODE
NPTS		NUMBER OF POINTS ON THE AIRFRAME AT WHICH OUTPUT IS REQUESTED (20 MAXIMUM)
ROIS(J)	BCS	ROISX, ROISY, ROISZ COMPONENTS OF POSITION VECTOR FOR J TH POINT ON FLEXIBLE AIRFRAME AT WHICH OUTPUT IS REQUESTED
OUTMOD(I)	BCS	X,Y,Z COMPONENTS OF I TH MODE SHAPE FOR POINTS ON FLEXIBLE AIRFRAME AT WHICH OUTPUT IS REQUESTED.
IFLX(I)		INDICATES THE POINTS WHOSE DATA WILL BE STORED ON TAPE

(1) NOTE: BCS = BODY COORDINATE SYSTEM SCS = STRUT COORDINATE SYSTEM

FIGURE 3-2 INPUT DATA FOR TOLA FLEXIBLE BODY OPTION

can be used. The natural frequency, GFREQ(I), and generalized mass, GMASS1(I), for each mode must be input. The mode shape magnitudes, SXMOD(I), SYMOD(Y), SZMOD(Z), for each mode at the strut attachment locations should be input. While the program will run without these input data, it will use a value of zero for the mode shape magnitudes. Similarly, the mode shape data at the point of application of the engine thrust, TXMOD(I), and aerodynamic forces and moments, ARMODE(I), should be input for solution of any practical takeoff/landing problem.

The aerodynamic loads are treated as concentrated loads in TOLA in the form of total aerodynamic forces and moments acting at a selected reference point on the airframe. To obtain realistic flexible body response, weighting effects or participation factors, PF(I), of the aerodynamic loads on the response of each normal mode are required. If aerodynamic effects on the flexible airframe response are desired, the user must input the proper values for the PF(I) array. If the PF(I) are not input, the default values for this array are zero and all effects of the aerodynamic loads on modal response are assumed to be small and therefore neglected. A general approach for calculating the aerodynamic weighting effects is suggested in Appendix B.

All of the arrays used in the flexible body option are in vector form (one dimensional), and the subroutine expects the modal data to appear in a particular order on the data input cards. The order required by the subroutine is best shown through an example. If the aircraft simulated in the program has three landing gear struts and two engines, and four vibratory modes are selected to represent airframe flexibility, then the typical strut and engine attachment point modal data would appear as follows:

Strut 1 Attach Point

Mode	X	Y	Z
1	-.41	.68	-.14
2	.38	.03	.79
3	-.40	-.08	.03
4	-.25	.16	.17

### Strut 2 Attach Point

Mode	X	Y	Z
1	-.83	.69	-.33
2	.48	.06	.86
3	-.83	-.07	.05
4	-.47	.17	.38

### Strut 3 Attach Point

Mode	X	Y	Z
1	-1.00	.69	-.41
2	.52	.07	.89
3	-1.00	-.08	.05
4	-.55	.17	.49

### Engine 1 Attach Point

Mode	X
1	-.64
2	.29
3	-.59
4	-.32

### Engine 2 Attach Point

Mode	X
1	-.68
2	.36
3	-.65
4	-.37

Write each component of the strut attachment point mode shape as though in an array dimensioned number-of-struts x number-of-modes.

$$\begin{aligned}
 [\text{SXMOD}] &= \begin{bmatrix} -.41 & .38 & -.40 & -.25 \\ -.83 & .48 & -.83 & -.47 \\ -1.0 & .52 & -1.0 & -.55 \end{bmatrix} \\
 [\text{SYMOD}] &= \begin{bmatrix} .68 & .03 & -.08 & .16 \\ .69 & .06 & -.07 & .17 \\ .69 & .07 & -.08 & .17 \end{bmatrix} \\
 [\text{SZMOD}] &= \begin{bmatrix} -.14 & .79 & .03 & .17 \\ -.33 & .86 & .05 & .38 \\ -.41 & .89 & .05 & .49 \end{bmatrix}
 \end{aligned}$$

The engine attachment point modal data should be written in an array dimensioned number-of-engines x number-of-modes:

$$[\text{TXMOD}] = \begin{bmatrix} -.64 & .29 & -.59 & -.32 \\ -.68 & .36 & -.65 & -.37 \end{bmatrix}$$

Transform each array into vector form by reading the matrix elements by columns. Thus the order in which the data is read would be as follows:

SXMOD = -.41	SYMOD = .68	SZMOD = -.14	TXMOD = -.64
-.83	.69	-.33	-.68
-1.0	.69	-.41	.29
.38	.03	.79	.36
.48	.06	.86	-.59
.52	.07	.89	-.65
-.40	-.08	.03	-.32
-.83	-.07	.05	-.37
-1.0	-.08	.05	
-.25	.16	.17	
-.47	.17	.38	
-.55	.17	.49	

These data would then be placed on cards according to the format described in the previous section.

Typical aerodynamic data and participation factors would appear as follows:

#### Aerodynamic Data

Mode	X	Y	Z	$\theta_X$	$\theta_Y$	$\theta_Z$
1	.16	.20	-.89	.0004	.0045	.0009
2	.20	.15	-.96	.0002	.0053	-.0003
3	.12	.08	-.65	-.0001	.0038	.0010
4	.05	.09	-.59	.0003	.0036	-.0007

#### Participation Factors

Mode	X	Y	Z	$\theta_X$	$\theta_Y$	$\theta_Z$
1	.30	.36	-1.87	.15	-.93	.20
2	.46	.39	2.15	.12	-1.15	-.09
3	.28	.21	-1.13	.04	-.83	.21
4	.16	.24	.97	.08	-.79	-.17

Again, write the data in an array where each column represents the data for a single mode; then read the matrix columnwise.

$$\text{ARMODE} = \begin{bmatrix} .16 & .20 & .12 & .05 \\ .20 & .15 & .08 & .09 \\ -.89 & -.96 & -.65 & -.59 \\ .0004 & .0002 & -.0001 & .0003 \\ .0045 & .0053 & .0038 & .0036 \\ .0009 & -.0003 & .0010 & -.0007 \end{bmatrix} \quad \text{PF} = \begin{bmatrix} .30 & .46 & .28 & .16 \\ .36 & .39 & .21 & .24 \\ -1.87 & 2.15 & -1.13 & .97 \\ .15 & .12 & .04 & .08 \\ -.93 & -1.15 & -.83 & -.79 \\ .20 & -.09 & .21 & -.17 \end{bmatrix}$$

ARMODE = .16

.20

-.89

.0004

.0045

.0009

.20

.15

.

.

.

PF = .30

.36

1.87

.15

-.93

.20

.46

.39

.

.

.

SKC(K) and DCMODE(I) are optional data. The program sets these quantities to zero if not input. SKC(K) is the distance from the tire axle to the strut center of mass measured along the strut stroke. It is approximately equal to zero for many landing gears. The order in which the struts are numbered in SKC(K) must be consistent with the order implied by the strut attachment point mode shapes. If the third row in the modal data represents the motion of the third strut attachment point, the third element in array SKC(K) must be the described distance for that strut.

DCMODE(I) defines the mode shape at the drag chute attach point and is necessary only when the aircraft has a drag chute. These modal data are input in an order similar to that for the aerodynamic data. If written in a two-dimensional array, each column of data represents the X, Y, Z components of the mode shape for a given mode.

The remaining input data indicated in Figure 3-2 are necessary to obtain flexible body response output on the airframe. NPTS indicates the number of points at which output is requested. ROIS(J) are the X, Y, Z components of

the position vector defining the location of the points relative to the airframe or 0th body coordinate system. OUTMOD(I) are the components of each mode shape at those points for which output is specified. As before, the order of the data is significant and an example will best show this. If output is desired at two points on the aircraft, typical data would appear as below:

Point 1

Location	Mode	1	2	3	4
X = 2.71	X	.09	.11	-.05	.02
Y = 17.63	Y	.02	.01	-.03	.01
Z = 1.52	Z	.95	-.98	.87	-.77

Point 2

Location	Mode	1	2	3	4
X = 2.71	X	.07	.10	-.04	.01
Y = 8.42	Y	.01	-.02	-.03	-.02
Z = 1.25	Z	.43	-.39	.41	-.29

The matrix ROIS(J) should be written as though dimensioned 3(X,Y,Z) x NPTS and then read by columns. For the above example, ROIS(J) would appear as follows:

$$\text{ROIS(J)} = 2.71, 17.63, 1.52, 2.71, 8.42, 1.25$$

Each column of OUTMOD(I) should contain all of the modal data for a given point. The X component of data for all modes should precede the Y component, with the Y component preceding the Z. Written in two dimensional form for the example being considered, OUTMOD(I) would be given as:

$$[\text{OUTMOD}] = \begin{bmatrix} .09 & .07 \\ .11 & .10 \\ -.05 & -.04 \\ .02 & .01 \\ .02 & .01 \\ .01 & -.02 \\ -.03 & -.03 \\ .01 & -.02 \end{bmatrix} \left\{ \begin{array}{l} \text{X Component} \\ \text{Y Component} \end{array} \right.$$



$$\begin{bmatrix} .95 & .43 \\ -.98 & -.39 \\ .87 & .41 \\ -.77 & -.29 \end{bmatrix} \left. \vphantom{\begin{bmatrix} .95 & .43 \\ -.98 & -.39 \\ .87 & .41 \\ -.77 & -.29 \end{bmatrix}} \right\} \text{Z Component}$$

This matrix should be transformed to vector form by reading the elements by column.

The array IFLX(I) dictates which flexible body response data will be saved on tape and used as input for a plot routine. Subroutine FLEX can formulate and print the flexible body response at up to twenty points on the aircraft. IFLX(I) enables the user to select from these points, those whose data will be plotted. Each output point is assigned a number by the order in which their modal data appears in array ØUTMØD(I). An element in IFLX whose value is one will cause the data for that respective point to be placed on tape. For example, if response data is formulated at five points on the aircraft, IFLX = (1, 0, 1, 1, 0) will cause all flexible body data associated with point numbers one, three and four to be saved on tape. Other indicators required to store TOLA output data are discussed in Section 3.2.5. If no flexible body response data is desired, NPTS, RØIS, ØUTMØD and IFLX need not be input.

There is no specific system of units associated with the input information, except for the modal frequencies which must be expressed in radians/unit time. All other parameters may be expressed in any consistent set of units, either English or Metric (inches or centimeters, pounds or dynes). The units selected must, of course, be consistent with the rigid body set used (see Reference 1).

3.2.3 Output Data from the Flexible Body Option - The data that can be output from subroutine FLEX1 consists of the flexible body components of the inertial accelerations, velocity and displacement in each of the three body coordinate directions and the total inertial acceleration and velocity in each coordinate direction. The output variable names used in FLEX1 and their definition are given in Figure 3-3.

3.2.4 Staging the Flexible Body Option into the Program - If aircraft elasticity is desired in an analysis, the program will turn the flexible body option subroutine on at the same time the landing gear subroutine is staged

ALL QUANTITIES ARE IN BODY COORDINATES

POINT - DEFINES THE POINT NUMBER (1-20)

XD2F -- X COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

XD2T -- X COMPONENT OF THE TOTAL INERTIAL ACCELERATION

YD2F -- Y COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

YD2T -- Y COMPONENT OF THE TOTAL INERTIAL ACCELERATION

ZD2F -- Z COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

ZD2T -- Z COMPONENT OF THE TOTAL INERTIAL ACCELERATION

XD1F -- X COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

XD1T -- X COMPONENT OF THE TOTAL INERTIAL VELOCITY

YD1F -- Y COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

YD1T -- Y COMPONENT OF THE TOTAL INERTIAL VELOCITY

ZD1F -- Z COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

ZD1T -- Z COMPONENT OF THE TOTAL INERTIAL VELOCITY

XDOF -- X COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

YDOF -- Y COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

ZDOF -- Z COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

FIGURE 3-3 OUTPUT VARIABLES USED IN FLEX1



into the program. This is done by testing the values of both the flexible body option indicator (INDFLX) and the landing gear indicator (INDLG). Both must be non-zero for flexibility effects to be included.

Initial generalized displacements are calculated based on values of variables at the time the option is staged into the program. These initial displacements are then used in subsequent calculation of the generalized accelerations.

3.2.5 Data Plotting Information - Major revisions were made to the subroutine that stores data for use by a separate plotting program. As now rewritten, subroutine SDFLGP first prints headers that identify the variable names of the data that follow. These headers are printed only once. Each call to the subroutine then writes to tape all data associated with a single time point. This eliminates the need to store the data in intermediate arrays.

The indicators described in Reference 1 and earlier in this report that control the logic in SDFLGP have not been modified. They are as follows:

IPLT = 1	denotes that data will be stored on tape for plotting
ISDF = 1	indicates rigid body data will be saved
ISTPL1 = 1	} denotes that data for landing gears number 1 through 5 will be stored on tape
ISTPL2 = 1	
ISTPL3 = 1	
ISTPL4 = 1	
ISTPL5 = 1	
IFLX(I) = 1	indicates that flexible response data for the i th output point will be saved

A new plotting program was developed to be compatible with the data format of the revised TOLA subroutine SDFLGP. This program, entitled PLTDAT, is submitted as a separate job after a data tape has been generated by the TOLA program. The plot tape generated by PLTDAT can then be used by any off-line plotting device. A listing of the PLTDAT computer program is given in Appendix C.

The plot program was designed to permit the user a high degree of flexibility in the use of the program. Any variable stored for plotting may be chosen as the independent variable. Not only does this allow conventional time history plots to be made, but also such plots as the altitude of the

center of mass versus downrange position or strut acceleration versus strut stroke. A maximum of five dependent variables can be plotted on a single graph. This enables the user to make direct comparisons of several simultaneously displayed variables.

All graphs are scaled to an 8-1/2 x 11 inch page size; however, the actual plotting area depends on the number of dependent variables. The ordinate (dependent variable) axis is six inches in length. The length of the abscissa (independent variable) axis ranges from 9.4 inches for one dependent variable to 7.0 inches for five dependent variables.

The input data required by the plot program must follow a particular format. The first card contains an integer (format I6) that specifies the number of data points plotted per graph. The remaining cards control the number of plots, define graph titles and dictate the dependent and independent variables. This is accomplished by beginning each data card with a control identifier. These control identifiers are TITLE1, TITLE2, INDVAR, DEPVAR and PLOT. All identifiers must begin in column 1 with their associated data beginning in column 11. TITLE1 and TITLE2 permit a 40 character title and subtitle to be printed on the graph. If no titles are desired, these data are omitted. INDVAR defines the variable name on that card as the independent variable. DEPVAR defines a maximum of five variable names (format 5A10) as dependent variables. The word PLOT causes the graphs to be generated with the current titles, dependent and independent variables.

In order to uniquely identify all variables, a two digit numerical prefix is assigned to each repetitive data name. For example, if TOLA subroutine SDFLGP has saved data for landing gears one, three, and five, PLTDAT will assign a 01 prefix to all data for gear one, a 02 prefix to all data for gear three, and a 03 prefix to all data for gear five. Thus the strut acceleration for gear five would be 03SD2 while the strut stroke for gear three would be 02S.

Figure 3-8 shows a sample of input data for the plotting program. TOLA subroutine SDFLGP has already saved flexible body data for three points on the aircraft and landing gear data for gear numbers one, three, four and five. The first line in the plotting data indicates that two hundred points will be plotted on each graph. The main title for the first plot is "TOLA TIME HISTORY" while the subtitle is "STRUT ACCELERATIONS". The independent variable is time.

The dependent variables are the strut accelerations corresponding to the first three gears for which data is stored, struts one, three, and four.

[illegible]

FIGURE 3-4. SAMPLE OF PLOTTING DATA

For the second graph, no main title is defined so the program uses the current title defined by TITLE1. The subtitle for this plot is "STRUT DISPLACEMENTS" as shown by the TITLE2 card. The independent variable has not been redefined and therefore is still time. The dependent variables are the strut displacements for gears one, three and four.

The third and final plot indicated by these data also uses the current main title but redefines the subtitle as "FLEXIBLE ACCELERATION-PILOT STATION". The independent variable is still time while the single dependent variable is the vertical acceleration at the first flexible body point.

The following standard CalComp plotting routines are called by PLTDAT:

PLOTS	PLOT	SCALE	NUMBER
LABEL	SYMBOL	AXIS	

3.2.6 Comments on Program Operation - In addition to a working knowledge of the program, the user is generally interested in the size of the program

and its operating cost. Using the existing OVERLAY structure, the TOLA computer program with the flexible body option has a core requirement of 67K octal words. Most of the space associated with the flexible body option itself is allocated to store the potentially large quantity of input modal data. Every effort was made during program development to streamline the option.

Program operating costs vary from one computer system to the next so it is not possible to develop a single cost formula. Several observations, however, can be made. The major factors that effect the cost of a TOLA run are the total number of integration steps and the number of variables that need to be integrated. The number of integration steps is dictated by the time length of the analysis and the integration step size. Although the user has little control over the step size chosen by the integration routine, he can directly input the time at which the program will terminate. Care should be taken to insure that the program does not continue to run beyond the points of interest. An approximation to determine the time of a flexible body run is given by the expression:

$$(\text{TIME})_{\text{FLEX}} \approx (\text{TIME})_{\text{RIGID}} \cdot \left( \frac{(\text{NO. OF INTEGRATED VARIABLES})_{\text{FLEX}}}{(\text{NO. OF INTEGRATED VARIABLES})_{\text{RIGID}}} \right)^{1.4}$$

#### 4. SUBROUTINE DESCRIPTIONS

A description of all subroutines added to the original version of the TOLA computer program is included in this section. Also, those existing equations that were modified to include flexibility effects are shown. The executive subroutine of the flexible body option is FLEX1. This routine contains calls to the other subroutines associated with the option, and as a group, formulates and solves the equations of motion for points on the flexible airframe.

4.1 FLEX1 - Subroutine FLEX1 formulates a maximum of twenty coupled, second order differential equations, and through matrix manipulation, solves the following set of simultaneous linear equations:

$$[A] \{ \ddot{q} \} = \{ B \} \quad (4-1)$$

The coefficient matrix  $[A]$  is a function of the generalized mass corresponding to each mode, the mode shape defined at each strut attach point, and the strut masses. The matrix  $B$  is a function of all external forces and terms considered as forces during each time increment. The independent variables  $\{ \ddot{q} \}$  are the second derivative of the generalized coordinates with respect to time.

The overall subroutine is divided into several entry points with each entry performing the function described below:

FLEX1 establishes data blocks and array sizes and initializes variables.

FLEX2 computes those components of matrices  $[A]$  and  $\{ B \}$  that are time invariant and determines the initial generalized displacements.

FLEX3 computes the time varying components of matrix  $\{ B \}$  and formulates the simultaneous linear equations as a function of  $\ddot{q}$ .

FLEX4 is null.

FLEX5 is null.

FLEX6 formulates and prints the output data generated by the flexible body option.

FLEX7 transfers time dependent variables to and from the integration routine.

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4.2 DECOMP - Subroutine DECOMP is part of a package that solves the set of simultaneous equations defined in equation (4-1). DECOMP manipulates the coefficient matrix [A] into upper and lower triangular form which, combined with subroutine SOLVE, eliminates the need for a matrix inverse routine. Subroutine DECOMP is called from ENTRY FLEX2.

4.3 SOLVE - Subroutine SOLVE determines the values of  $\{\ddot{q}\}$  based on the upper and lower triangular coefficient matrix calculated in DECOMP and the matrix  $\{B\}$  determined in FLEX3. Subroutine SOLVE is called from ENTRY FLEX3.

4.4 SING - Subroutine SING prints error diagnostics and terminates the program if subroutine DECOMP cannot properly transform the coefficient matrix [A] into upper and lower triangular form. SING is called from DECOMP.

4.5 Matrix Subroutines - The subroutines that follow are standard CDC library matrix routines that are included with the option to make the program independent of any machine library shortcomings or limitations. All of these routines are called from ENTRY FLEX2 or ENTRY FLEX3.

ARRAY - Subroutine ARRAY converts a data array from single to double dimension. The CDC library title for this routine (ARRAY) was changed since there was an existing TOLA subroutine by that name.

CTIE - Subroutine CTIE adjoins two matrices by columns.

LOC - Subroutine LOC computes a vector subscript for an element in a matrix of specified storage mode.

GTPRD - Subroutine GTPRD gives the transpose product of two general matrices.

GMSUB - Subroutine GMSUB will subtract two general matrices.

GMADD - Subroutine GMADD adds two general matrices.

GMPRD - Subroutine GMPRD computes the product of two general matrices.

4.6 Modifications to Existing TOLA Equations - Existing TOLA equations were modified to include the effects of flexibility on landing gear displacements, velocities and accelerations. The three components of the strut attach point position vectors,  $R_{AX}$ ,  $R_{AY}$ ,  $R_{AZ}$ , were revised to include the generalized flexible displacement as follows:

$$\begin{Bmatrix} R_{AX} \\ R_{AY} \\ R_{AZ} \end{Bmatrix} = \begin{Bmatrix} R_{AX} \\ R_{AY} \\ R_{AZ} \end{Bmatrix} + \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix} \begin{Bmatrix} \sum_{n=1}^N \phi_{xn}^k q_n \\ \sum_{n=1}^N \phi_{yn}^k q_n \\ \sum_{n=1}^N \phi_{zn}^k q_n \end{Bmatrix} \quad (4-2)$$

where  $l_1$ ,  $m_1$ , and  $n_1$  transform the displacements from inertial axes to body axes systems.

The changes in the strut velocity equations resulted from introducing the generalized flexible velocity  $\dot{q}$ . As rewritten, the components of the strut attach point velocity vector are as follows:

$$\begin{aligned} R_{DX} &= R_{DX} + \left( q \sum_{n=1}^N \phi_{zn}^k - r \sum_{n=1}^N \phi_{yn}^k \right) q_n + \sum_{n=1}^N \phi_{xn}^k \dot{q}_n \\ R_{DY} &= R_{DY} + \left( r \sum_{n=1}^N \phi_{xn}^k - p \sum_{n=1}^N \phi_{zn}^k \right) q_n + \sum_{n=1}^N \phi_{yn}^k \dot{q}_n \\ R_{DZ} &= R_{DZ} + \left( p \sum_{n=1}^N \phi_{yn}^k - q \sum_{n=1}^N \phi_{xn}^k \right) q_n + \sum_{n=1}^N \phi_{zn}^k \dot{q}_n \end{aligned} \quad (4-3)$$

where  $p$ ,  $q$ , and  $r$  are the rigid body roll, pitch and yaw rates respectively.

Similarly, the strut acceleration equations are modified by incorporating the generalized flexible acceleration  $\ddot{q}$ . The revised equation then takes on the form

$$\ddot{S} = \ddot{S} + a_{k31} \sum_{n=1}^N \phi_{xn}^k \ddot{q}_n + a_{k33} \sum_{n=1}^N \phi_{zn}^k \ddot{q}_n \quad (4-4)$$

All of these modifications to the landing gear equations were made in subroutine LGEA3C.

The forces and moments resulting from landing gear flexibility were incorporated into the rigid body equations as shown below.



$$F_X = F_X - \sum_{n=1}^N \sum_{k=1}^K m_k \phi_{xn}^k \eta_n$$

$$F_Y = F_Y - \sum_{n=1}^N \sum_{k=1}^K m_k \phi_{yn}^k \eta_n$$

$$F_Z = F_Z - \sum_{n=1}^N \sum_{k=1}^K m_k \phi_{zn}^k \eta_n$$

$$L = L - \sum_{n=1}^N \sum_{k=1}^K m_k \{ R_{ksy} \phi_{zn}^k - [R_{ksz} + a_{k11} (r_{Fk} - S_{kc})] \phi_{yn}^k \} \eta_n \quad (4-5)$$

$$M = M - \sum_{n=1}^N \sum_{k=1}^K m_k \{ [R_{ksz} + a_{k11} (r_{Fk} - S_{kc})] \phi_{xn}^k - [R_{ksx} - a_{k13} (r_{Fk} - S_{kc})] \phi_{zn}^k \} \eta_n$$

$$N = N - \sum_{n=1}^N \sum_{k=1}^K m_k \{ -R_{ksy} \phi_{xn}^k + [R_{ksx} - a_{k13} (r_{Fk} - S_{kc})] \phi_{yn}^k \} \eta_n$$

These additions were made in subroutine LGEAR1.

## 5. FLOW LOGIC FOR FLEXIBLE BODY OPTION

Subroutine FLEX1 employs a matrix approach to formulate and solve the flexible body equations of motion. These equations are given as

$$\begin{aligned}
 & \left[ m_s \right] \left\{ \ddot{q}_s \right\} + \left[ \omega_s^2 \quad m_s \right] \left\{ q_s \right\} \\
 & + \left[ \left[ \phi_{xs}^k \right]^T \left[ m_k \right] \left[ \phi_{xn}^k \right] + \left[ \phi_{ys}^k \right]^T \left[ m_k \right] \left[ \phi_{yn}^k \right] + \left[ \phi_{zs}^k \right]^T \left[ m_k \right] \left[ \phi_{zn}^k \right] \right] \left\{ \ddot{q}_n \right\} \\
 & + \left[ \left[ \phi_{xs}^k \right]^T \left[ \phi_{ys}^k \right]^T \left[ \phi_{zs}^k \right]^T \right] \begin{bmatrix} \left\{ m_k \right\} & 0 & 0 \\ 0 & \left\{ m_k \right\} & 0 \\ 0 & 0 & \left\{ m_k \right\} \end{bmatrix} \begin{bmatrix} \ddot{X} \\ \ddot{Y} \\ \ddot{Z} \end{bmatrix} - \begin{bmatrix} a_{k31} \\ 0 \\ a_{k33} \end{bmatrix} \left\{ \ddot{s}_k \right\} \right] \\
 & + \left( \left[ \phi_{zs}^k \right]^T \left[ R_{ksy} \right] - \left[ \phi_{ys}^k \right]^T \left[ R_{ksz} \right] + \left[ r_{Fk} - s_{kc} \right] \left[ a_{k11} \right] \right) \left\{ \dot{\omega}_x m_k \right\} \\
 & + \left( \left[ \phi_{xs}^k \right]^T \left[ R_{ksz} \right] + \left[ r_{Fk} - s_{kc} \right] \left[ a_{k11} \right] - \left[ \phi_{zs}^k \right]^T \left[ R_{ksx} \right] - \left[ r_{Fk} - s_{kc} \right] \right. \\
 & \quad \left. \left[ a_{k13} \right] \right) \left\{ \dot{\omega}_y m_k \right\} \\
 & + \left( \left[ \phi_{ys}^k \right]^T \left[ R_{ksx} \right] - \left[ r_{Fk} - s_{kc} \right] \left[ a_{k13} \right] - \left[ \phi_{xs}^k \right]^T \left[ R_{ksy} \right] \right) \left\{ \dot{\omega}_z m_k \right\} = \left\{ Q_s \right\} \quad (5-1)
 \end{aligned}$$

Definition of these symbols with their program variable names are given in Figure 5-1.

Many of the terms in Equation (5-1) are constant and need be calculated only in the initial call to subroutine FLEX1 after the option has been staged into the program. Rewriting this equation in a shorthand matrix form that separates the constant terms from the time dependent variables yields

$$\begin{aligned}
 & [M] \left\{ \ddot{q} \right\} + [K] \left\{ q \right\} + [GFORC1] \begin{bmatrix} \ddot{X} - a_{k31} \ddot{s}_k \\ \ddot{Y} \\ \ddot{Z} - a_{k33} \ddot{s}_k \end{bmatrix} + [GFORC2] \left\{ \dot{\omega}_x m_k \right\} \\
 & + [GFORC3] \left\{ \dot{\omega}_y m_k \right\} + [GFORC4] \left\{ \dot{\omega}_z m_k \right\} = \left\{ Q_s \right\} \quad (5-2)
 \end{aligned}$$

A comparison of Equations (5-1) and (5-2) will aid in determining which terms are included in each of the shorthand matrix expressions.

Each matrix in Equation (5-2) is formulated in a particular section or entry of subroutine FLEX1. The subroutine further manipulates the equation

into a set of linear, simultaneous equations with  $\ddot{q}$  as the independent variable.

$$[M] \{\ddot{q}\} = \{B\} \quad (5-3)$$

This set of equations is then solved for  $\ddot{q}$ .

The flow diagrams that follow indicate the sequential approach used to formulate the components of the flexible body equations of motion and the subsequent solution of these equations. A section of subroutine coding is listed preceded by an explanation of the function of that section. The notation used in the coding is given in Figure (5-1).

A complete listing of the modified TOLA computer program with the flexible body option is given in Appendix A.

$m_s$ GMASS1	GENERALIZED MASS OF $s^{th}$ MODE
$\omega_s$ GFREQ	NATURAL FREQUENCY OF $s^{th}$ MODE
$Q_{xs}^k, Q_{ys}^k, Q_{zs}^k$ SXMOD, SYMOD, SZMOD	X, Y, Z COMPONENTS OF THE MODAL DEFLECTIONS FOR THE $k^{th}$ STRUT ATTACH POINT
$m_k$ SMASS	MASS OF $k^{th}$ STRUT
$\ddot{X}, \ddot{Y}, \ddot{Z}$	RIGID BODY TRANSLATIONAL ACCELERATIONS
$a_{k11}, a_{k13}, a_{k31}, a_{k33}$ A11, A13, A31, A33	DIRECTION COSINES RELATING STRUT COORDINATE SYSTEM TO BODY COORDINATE SYSTEM
$\ddot{S}_k$ SDD	ACCELERATION OF $k^{th}$ STRUT
$R_{ksx}, R_{ksy}, R_{ksz}$	X, Y, Z COMPONENTS OF STRUT ATTACH POINT POSITION VECTOR
$r_{Fk}$	DISTANCE FROM STRUT ATTACH POINT TO EXTENDED POSITION OF AXLE
$S_{kc}$	DISTANCE FROM STRUT AXLE TO STRUT CENTER OF MASS
$\dot{\omega}_x, \dot{\omega}_y, \dot{\omega}_z$	RIGID BODY ANGULAR ACCELERATIONS
$Q_s$	GENERALIZED FORCES

FIGURE 5-1 DEFINITION OF SYMBOLS

# ENTRY FLEX1

## ESTABLISH COMMON REGION AND DIMENSION LOCAL ARRAYS

```

COMMON/DIRCOM/SKIPUP,DUD(7),AMINER,DM1(13),AA77P,DM2(81),ALA77F,
*DM3(35),AMA77F,DM4(9),ANA77F,ANA77P,DM5(12),AX77F,DM6,AY77F,
*DM7(2),AZ77F,DM8(81),YA77P,DM9(188),PI77R,DM10,PI77R1,DM11(5),
*QI77R,DM12,QI77R1,DM13(5),RI77R,DM14,RI77R1,DM15(15),
*U777F,DM16(19),V777F,DM17(3),W777F,DM18(93),NSTRU,
*MASS(5),RX(5),RY(5),RZ(5),DM19(32),RF(5),DM20(97),SD21(2),
*SD22(2),SD23(2),SD24(2),SD25(2),DM21(99),IN,DM22(153),
*INDLG,DM23(151),INDFLX,NMODE,GMASS1(20),GFREQ(20),
*SXMOD(100),SYM00(100),SZMOD(100),SKC(5),TXMOD(30),
*DCMODE(60),ARMCDE(120),NPTS,OUTMOD(120),ROIS(60),
*PF(120),GU(20),GQD1(20),GQD2(20),DDM24(20),
COMMON/FLXOP/GFORC2(100),GFORC3(100),GFORC4(100),
*T(5),FCX,FCY,FCZ,XU2F(20),XU2T(20),YU2F(20),YU2T(20),ZU2F(20),
*ZU2T(20),XD1F(20),XD1T(20),YD1F(20),YD1T(20),ZD1F(20),ZD1T(20),
*XU5F(20),YU5F(20),ZU5F(20),
COMMON/LGE/A11(5),A13(5),A31(5),A33(5),DM24(279)
COMMON/HTCOM/HT,DDMH(2)
REAL MASS
DIMENSION GMASS(400),SMASS(25),GS400(400),COPMAS(20,20),
*QS(20),QS1(20),GFORC1(60),DIFF(5),RZA11(25),RXA13(25),RKSY(25),
*SD0(10),VARY1(3),OMXD1M(5),OMYD1M(5),OMZD1M(5),GF(20),FDC(3),
*CTMP1(120),GTF(20),SU(3),SD1(3),SD2(3),TITL(16),LA(40),
*COEF(20,20)
EQUIVALENCE (SD21(1),SD0(1))
DATA HDR/5H FLEX/, (TITL(I),I=1,16)/5HPOINT,4HXD2F,4HXD2T,4HYD2F,
*4HYD2T,4HZD2F,4HZD2T,4HXD1F,4HXD1T,4HYD1F,4HYD1T,4HZD1F,
*4HZD1T,4HXD1F,4HYD1F,4HZD1F/

```

## INITIALIZE VARIABLES

```

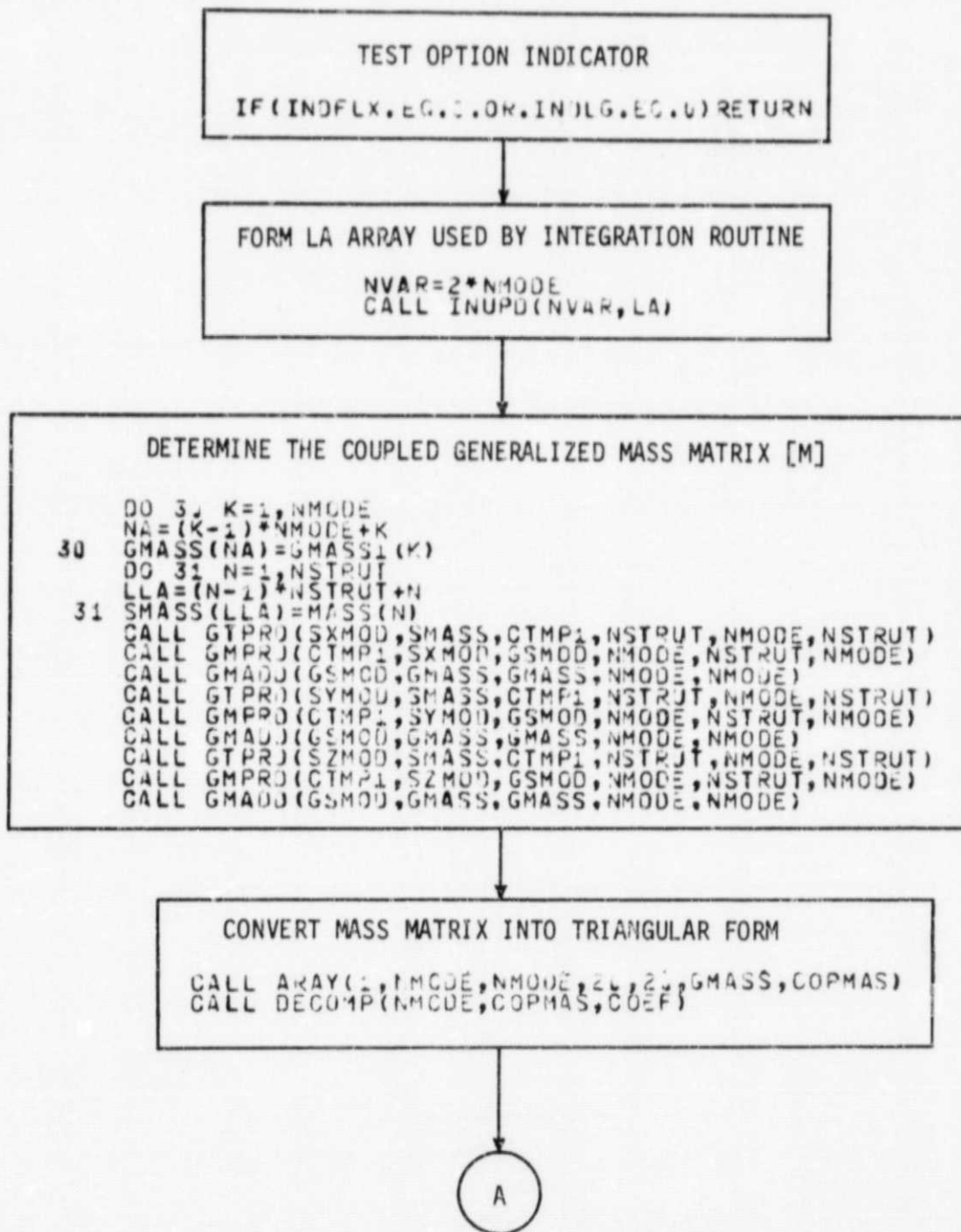
DO 1 I=1,400
1  GMASS(I)=0.
DO 2 I=1,25
2  SMASS(I)=0.
RZA11(I)=0.
RXA13(I)=0.
DO 15 I=1,40
15 LA(I)=0
NMODE=1

```

RETURN

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ENTRY FLEX2



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A

# FORM MATRICES GFORC1, GFORC2, GFORC3, GFORC4

```

CALL GTPRO(SXMOD, MASS, QS, NSTRUT, NMODE, 1)
CALL GTPRO(SYMOD, MASS, QS1, NSTRUT, NMODE, 1)
CALL CTIE(QS, QS1, CTMP1, NMODE, 1, 0, 0, 1)
CALL GTPRO(SZMOD, MASS, QS, NSTRUT, NMODE, 1)
CALL CTIE(CTMP1, QS, GFORC1, NMODE, 2, 0, 0, 1)
DO 33 L=1, NSTRUT
DIFF(L)=RF(L)-SKC(L)
MA=(L-1)*NSTRUT+L
RZA11(MA)=RZ(L)+DIFF(L)*A11(L)
RXA13(MA)=RX(L)-DIFF(L)*A13(L)
33 RKSY(MA)=RY(L)
CALL GTPRO(SZMOD, RKSY, CTMP1, NSTRUT, NMODE, NSTRUT)
CALL GTPRO(SYMOD, RZA11, GSMOD, NSTRUT, NMODE, NSTRUT)
CALL GMSUB(CTMP1, GSMOD, GFORC2, NMODE, NSTRUT)
CALL GTPRO(SXMOD, RZA11, CTMP1, NSTRUT, NMODE, NSTRUT)
CALL GTPRO(SZMOD, PXA13, GSMOD, NSTRUT, NMODE, NSTRUT)
CALL GMSUB(CTMP1, GSMOD, GFORC3, NMODE, NSTRUT)
CALL GTPRO(SYMOD, RXA13, CTMP1, NSTRUT, NMODE, NSTRUT)
CALL GTPRO(SXMOD, RKSY, GSMOD, NSTRUT, NMODE, NSTRUT)
CALL GMSUB(CTMP1, GSMOD, GFORC4, NMODE, NSTRUT)

```

## DETERMINE INITIAL DISPLACEMENTS

```

SUM1=0.
SUM3=0.
DO 34 I=1, NSTRUT
SUM1=SUM1+A31(I)*SDD((I-1)*2+1)
34 SUM3=SUM3+A33(I)*SDD((I-1)*2+1)
VARY1(1)=AX77F-SUM1
VARY1(2)=AY77F
VARY1(3)=AZ77F-SUM3
CALL GMPRO(GFORC1, VARY1, QS, NMODE, 3, 1)
DO 35 I=1, NSTRUT
OMXD1M(I)=PI77R1*MASS(I)
OMYD1M(I)=QI77R1*MASS(I)
35 OMZD1M(I)=RI77R1*MASS(I)
CALL GMPRO(GFORC2, OMXD1M, GF, NMODE, NSTRUT, 1)
CALL GMAO(QS, GF, QS, NMODE, 1)
CALL GMPRO(GFORC3, OMYD1M, GF, NMODE, NSTRUT, 1)
CALL GMAO(QS, GF, QS, NMODE, 1)
CALL GMPRO(GFORC4, OMZD1M, GF, NMODE, NSTRUT, 1)
CALL GMAO(QS, GF, QS, NMODE, 1)

```

B



B

```

CALL GTPRO(TXMOD,T,GF,IN,NMODE,1)
CALL GMSUB(GF,QS,QS,NMODE,1)
FDC(1)=FCX
FDC(2)=FCY
FDC(3)=FCZ
CALL GTPRO(DCMODE,FDC,GF,3,NMODE,1)
CALL GMAUD(GF,QS,QS,NMODE,1)
DO 36 I=1,NMODE
  NN=(I-1)*6+1
  CTMP1(NN)=-ARMODE(NN)*AA77P
  CTMP1(NN+1)=ARMODE(NN+1)*YA77P
  CTMP1(NN+2)=-ARMODE(NN+2)*ANA77P
  CTMP1(NN+3)=ARMODE(NN+3)*ALA77F
  CTMP1(NN+4)=ARMODE(NN+4)*AMA77F
36  CTMP1(NN+5)=ARMODE(NN+5)*ANA77F
DO 37 II=1,NMODE
  GF(II)=.
DO 37 JJ=1,6
  MJ=(II-1)*6+JJ
37  GF(II)=GF(II)+CTMP1(MJ)*PF(MJ)
  CALL GMAUD(GF,QS,QS,NMODE,1)
DO 38 IG=1,NMODE
  GTF(IG)=GMASS1(IG)*GFREQ(IG)**2.
38  GQ(IG)=QS(IG)/GTF(IG)

```

TRANSFER DISPLACEMENTS TO INTEGRATION ROUTINE

```

SKIPUP=.TRUE.
DO 39 I=1,NMODE
  N22=2*I
  CALL UPDAT(1,LA(N22),GQ(I),DU,DU,DU,DU)
39  CONTINUE
SKIPUP=.FALSE.
RETURN

```

RETURN



# ENTRY FLEX3

## TEST OPTION INDICATOR

IF (INDFLEX.EQ.0.OR.INDLG.EQ.0) RETURN

## FORM TIME DEPENDENT COMPONENTS OF GFORC1, GFORC2, GFORC3, GFORC4 PRODUCTS

```

SUM1=0.
SUM3=0.
DO 40 I=1,NSTRUT
SUM1=SUM1+A31(I)*SDD((I-1)*2+1)
40 SUM3=SUM3+A33(I)*SDD((I-1)*2+1)
VARY1(1)=AX77F-SUM1
VARY1(2)=AY77F
VARY1(3)=AZ77F-SUM3
CALL GMPRO(GFORC1,VARY1,GTF,NMODE,3,1)
DO 46 I=1,NMODE
46 QS(I)=0.
CALL GMSUB(QS,GTF,QS,NMODE,1)
DO 41 I=1,NSTRUT
OMXD1M(I)=PI77R1*MASS(I)
OMYD1M(I)=QI77R1*MASS(I)
41 OMZD1M(I)=RI77R1*MASS(I)

CALL GMPRO(GFORC2,OMXD1M,GTF,NMODE,NSTRUT,1)
CALL GMSUB(QS,GTF,QS,NMODE,1)
CALL GMPRO(GFORC3,OMYD1M,GTF,NMODE,NSTRUT,1)
CALL GMSUB(QS,GTF,QS,NMODE,1)
CALL GMPRO(GFORC4,OMZD1M,GTF,NMODE,NSTRUT,1)
CALL GMSUB(QS,GTF,QS,NMODE,1)

```

## CALCULATE GENERALIZED THRUST FORCES

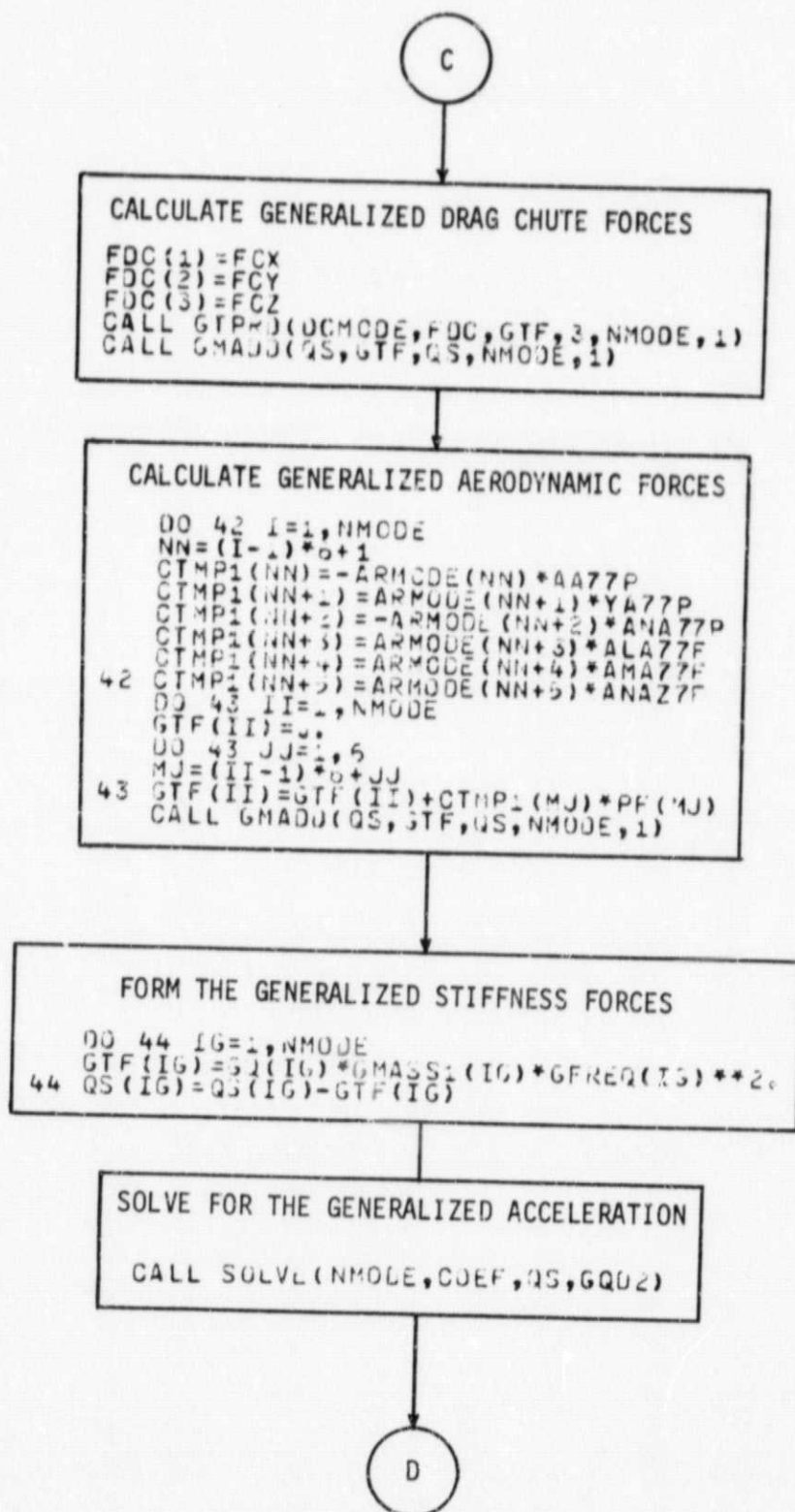
```

CALL GTPRO(TXMOD,T,GTF,IN,NMODE,1)
CALL GMADD(QS,GTF,QS,NMODE,1)

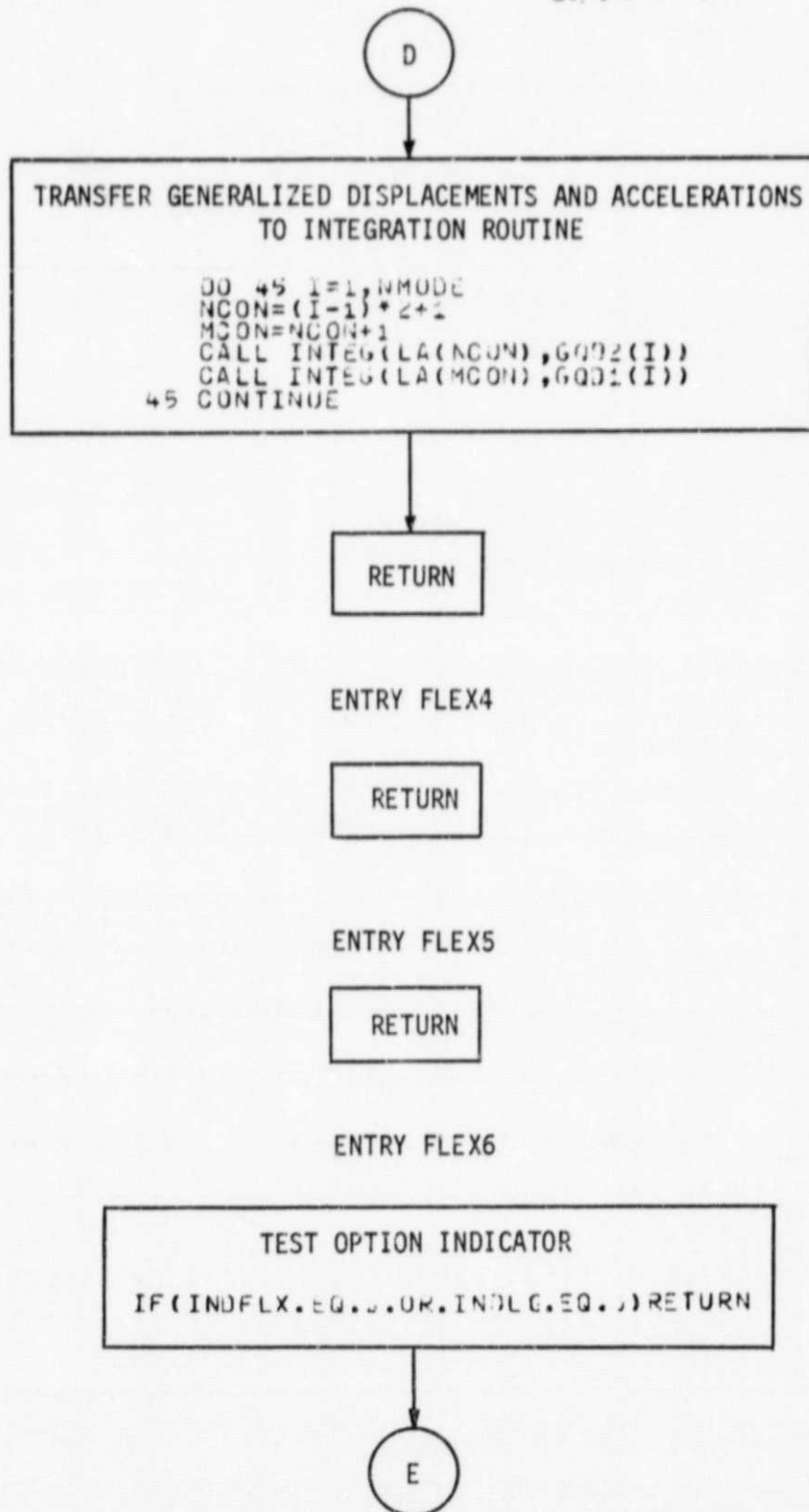
```

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E

TEST IF OUTPUT IS DESIRED  
IF (NPTS.EQ.L) RETURN

FORMULATE AND PRINT OUTPUT DATA

```

CALL STFL(,1,HOR)
CALL STFL(,16,TITL)
DO 52 I=1,NPTS
DO 61 K=1,3
SD1(K)=0.
SD2(K)=0.
DO 61 J=1,NMODE
NCON=((I-1)*3+K-1)*NMODE+J
SD1(K)=SD1(K)+OUTMOD(NCON)*GQ(J)
SD2(K)=SD2(K)+OUTMOD(NCON)*GQD1(J)
51 SD2(K)=SD2(K)+OUTMOD(NCON)*GQD2(J)
LX=(I-1)*3+1
LY=LX+1
LZ=LY+1
XD2F(I)=SD2(1)
XD2T(I)=AX77F+XD2F(I)+2.*(QI77R*SD1(3)-RI77R*SD1(2))+
*(PI77R*RI77R+QI77R1)*(ROIS(LZ)+SDJ(3))+(PI77R*RI77R
*-RI77R1)*(ROIS(LY)+SDJ(2))-(QI77R*QI77R+RI77R*RI77R)
* (ROIS(LX)+SDJ(1))
YD2F(I)=SD2(2)
YD2T(I)=AY77F+YD2F(I)+2.*(RI77R*SD1(1)-PI77R*SD1(3))+
*(QI77R*PI77R+RI77R1)*(ROIS(LX)+SDJ(1))+(QI77R*RI77R
*-PI77R1)*(ROIS(LZ)+SDJ(3))-(RI77R*RI77R+PI77R*PI77R)
* (ROIS(LY)+SDJ(2))
ZD2F(I)=SD2(3)
ZD2T(I)=AZ77F+ZD2F(I)+2.*(PI77R*SD1(2)-QI77R*SD1(1))+
*(RI77R*QI77R+PI77R1)*(ROIS(LY)+SDJ(2))+(RI77R*PI77R
*-QI77R1)*(ROIS(LX)+SDJ(1))-(PI77R*PI77R+QI77R*QI77R)
* (ROIS(LZ)+SDJ(3))
XD1F(I)=SD1(1)
XD1T(I)=U777F+XD1F(I)+QI77R*(ROIS(LZ)+SDJ(3))-RI77R*
*(ROIS(LY)+SDJ(2))
YD1F(I)=SD1(2)
YD1T(I)=V777F+YD1F(I)+RI77R*(ROIS(LX)+SDJ(1))-PI77R*
*(ROIS(LZ)+SDJ(3))
ZD1F(I)=SD1(3)
ZD1T(I)=W777F+ZD1F(I)+PI77R*(ROIS(LY)+SDJ(2))-QI77R*
*(ROIS(LX)+SDJ(1))
XDJF(I)=SDJ(1)
YDJF(I)=SDJ(2)
ZDJF(I)=SDJ(3)
PTN=FLOAT(I)
CALL STOVAR(8,PTN,XD2F(I),XD2T(I),YD2F(I),YD2T(I),ZD2F(I),
*ZD2T(I),XDJF(I))
CALL STOVAR(8,XD1T(I),YD1F(I),YD1T(I),ZD1F(I),ZD1T(I),XDJF(I),
*YDJF(I),ZDJF(I))
62 CONTINUE

```

RETURN

ENTRY FLEX7

TEST OPTION INDICATOR

IF (INDFLX.EQ.0,OR,INDLG.EQ.0) RETURN

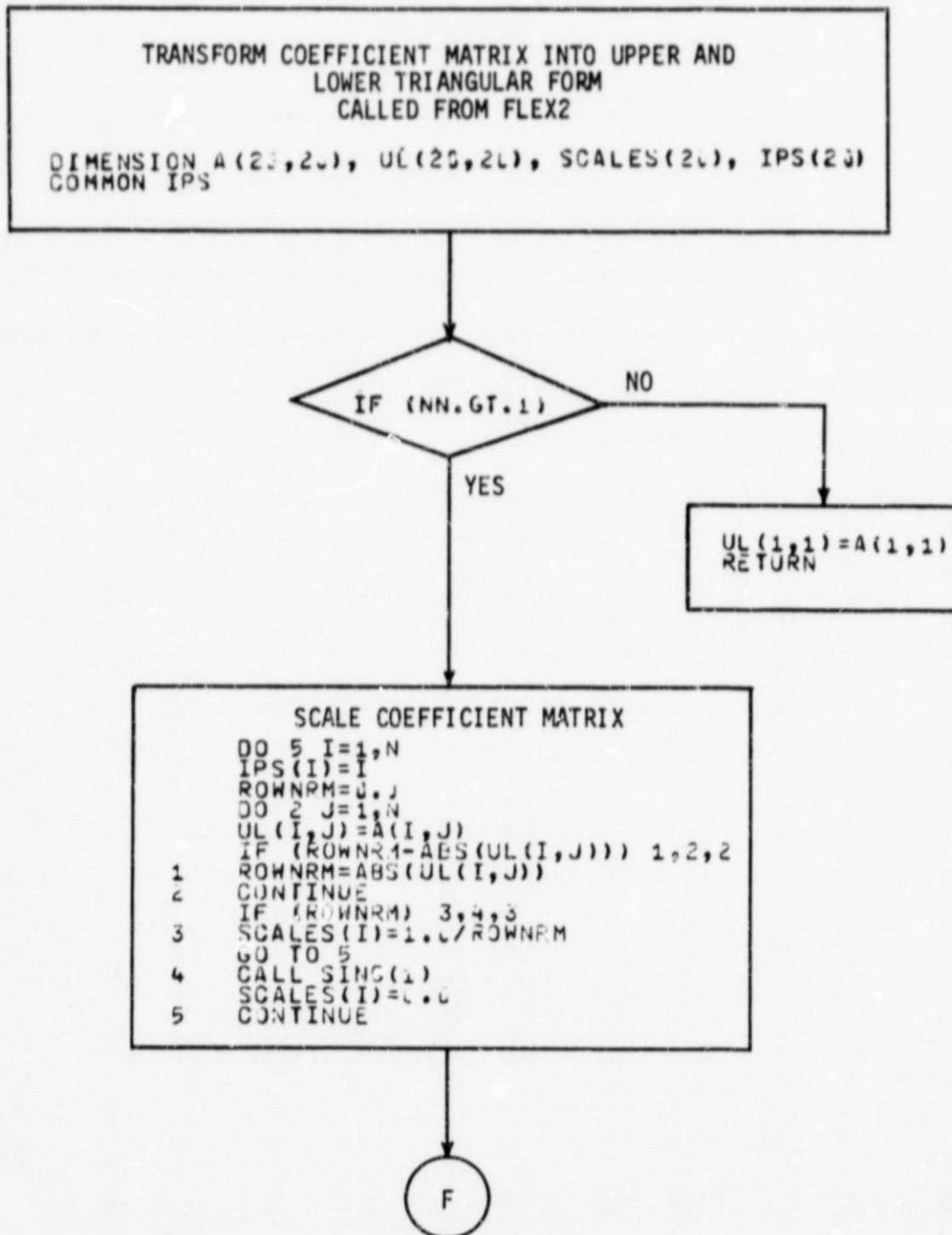
TRANSFER VARIABLES TO AND FROM  
INTEGRATION ROUTINE

```
RVAR=2.*FLOAT(NMODL)/4.  
K=IFIX(RVAR)  
IF (K.EQ.0) GO TO 71  
DO 70 I=1,K  
  N=4*I-3  
  MD1=2*I-1  
  MD0=2*I  
  CALL UPDAT(4,LA(N),GQ01(MD1),GQ(MD1),GQ01(MD0),GQ(MD0),DU)  
70 CONTINUE  
  L=2*K  
  IF(L.EQ.NMODE) RETURN  
71 M=4*K+1  
  MP=2*K+1  
  CALL UPDAT(2,LA(M),GQ01(MP),GQ(MP),DU,DU,DU)
```

RETURN

END

# SUBROUTINE DECOMP





# FORMULATE UPPER AND LOWER MATRICES

```

NM1=N-1
DO 17 K=1,NM1
BIG=0
DO 11 I=K,N
IP=IPS(I)
SIZE=ABS(UL(IP,K))*SCALES(IP)
IF (SIZE-BIG) 11,11,1
10 BIG=SIZE
IDXPIV=I
11 CONTINUE
IF (BIG) 12,12,13
12 CALL SING(2)
GO TO 17
13 IF (IDXPIV-K) 14,15,14
14 J=IPS(K)
IPS(K)=IPS(IDXPIV)
IPS(IDXPIV)=J
15 KP=IPS(K)
PIVOT=UL(KP,K)
KP1=K+1
DO 16 I=KP1,N
IP=IPS(I)
EM=-UL(IP,K)/PIVOT
UL(IP,K)=-EM
DO 16 J=KP1,N
UL(IP,J)=UL(IP,J)+EM*UL(KP,J)
16 CONTINUE
17 CONTINUE
KP=IPS(N)
IF (UL(KP,N)) 19,18,14
18 CALL SING(2)

```

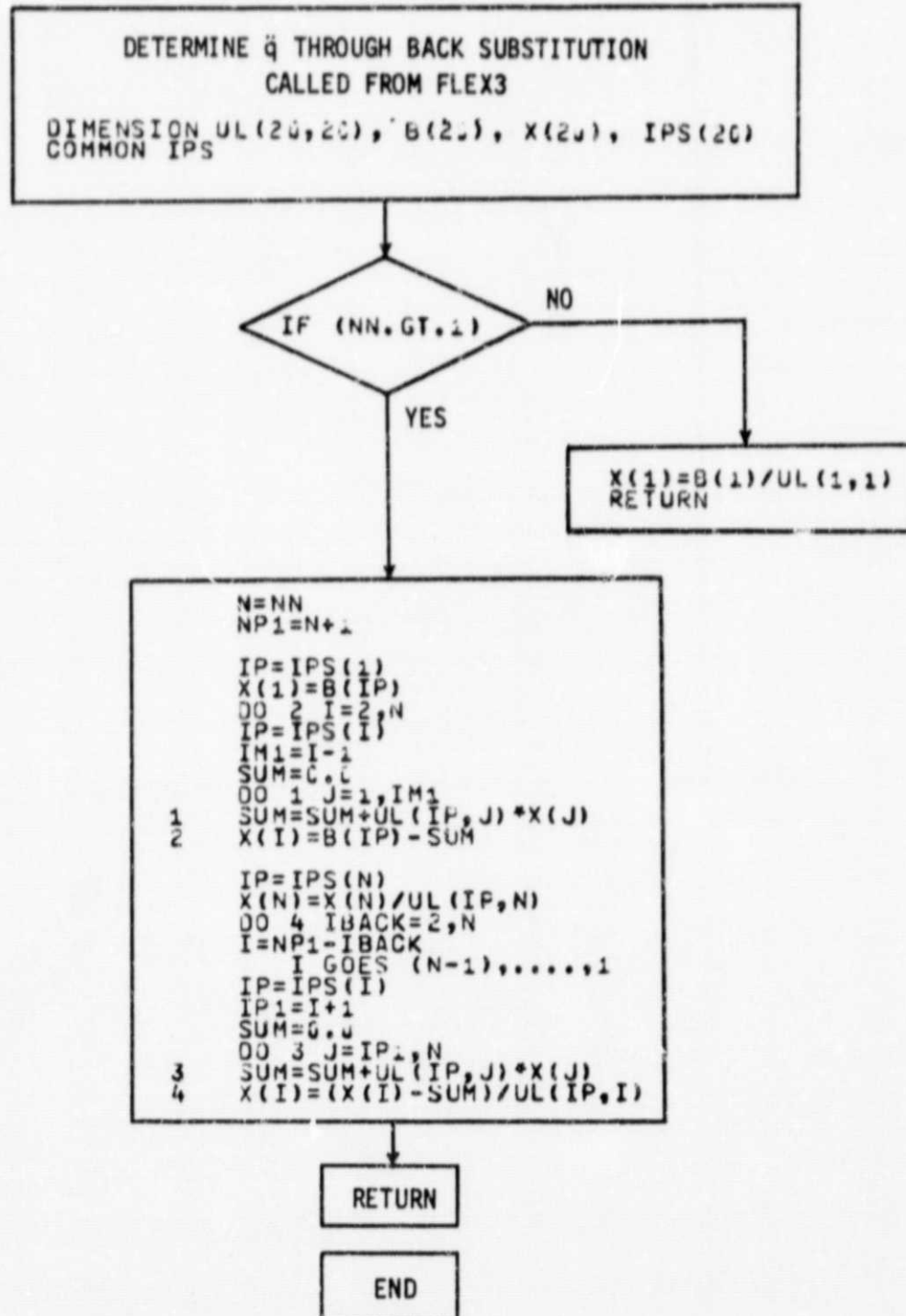
RETURN

END

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# SUBROUTINE SOLVE



# SUBROUTINE SING

PRINT DIAGNOSTICS AND TERMINATE PROGRAM IF  
COEFFICIENT MATRIX IS ILL-CONDITIONED  
CALLED FROM DECOMP

```
11  FORMAT(54H,MATRIX WITH ZERO ROW IN DECMFOSE.      )  
12  FORMAT(54H,SINGULAR MATRIX IN DECMFOSE. ZERO DIVIDE IN SOLVE.  )  
    NOUT=6  
    NOUT=STANDARD OUTPUT UNIT  
    GO TO (1,2),IWHY  
1   WRITE (NOUT,11)  
    GO TO 1  
2   WRITE (NOUT,12)  
10  CALL EXERR(0)
```

RETURN

END

## 6. EXAMPLES

This section provides two examples illustrating the modified TOLA computer program input and results. It is intended to show actual program operation with emphasis placed on properly interpreting and incorporating flexible body data. Each example consists of a brief explanation with a listing of all input data and sample output given in the appendix section. Input data for both cases were supplied by the NASA Langley Research Center.

**6.1 Rigid Body Example** - This case demonstrates how to exercise the modified TOLA computer program without including the effects of flexibility. All the data defined in Reference 1 for a rigid body case are required. As can be seen in the input data listing of Appendix D, setting the indicator INDFLX to zero is the only flexible body data required when running a rigid body case.

**6.2 Flexible Body Example** - This case demonstrates how to incorporate the effects of flexibility in a takeoff or landing analysis through the use of the flexible body option. All modal data required by the option was supplied by NASA and are shown in Figure 6-1. These data consist of a modal frequency, generalized mass, and modal deflections for sixteen free-free normal modes.

Several observations can be made that help in interpreting program input and results. Only modal deflections in the vertical (Z) direction are given, consequently, there is no flexible body response in the X and Y direction. In addition, the mode shapes defined by the deflections are all symmetric from wing tip to wing tip. This results in a symmetric landing (simultaneous main gear touchdown) since all the rigid body rigid body data are also symmetric.

The first four modes shown in Figure 6-1 were used to represent airframe elasticity. Referring to the input data listing in Appendix E, the flexible body option indicator is set equal to one. Each modal frequency and generalized mass are placed in arrays GFREQ and GMASS1 respectively. The vertical deflections for each landing gear attach point are in SZMOD. Since there are no other landing gear data, SXMOD and SYMOD are not input. Modal data for the aerodynamic reference point are contained in ARMODE. Aerodynamic weighting factors were calculated using the procedure outlined in Appendix B assuming an elliptical spanwise lift distribution over the aircraft's wing. These factors are in array PF. Engine attach point modal data in the X direction are assumed zero; therefore, TXMODE is not input. Flexible body responses are output for four points

MODE NUMBER	MODAL FREQ HZ	MODAL MASS SLUGS	NORMALIZED MODAL DATA - POSITIVE DOWN						
			PILOT STA.	NOSE GEAR	AERO DEF	AERO SLOPE	MAIN GEARS	ENGINE	TAIL
1	2.099	66.6617	+ .1970	+ .0800	- .1140	-4.239E-4	- .1000	- .0400	+ .2030
2	2.628	79.4557	- .0385	- .0200	- .0414	3.643E-4	- .0042	+ .1885	- .2440
3	4.784	70.8341	+ .0035	- .1530	+ .0405	-6.03E-4	+ .1393	+ .1380	- .1072
4	6.907	18.1131	+ .0035	- .0650	+ .0644	-3.034E-5	+ .0112	- .0510	- .1250
5	7.671	20.0656	+ .0254	+ .0400	- .0342	-5.653E-5	- .0087	+ .0111	+ .1998
6	9.728	99.7316	+ .3028	+ .1850	- .0054	-1.351E-1	+ .1200	+ .0559	- .4409
7	11.797	70.4027	- .1673	- .0100	- .1258	3.716E-4	+ .1050	+ .0588	- .0165
8	13.878	31.6212	- .1157	+ .0500	- .0323	-9.602E-4	- .0100	+ .0350	- .2167
9	15.552	40.4199	+ .0494	- .0300	- .0036	7.309E-4	+ .0500	+ .1025	+ .2985
10	17.638	12.1885	- .0038	+ .0050	- .0044	8.596E-7	+ .0500	+ .0100	+ .0982
11	20.019	27.2611	+ .0370	- .0500	- .0814	5.78E-4	- .0870	- .0200	- .3728
12	21.099	25.7565	+ .0181	- .0350	- .0653	2.801E-4	+ .0200	+ .0075	- .0837
13	23.396	37.8456	+ .0135	- .0500	+ .0085	1.617E-4	.0000	+ .0400	- .1269
14	23.969	39.6848	- .0180	+ .0400	- .0009	-1.503E-4	+ .0350	+ .0250	- .2163
15	25.637	29.5837	- .0072	+ .0150	+ .0174	-1.417E-4	- .1300	- .0300	+ .2243
16	25.694	8.2589	- .0023	+ .0075	+ .0044	-4.213E-5	- .0320	+ .0050	+ .0670

PILOT STATION X = 42.6667  
 NOSE GEAR X = 35.08333  
 MAIN GEARS X = -2.83867  
               Y =  $\pm$ 8.3333  
               Z = 0.509583

ENGINES X = -5.4722  
           Y =  $\pm$ 14.1667  
 TAIL X = -32.333

FIGURE 6-1 FLEXIBLE BODY DATA

on the aircraft, the pilot station, nose gear, right main gear, and tail. Modal data for these points are in OUTMOD and, their position vectors are defined in ROIS.

Sample output for this run follows the input listing.

#### 7. REFERENCES

1. Lynch, Urban H. D., and Dueweke, John J., "Takeoff and Landing Analysis Computer Program (TOLA); Part III - User's Manual," Air Force Flight Dynamics Laboratory Technical Report AFFDL-TR-71-155, April 1974.
2. Young, Fay O., and Dueweke, John J., "Takeoff and Landing Analysis Computer Program (TOLA); Part IV - Programmer's Manual," Air Force Flight Dynamics Laboratory Technical Report AFFDL-TR-71-155, January 1975.
3. Dick, J. W., and Benda, B. J., "Addition of Flexible Body Option to the TOLA Computer Program, Part I - Final Report", NASA CR-132732, October 1975.

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APPENDIX A

PROGRAM LISTING - TOLA COMPUTER PROGRAM  
WITH FLEXIBLE BODY OPTION



```

OVERLAY(TOLA,0,0)
PROGRAM TOLA(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT,
1TAP=13,TAPE16,TAPE21)
COMMON/TABDIR/TABLE(8,0)
COMMON/REAU1/DM1(64),JBC,INXQ
CALL FTN3IN(1,J,DUMMY)
REWIND 13
C READ SUBROUTINE INITIALIZATION
JBC=-1
INXQ=1
1 CALL EXE
GO TO 1
END
C SUBROUTINE EXE
EXECUTIVE PROGRAM
DIMENSION INTND(1)
LOGICAL INDAWC, END, SKIPUP
LOGICAL STSWCH, TAUSTP
COMMON /STOPIT/ STSWCH, TAUSTP
COMMON /DIRCOM/
* SKIPUP, H, T, TIMINT, DM1(4)
* AMI, IER, AMAXER, DM2(7), AINGRS(4), DM4(46), TIMER, DM3(64),
* RELE1, DM7(5), RELE2, DM2(7), AINGRS(4), DM4(46), TIMER, DM3(64),
* AMAXH, DM1(180), DECRES(4),
* DM13 ( 8), DELTS, DM14 ( 6), ULH1, DM15 ( 4),
* DLTM1, DLTM2, DLTM3, DM16(18), EPS1, DM8,
* EPS11, DM21, EPS13, DM22 ( 12), EPS25
* DM23, EPS3, DM24,
* EPS7, DM26, EPS9, DM27 ( 25), GREFF
* DM28(17), HGC7F, DM29(44),
* INDAWC, DM31 ( 2), INDAWC, DM32
* INDAWC, INDAUT, DM33(123), INOPSK, DM38(34)
COMMON /DIRCOM/
* INDSKP, DM4, INDSKE, INDSF, INDSIG
* DM42 ( 2), INDSR, INDSY, DM42, INDSF
* DM43, INDSR, DM44 ( 9),
* NSTAGE, DM46 ( 3), DMGPR, DM47 ( 63), REP ( 30),
* RE77F, DM48 ( 28), RP77F, DM50 ( 14),
* DM51(6), SIGN, DM52(66), TIME, DM9(2),
* TIMES, DM52 ( 3), TIMES, DM56, TL1
* TL1, TL12, TL13, DM57 (127),
* PRINT, DM58 ( 6), STGVAR( 2), DM59 ( 13),
* DM60(277), NSTRT, DM61(89), IL, DM62(215), ALPOES, DM61(111),
* INDLG, DM1(151), DM1(151),
COMMON/TAUSTP/COMMON(11)
COMMON/EXLAUT/400DM1, SW1, TIME1, ALPOD1, DUMH1(5)
COMMON/LG/DM1(7)
COMMON/AUTSC/DM4(4)
COMMON/AUTSPC/DM5(5)
COMMON/LG/AUTS/DM6(14)
COMMON/FLXOP/DM1(6)
COMMON/AUTSAC/ALPJR1, QDESR, DUMH3(4)
COMMON/HTCOM/HT1, HT2
COMMON/CONTR/CONTR, CONTR1, CONTR2, CONTR3
LOGICAL SW1, SW2, SW3
EQUIVALENCE (INTND, SKIPUP)
DATA STCOM2, STCOM3, BLANK/4HTMAX, SHSTAGE, 6H
FORMAT (1H, 15X, 1A6/ (1H, 15X, 10A6))
FORMAT (1H, 15X, 4HSTOP)
FORMAT (1H, 15X, 16HSTAGE DATA ERROR)
FORMAT (1H, 15X, 11H STAGE ON--2A6)
FORMAT (1H, 15X, 5HSTOP- A6)
*****
INITIALIZATION BEFORE DATA REAU FOR ALL SUBPROGRAMS
*****

```

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35 0J 35 11=1,3959
36 IATHO(11)=1
DO 35 11=1,16
REM(11)=BLANK
0J 16 11=1,4
AINCRS(11)=BLANK
100 JECRES(11)=BLANK
DO 20 11=1,40
10M4(11)=1
DO 21 11=1,63
21 10M5(11)=1
0J 23 11=1,14
23 10M6(11)=1
0J 24 11=1,658
24 10M1(11)=1
CALL LGERR1
CALL TPCSI
CALL VPCSI
CALL SACS
CALL OPT
CALL FLX
SATC=.FALSE.
SAT3=.TRUE.
NATAGE=1
I4ISTE=1
I4IATH=1
SIGN=1.
AMAXH=.4E0
DELTS=.1
PRINT=.
ULIM1=.
OLTM1=.
TIMER=0.
DLH1=1.
PS1=.
PS2=.
PS3=.
PS4=.
PS5=.
PS6=.
PS7=.
PS8=.
PS9=.
PS10=.
PS11=.
PS12=.
PS13=.
PS14=.
PS15=.
OMGPO=7.2911518E-5
AC77F=.
RP77F=.
RCLER1=.
RCLER2=.
AMINER=.
AMAXER=.
TIMINT=.
OLTM3=.
G2EFF=.
C
AUIS SUBROUTINE INITIALIZATION
SAT=.TRUE.
ALPDD1=.
C
AUIS - SACS SUBROUTINES INITIALIZATION
ALPJR1=.
QDESR=.
C
*****
C
POST DATA INITIALIZATION AND PRINT
*****
264 ICONTR=1
CALL OVERLAY(4LTOLA,1,,6HRECALL)
266 CALL STGTS1
267 CALL DEF

```

```

O  INDSKPS=
   H2=DELTS
   IF (TIMINT .LT. AMINER) TIMINT = AMINER
   CALL INPUT2
   IF (SWT2) GO TO 302
C  AUTS SUBROUTINE INITIALIZATION
   ADDIM1=ALPUES
   TIME1=TIME
C
   H1=DELTS
   H2=HT
   H3=HT
   SWT2=.TRUE.
302 T=TIME
   TL1=TIME
   TL2=TIME
   TL3=TIME
   TL4=TIME
   TIMES=TIME-TIMEX
   INJARG = HUC7F .GT. AMAXH
   CALL LINES (13)
   WRITE (9,1) (REM(I),I=1,30)
   IF (INDVPC.EQ.0) GO TO 303
   ICONTX=4
   CALL OVERLAY(4LTOLA,1,6HRECALL)
303 IF (INOTFF.EQ.0) GO TO 304
   ICONTX=2
   CALL OVERLAY(4LTOLA,1,6HRECALL)
304 IF (INDAL2.EQ.0) GO TO 305
   ICONTX=3
   CALL OVERLAY(4LTOLA,1,6HRECALL)
305 ICONTX=5
   CALL OVERLAY(4LTOLA,1,6HRECALL)
   IF (INDLG.EQ.0) GO TO 306
   ICONTX=6
   CALL OVERLAY(4LTOLA,1,6HRECALL)
306 SKIPUP=.TRUE.
   CALL VPCC2
C  POST DATA INITIALIZATION FOR SUBPROGRAMS
   CALL LUGR42
   CALL OPT2
   CALL FLEX2
413 CALL OPT7
   CALL SUFLGP
   CALL OPT6
   IF (INDAUT.EQ.0) GO TO 307
   ICONTX=2
   CALL OVERLAY(4LTOLA,2,6HRECALL)
307 SKIPUP=.FALSE.
   END=.FALSE.
   TIMEA=DELTS+T-1.E-6
   TIMEP=PRINT+T-1.E-6
   *****
C  EXECUTIVE PROGRAM
C  *****
412 TPD = T+DELTS
   IF (TPD .LT. TMAX) GO TO 413
   DELTS = TMAX-T
   H2 = DELTS
   END=.TRUE.
413 CALL HMINIMIM
   IF (HIM.NE.0) GO TO 415
   CALL SUFLGP
   IF (INDSTL.EQ.0) GO TO 417
   IF (END) GO TO 417

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C IF (INDSTG.NE.0) GO TO 417
  TIMEA=T+DELTS-1.E-6
  IF (T.LT.TIMEP) GO TO 414
  TIMEP=T+PRINT-1.E-6
  CALL OPTG
  IF (INDAUT.EQ.0) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,0,6HRECALL)
  GO TO 410
414 IF (INDAUT.EQ.0) GO TO 416
  ICONTR=1
  CALL OVERLAY(4LTOLA,2,0,6HRECALL)
  GO TO 410
415 CALL SUFLGP
  IF (T.LT.TMAX) END=.FALSE.
  IF (INDSTG.EQ.0) GO TO 417
  IF (END) GO TO 417
  IF (INDSTG.NE.0) GO TO 417
  CALL OPTG
  TIMEP=T+PRINT-1.E-6
  IF (T.LT.TIMEA) GO TO 416
  TIMEA=T+DELTS-1.E-6
  IF (INDAUT.EQ.0) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,0,6HRECALL)
  GO TO 410
417 CALL OPTG
  IF (INDAUT.EQ.0) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,0,6HRECALL)
416 IF (INDSTG.EQ.0) GO TO 744
  IF (INDSTG.EQ.0) GO TO 743
  IF (INDSTG.EQ.0) GO TO 412
  *****
  STAGING IS REQUIRED
  *****
C 511 INDSTG = J
  CALL LINES (2)
  WRITE (0,3) (STGVAR(I),I=1,2)
524 DO 525 JJ=1,4
  AINCRS(JJ)=BLANK
525 DECRS(JJ)=BLANK
  IF (INDSTF.EQ.0) GO TO 537
  INDSTF=L
  CALL LINES (2)
  WRITE (6,1,3) STCOM3
  GO TO 744
537 INUSKP=1
  CALL DEF
  ICONTR=1
  CALL OVERLAY(4LTOLA,1,0,6HRECALL)
  STAGE DATA IS READ - FIRST MAJOR OR MINOR
C 543 INUSKP=J
572 IF (INDSTY.NE.0) GO TO 601
  CALL STGT31
  Y=TIME
  MC=DELTS
  SKIPUP = .TRUE.
  IF (SMT3) GO TO 22
  IF (INDLG.NE.2) GO TO 22
  NDEFS=5*NSTRUT
  IF (IL.NE.0) NDEFS=3*NSTRUT
  CALL LNUPD(NDEFS)
  SMT3=.TRUE.
  IF (ISIGN(1,INDLG).GT.L) GO TO 410

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C SWI=FALSE
  IOLG=-INJL
  ICONTR=0
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
  CALL LGEAR2
  CALL LGEAR3
  CALL FLEX2
  GO TO 41
601 INDSY=F
  CALL DEF
  IF (INDSTR.EQ.J) GO TO 604
  INDSY=J
  TIMSX=T
  NSTAGE=NSTAGE+1
604 IF (ISIGN(1,INDVPC).GT.0) GO TO 635
  CALL VPCS1
  INDVPC=-INDVPC
  ICONTR=4
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
605 IF (ISIGN(1,INDTFF).GT.0) GO TO 648
  CALL TFF3
  INDTFF=-INDTFF
  ICONTR=2
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
608 IF (ISIGN(1,INDALR).GT.0) GO TO 664
  CALL SAC31
  INDAER=-INDAER
  ICONTR=3
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
  GO TO 604
743 CALL LINES (2)
  WRITE (6,1) STCOM2
C744 GENERAL STOP
744 CALL LINES (2)
  WRITE (6,1)
  STWCH=TRUE.
  CALL LGEAR4
  RETURN
END
SUBROUTINE INUPD (N,L)
  INTEGER L(1)
  COMMON/DIACOM/SKIPUP(646),INDSTE(1245),OM(2068)
  COMMON/UPDCAL/NUM,P(90),Y(90)
  IF (NUM+L.LE. 90) GO TO 5
  CALL DEF
  WRITE (6,700)
700 FORMAT(55H,NUMBER OF INTEGRATION VARIABLES EXCEEDS MAX LIMIT 90)
  STOP
5 DO 20 I=1,N
  NUM=NUM+1
  L(I)=NUM
20 RETURN
END
SUBROUTINE LNUPD(MN)
  COMMON/UPDCAL/NUM,P(90),Y(90)
  NUM=NUM-MN
  RETURN
END
SUBROUTINE INPUZ
  COMMON/UPDCAL/NUM,P(90),Y(90)
  NUM=J
9 DO 10 I=1,90
  P(I)=0.
  Y(I)=J.
10 RETURN

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END
SUBROUTINE INTEG(K,XU)
COMMON/UPICAL/NUM,P(9),Y(90)
P(K) = XU
RETURN
END
SUBROUTINE UPDAT (JX1,JX2,XJ1,XJ2,XJ3,XJ4,XJ5)
COMMON/DIRGDF/SKIPUP,DM(645),INDSTE(1245),DM1(2665)
COMMON/UPICAL/NUM,P(9),Y(90)
LOGICAL SKIPUP
IF (SKIPUP) GO TO (204,201,202,203,204) ; JX1
GO TO (101,101,102,103,104) ; JX1
104 XJ5 = Y(JX4+4)
103 XJ4 = Y(JX3+3)
102 XJ3 = Y(JX2+2)
101 XJ2 = Y(JX1+1)
100 XJ1 = Y(JX0)
RETURN
204 Y(JX2+4) = XJ5
203 Y(JX2+3) = XJ4
202 Y(JX2+2) = XJ3
201 Y(JX2+1) = XJ2
200 Y(JX2) = XJ1
RETURN
END
SUBROUTINE MININ(MIN)
LOGICAL
COMMON/DIRCOM/F,DX,X,STOPIT,IVAR8H,SW,DM1(2),DXMIN,
*UXMAX,KELLER1,DM2(5),KELLER2,DM3(629),INDSTE,DM4(930),
*PTMIN,DM5(101),INDLG,DM6(151),DM7(2068)
COMMON/UPICAL/N,P(9),Y(90)
COMMON/HTCOM/HT,HT1,HT2
DIMENSION YMAX(90),YU(90),P(90),S(90),YP(90),Y1(90),Z(90),
CXX(90,3)
MIN=L
ACH=L
AF=X+DX
IF (IVAR8H .NE. 0) GO TO 300
XU=X
DO 20 I=1,N
YMAX(I)=ABS(Y(I))
H=AMIN1(HT,HT1,HT2)
X=X
H=AMIN1(AJS(H),ABS(UXMAX))
DO 30 I=1,N
YU(I)=Y(I)
CALL OPT7
CALL OPT4
IF (SW.OR.(INDSTE.EQ.)) GO TO 360
DO 50 I=1,N
P(I)=P(I)
Y(I)=YU(I)+.5*H*P(I)
X=X+.5*H
CALL OPT7
CALL OPT4
IF (INDSTE.EQ.) GO TO 360
IF (SW.AND.(H.GT.STOPT)) GO TO 270
DO 60 I=1,N
S(I)=2.*J*P(I)+P(I)
Y(I)=YU(I)+.5*H*P(I)
CALL OPT7
CALL OPT4
IF (INDSTE.EQ.) GO TO 360
IF (SW.AND.(H.GT.STOPT)) GO TO 270
DO 90 I=1,N

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```

S(I)=0.5*P(I)+S(I)
Y(I)=Y(I)+R*P(I)
X=XJ+H
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 100 I=1,N
Y(I)=Y(I)+H*(P(I)+S(I))/6.
100 X=XJ+0.25*H
DO 120 I=1,N
120 Y(I)=Y(I)+0.25*H*P(I)
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 130 I=1,N
130 J(I)=2.*P(I)+P(I)
Y(I)=Y(I)+0.25*H*P(I)
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 140 I=1,N
140 S(I)=2.*P(I)+S(I)
Y(I)=Y(I)+0.5*H*P(I)
X=XJ+0.5*H
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 150 I=1,N
150 Y1(I)=Y(I)+0.5*H*(P(I)+S(I))/6.
Y(I)=Y1(I)
CALL OPT7
CALL OPT4
IF(SW.OR.(INOSTE.EQ.0))GO TO 360
DO 160 I=1,N
160 S(I)=P(I)
Y(I)=Y(I)+0.25*H*P(I)
X=XJ+0.75*H
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 170 I=1,N
170 S(I)=2.*P(I)+S(I)
Y(I)=Y(I)+0.25*H*P(I)
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
DO 180 I=1,N
180 S(I)=2.*P(I)+S(I)
Y(I)=Y1(I)+0.5*H*P(I)
X=XJ+H
CALL OPT7
CALL OPT4
IF(INOSTE.EQ.0)GO TO 360
IF(SW.AND.(H.GT.STOPT)) GO TO 270
R=C
DO 190 I=1,N
190 Y(I)=Y(I)+0.5*H*(P(I)+S(I))/6.
ERR=(Y(I)-YF(I))/19.
Z(I)=AMAX1(YMAX(I),ABS(Y(I)))

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      B = AMAX1( B,ABS(EMR) / AMAX1( Z(I) ,1.0 ) )
      IF (RELER2 - R) 182,19,1,90
185  IF (ABS(H),GT,AUS(OXMIN)) GO TO 270
190  YMAX(I)=Z(I)
      IF (INDLG.NE.L) CALL LGDET
      IF (SW) GO TO 360
205  X=X0+H
      IF (ABS(XF-X0),GT,1.E-10) GO TO 211
210  CALL OPT7
      CALL OPT4
      GO TO 360
211  IF (H,GT,PRIMIN) GO TO 212
      ACH=ACH+H
      IF (ACH,GE,PRIMIN) GO TO 213
      GO TO 220
213  CALL OPT7
      CALL OPT4
      HT=H
      CALL LINES(1)
      WRITE(6,70) HT
700  FORMAT(22H INTEG RTN,      HT = ,E15.8)
      HT=H
      RETURN
212  ACH=H
      IF (RELER2 ) 230,230,240
230  H=H+H
235  IF (ABS(H),LE,ABS(XF-X0)) GO TO 40
240  HT=H
      H=XF-X0
      GO TO 40
270  H=.5*H
      DO 300 I=1,N
280  YP(I)=Y1(I)
      GO TO 310
300  KF=FIX(OX/OXMIN)
      H=OX/AUS(FLOAT(KF))
      K=
305  K=X+1
      DO 320 I=1,N
310  Y(I)=Y(I)
      CALL OPT7
      CALL OPT4
      IF (SW.OR.(INDSTE.EQ.J)) GO TO 360
      X=X+.5*H
      DO 330 J=1,2
      DO 320 I=1,N
      XK(I,J)=H*P(I)
320  Y(I)=Y(I)+.5*XK(I,J)
      CALL OPT7
      CALL OPT4
330  IF (INDSTE.EQ.C) GO TO 360
      X=X+.5*H
      DO 340 I=1,N
      XK(I,3)=H*P(I)
340  Y(I)=Y(I)+XK(I,3)
      CALL OPT7
      CALL OPT4
      IF (INDSTE.EQ.J) GO TO 360
      DO 350 I=1,N
350  Y(I)=Y(I)+(XK(I,1)+2.*(XK(I,2)+XK(I,3))+H*P(I))/5.
      IF (K.LT,KF) GO TO 305
      X=XF
      IF (INDLG.NE.L) CALL LGDET
      CALL OPT7
      CALL OPT4

```

```

00 CALL LINE(3)
WRITE(6,7)J,HT
RETURN
END
SUBROUTINE LGDET
COMMON/UPDLOC/AMN,P(9),Y(9)
COMMON/LGDE/LA(24),FC2(5),P2(5),PRES(5),C(5),IPPT,LTPT
COMMON/UTCOM/CH,(646),INDSTE(675),NSTRUT,DM2(64)
CA2(5),IL,32T(5),CS2(5)
CUM3(5),MASS2(5),DM5(34),ES(5),SB(5),DM4(131),IB(5),DM6(127),
CINLG,DM7(151),DM8(2,68)
COMMON/HTCOM/HT,HT1,HT2
REAL MASS2
IF (INLG.EQ.2) RETURN
DO 1, I=1,NSTRUT
K=I+NSTRUT
J=LA(K)
KK=K-1
JJ=LA(KK)
L=KK+2*NSTRUT
LL=LA(L)
M=K+2*NSTRUT
MM=LA(M)
NN=LA(1)
HT1=HT
IF (P(J))77,77,78
TTIME=Y(J)/ABS(P(J))
79 IF (TTIME.GE.HT)GO TO 77
HT1=TTIME
GO TO 77
78 TTIME=(SH(I)-Y(J))/P(J)
GO TO 79
77 CONTINUE
IF (Y(J).GT.(-ES(I)))GO TO 50
WRITE(6,49)I,I,Y(J)
49 FORMAT(5X,4H-ES(,11,10H) EXCEEDED/
C5X,2H5(,11,4H) = L15.7)
50 IF (Y(J).LE.ES(I))GO TO 51
IF (Y(J).LE.(SH(I)-ES(I)))GO TO 55
IF (Y(J).LE.(SB(I)+ES(I)))GO TO 52
WRITE(6,53)I,I,Y(J)
53 FORMAT(5X,4H-ES(,11,10H) EXCEEDED/
C5X,2H5(,11,4H) = L15.7)
52 IF (Y(JJ).LE.L.)GO TO 20
Y(JJ)=.
P(JJ)=.
20 IF (P(JJ).LT.L.)GO TO 55
P(JJ)=.
GO TO 55
51 IF (Y(JJ).GE.L.)GO TO 21
Y(JJ)=.
P(JJ)=.
21 IF (P(JJ).LT.G.)P(JJ)=.
55 CONTINUE
IF (IL.NE.J)GO TO 64
HT2=HT
IF (P(MM))66,87,88
86 TTIME=Y(MM)/ABS(P(MM))
89 IF (TTIME.GE.HT)GO TO 87
HT2=TTIME
GO TO 87
88 TTIME=(S2T(1)-Y(MM))/P(MM)
GO TO 89
87 CONTINUE
IF (Y(MM).GT.(-ES2(I)))GO TO 58

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57 WRITE(6,47) I, IY(MM)
   FOPMAT(58X,5H-ESC(,11,1,H) EXCEEDED/
58 C58X,2H52(,11,4H) = E19,7)
   IF(IY(MM).LE.E52(I))GO TO 61
   IF(IY(MM).LE.(S2T(I)-E52(I)))GO TO 61
   IF(IY(MM).LE.(S2T(I)+E52(I)))GO TO 62
   WRITE(6,43) I, IY(MM)
63 FOPMAT(58X,5H-ESC(,11,1,H) EXCEEDED/
   C58X,2H52(,11,4H) = E19,7)
62 IF(IY(LL).LE.C.)GO TO 22
   Y(LL)=.
   P(MM)=.
22 IF(P(LL).LT.C.)GO TO 60
   GO TO 14
61 IF(Y'LL).GE.C.)GO TO 23
   Y(LL)=.
   P(MM)=.
23 IF(P(LL).GE.C.)GO TO 60
   P(LL)=.
140 CONTINUE
60 IF(IH(I).NE.(-1))GO TO 10
   P(NN)=.
   Y(NN)=.
10 CONTINUE
   RETURN
   END
   SUBROUTINE STGTS1
   LOGICAL SW
   COMMON /DIRCOM/
   *CMVAL(5), SW(19), AINCPS(4), DM2(292), DECRES(4), DM3(510),
   *STEST(4), STGTD(4), DM4(187), STGVAR(4), DM5(543),
   *ISTAGE(4), (314), DM7(2,68)
   COMMON/STG/ICOUNT,KCOUNT,LOCAIN(4),LOCAGE(4)
   COMMON/CONT/ICONT1,CONTR1,ICONT2,ICONT3
   DATA BLANK/1H /
   ICOUNT = 0
   KCOUNT = 0
   DO 1 I=1,4
   IF (AINCRS(I) .EQ. BLANK) GO TO 15
   ICONT1=8
   CONTR1=AINCRS(I)
   CALL OVERLAY(4LTOLA,1,0,6HRECALL)
   LOCAIN(I)=ICONT2
   IF(ICONT3.EQ.)GO TO 12
   WRITE (6,11) AINCPS(I)
11 FOPMAT (28H ERROR,THE STAGE VARIABLE **A6,
   * 28H** IS NOT IN THE DIRECTORY/24HJ...LOOKING FOR NEW CASE)
   CALL EXERR(1)
   RETURN
12 ICOUNT = ICOUNT+1
16 CONTINUE
15 DO 2 I=1,4
   IF (DECRES(I) .EQ. BLANK) GO TO 21
   ICONT2=8
   CONTR2=DECRES(I)
   CALL OVERLAY(4LTOLA,1,0,6HRECALL)
   LOCAGE(I)=ICONT2
   IF(ICONT3.EQ.)GO TO 24
   WRITE (6,11) DECRES(I)
   CALL EXERR(1)
   RETURN
24 KCOUNT = KCOUNT+1
20 CONTINUE
21 RETURN
   END

```

```

SUBROUTINE STGTST(INHSTG)
COMMON/DIRCOM/
1 COMVAL(5),SH,DM1(18),AINCRS(4),DM2(292),DECRS(4),DM3(510),
2 STEST(4),STESTD(4),DM4(187),STGVAR(4),DM5(543),ISTAGE,DM6(314),
3 DM7(258)
COMMON/STGT/ICOUNT,KCOUNT,LOCIN(4),LOCDE(4)
LOGICAL SW
DATA AINC,4DECR/5HINCR,,5HDECR./
22 IF (ICOUNT.EQ.0) GO TO 30
IF (ISTAGE.EQ.0) GO TO 61
DO 50 I=1,ICOUNT
J=LCCAIN(I)
IF (COMVAL(J).NE.STEST(I)) GO TO 30
64 CONTINUE
GO TO 43
61 DO 23 I=1,KCOUNT
J = LOCAIN(I)
IF (COMVAL(J).GE. STEST (I) ) GO TO 40
23 CONTINUE
30 IF (KCOUNT .EQ. 0) GO TO 33
IF (ISTAGE.EQ.0) GO TO 64
DO 65 I=1,KCOUNT
J=LCCADE(I)
IF (COMVAL(J).NE.STESTD(I)) GO TO 33
65 CONTINUE
GO TO 50
64 DO 32 I=1,KCOUNT
J = LOCAD(I)
IF (COMVAL(J) .LE. STESTD(I) ) GO TO 50
32 CONTINUE
33 INHSTG =
SW = .FALSE.
RETURN
40 STGVAR(2)=AINCRS(I)
STGVAR(1)=AINCR
GO TO 51
50 STGVAR(2)=DECRS(I)
STGVAR(1)=4DECR
51 INHSTG = 1
SW = .TRUE.
RETURN
END
BLOCK DATA TDATA
COMMON/TABCOM/LOCS(115),STABLE(115)
DATA (STABLE(I),I=1,115)/
*6HTTAB1,6HTTAB2,6HTTAB3,6HTTAB4,6HTTAB5,6HTTAB6,6HTTAB7,6HTTAB8,
*6HTTAB9,6HTTAB10,6HTTAB11,6HTTAB12,6HTTAB13,6HTTAB14,6HTTAB15,
*6HTTAB16,6HTTAB17,6HTTAB18,6HTTAB19,6HTTAB20,6HTTAB21,6HTTAB22,
*6HTTAB23,6HTTAB24,6HTTAB25,6HTTAB26,6HTTAB27,6HTTAB28,6HTTAB29,6HTTAB30,
*6HTTAB31,6HTTAB32,6HTTAB33,6HTTAB34,6HTTAB35,6HTTAB36,6HTTAB37,6HTTAB38,
*6HTTAB39,6HTTAB40,6HTTAB41,6HTTAB42,6HTTAB43,6HTTAB44,6HTTAB45,
*6HTTAB46,6HTTAB47,6HTTAB48,6HTTAB49,6HTTAB50,6HTTAB51,6HTTAB52,
*6HTTAB53,6HTTAB54,6HTTAB55,6HTTAB56,6HTTAB57,6HTTAB58,6HTTAB59,
*6HTTAB60,6HTTAB61,6HTTAB62,6HTTAB63,6HTTAB64,6HTTAB65,6HTTAB66,
*6HTTAB67,6HTTAB68,6HTTAB69,6HTTAB70,6HTTAB71,6HTTAB72,6HTTAB73,
*6HTTAB74,6HTTAB75,6HTTAB76,6HTTAB77,6HTTAB78,6HTTAB79,6HTTAB80,6HTTAB81,
*6HTTAB82,6HTTAB83,6HTTAB84,6HTTAB85,6HTTAB86,6HTTAB87,6HTTAB88,6HTTAB89,
*6HTTAB90,6HTTAB91,6HTTAB92,6HTTAB93,6HTTAB94,6HTTAB95,6HTTAB96,6HTTAB97,
*6HTTAB98,6HTTAB99,6HTTAB100,6HTTAB101,6HTTAB102,6HTTAB103,6HTTAB104,6HTTAB105,
*6HTTAB106,6HTTAB107,6HTTAB108,6HTTAB109,6HTTAB110,6HTTAB111,6HTTAB112,6HTTAB113,6HTTAB114,6HTTAB115/
END
SUBROUTINE TSEARCH(SYM2,LOC2,N2,IER)
COMMON/TABCOM/LOCS(115),STABLE(115)

```

INTEGER LOC2(N2)

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O DATA MAXT/115/
  DO 1000 I=1,MAXT
  IF (SYM2.NE. STABLE(I)) GO TO 1000
  JM=I
  DO 500 J=1,N2
  LOC2(J) = LOC1(JM)
500  JM=JM+1
  ICR = -1
  RETURN
1000 ICR = 1
  RETURN
  END
  SUBROUTINE ASPCH(LOC1,SYM1)
  COMMON/TABCOM/LOC1(115),STABLE(115)
  DATA BLANK,MAXT/1H,115/
  DO 2000 I=1,MAXT
  IF (LOC1.NE. LOC2(I)) GO TO 2000
  SYM1 = STABLE(I)
  RETURN
2000 SYM1 = BLANK
  RETURN
  END
  SUBROUTINE DEF
  TITLE PRINT ROUTINE
  COMMON /CI-COM/ O1(243), INDSOF, D2(19), LONG, NCASE, NPAGE,
  *NSTAGE, J3(2,24), O4(2,68)
  330 FORMAT(1H,3FX,4H,IX DEGPLES OF FREEDOM FLIGHT PATH STUDY/
  *1H,42X,CMHGENERALIZED COMPUTER PROGRAM/
  *1H,28X,7HINDSOF 12,5X,5HCASE A6,7X,
  3H,STAGE 12,5X,5HPAGE 16/1H )
  NPAGE=NPAGE+1
  LONG=J
  WRITE(6,900) INDSOF,NCASE,NSTAGE,NPAGE
  RETURN
  END
  SUBROUTINE STFL(JOPT,N,ARG1)
  C GENERAL PRINT ROUTINE
  LOGICAL CLEAN,INTEG
  COMMON/CLEAF/ I2,CLEAN,INTEG
  COMMON/STOFA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
  DIMENSION ARG1(1)
  IF(JOPT.EQ.1) GO TO 5
  IF(JOPT.EQ.3) GO TO 6
  DO 4 I=1,N
  ARG(I)=ARG1(I)
  IF(JOPT-1) 1,2,3
  NENT=1
  IF(I2.EQ.1) RETURN
  CLEAN=.T/
  CALL AKRAY(N,1)
  RETURN
  C
  2 NENT=2
  K=1
  CALL ARRAY(N,K)
  RETURN
  C
  3 NENT=4
  K=1
  CALL ARRAY(N,K)
  RETURN
  GETARG(1)=ARG1(1)
  NENT=5
  6

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```

      K=2
      CALL ARRAY(N,C)
      RETURN
    END
    BLOCK DATA STFLD
    COMMON/CLAUPT/I2,CLEAN,INTEG
    LOGICAL CLEAN,INTEG
    DATA I2,CLEAN,INTEG/.,.TRUE.,.FALSE./
    END
    SUBROUTINE STOVAR(N,A,B,C,D,E,F,G,H)
    COMMON/STORA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
    IF (IABS(N).LE.2) GO TO 2
    IF (IABS(N).LE.4) GO TO 1
    GETARG(1)=H
    GETARG(7)=G
    GETARG(6)=F
    GETARG(5)=E
    GETARG(4)=D
    GETARG(3)=C
    GETARG(2)=B
    GETARG(1)=A
    NENT=2
    K=2
    CALL ARRAY(N,C)
    RETURN
    END
    SUBROUTINE ARRAY(N,IOPT)
    LOGICAL CLEAN,INTEG
    COMMON/CLAUPT/I2,CLEAN,INTEG
    COMMON/STORA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
    705  FORMAT(5X,18,7I15)
    710  FORMAT(7X,10,7(9X,A6))
    715  FORMAT(1X,3(1PE15.7))
    720  FORMAT(1H )
    IF (IOPT.NE.1) GO TO 200
    IF (NENT.EQ.LENT) GO TO 1010
    IF (I2.LQ.0) GO TO 1005
    CLEAN=.TRUE.
    GO TO 210
    1005  CALL LINES (1)
    WRITE (6,720)
    IF (NENT.EQ.1) RETURN
    1010  INTEG = (N,LT,1)
    NMAX=IABS(N)
    LENT=NENT
    J=1
    GO TO 500
    C
    CLEAN OUT ARRAY
    2000  CALL LINES (1)
    IF (LENT.GE.4) GO TO 2010
    IF (INTEG) GO TO 2015
    WRITE (6,715) (ALIST(I),I=1,I2)
    GO TO 2020
    2005  WRITE (6,705) (ALIST(I),I=1,I2)
    GO TO 2020
    2010  WRITE (6,710) (ALIST(I),I=1,I2)
    2020  I2=C
    IF (.NOT.CLEAN) GO TO 500
    CLEAN=.FALSE.
    GO TO 1000
    C
    DEVELOP ARRAY
    500  ALIST (I2) = GETARG (J)

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C10 GO TO 52
520 ALIST (I) = ARG (J)
      J=J+1
      IF (I2.EQ. 8) GO TO 200J
500 IF (J.GT.4MAX) RETURN
      I2=I2+1
      GO TO (510,500),K
      END
SUBROUTINE LINES(LCOUNT)
      LINES ACCOUNTING ROUTINE
C COMMON /DIRCOM/D1(600),LONG,D2(1227),D3(2068)
      LONG=LON+LCOUNT
      IF (LONG.LE.51) RETURN
      CALL DLF
      LONG=LCOUNT
      RETURN
      END
FUNCTION ASIN(X)
      EXTERNAL ACOS
      ASIN=1.57-7963-ACOS(X)
      RETURN
      END
FUNCTION ACOS(X)
      IF (ABS(X).GT. 1.0) GO TO 100
      IF (ABS(X).GT. 7.4549846E-49) GO TO 50
      ACOS=1.57-7963
      RETURN
50 IF (X.NE. 1.) GO TO 40
      ACOS=0.
      RETURN
40 IF (X.NE. (-1.)) GO TO 30
      ACOS=3.1415926
      RETURN
30 A=0.
      X1=X
      DO 2( I=1,27
      IF (X1.GT. 0.) GO TO 10
      SA=1.
      X2=1.-(2.*X1**2)
      GO TO 5
10 SA=J.
      X2=(2.*X1**2)-1.
      A=A+SA*2.**(-(I-1)-1)
      X1=X2
5 X1=X2
20 ACOS=3.1415926*A
      RETURN
100 WRITE (6,200)X
200 FORMAT(26H,ARGUMENT OUT OF RANGE X =E20.8)
      ACOS=99999999.
      RETURN
      END
FUNCTION ATAN2 (Y,X)
*****
C SINGLE PRECISION FORTRAN ARCTANGENT FUNCTION SUBROUTINE
C NOTE: ----- ZERO ARGUMENTS WILL EXIT WITH ZERO ANSWER
*****
      LOGICAL INDIC
      REAL L
      DIMENSION AA(6),A(4),B(4),PN(4)
      DATA (AA(I), I = 1,6) /
C MIN IS AA(1), MAX IS AA(6)
      * .18020451E-8, .176326981E+0, .577350269E+0, .119175359E+1,
      2 * .274747742E+1, .134217728E+9 /
      DATA (A(I), I = 1,4) /
      * .449587214E+0, .195014224E+0, .944754986E-1, .288535359E-1 /

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DATA (U(I), I = 1,4) / 1.39857E+1, 1.396, 45266E+0, .218181818E+0, .168724015E+0 /
DATA (PH(I), I = 1,4) / 349.6985E+0, .698131701E+0, .104719755E+1, .139626340E+1 /
DATA C1, C2, C3, L / 511.1429E-1, .27098425E-2, .216649136E+0, .163636364E+0 /
DATA PIOV2, ONEPI / .57271633E+1, .314159265E+1 /
IF (Y.EQ. 0.0) GO TO 16
IF (X.EQ. 0.0) GO TO 15
INDIC = (X.LT. 0.0)
INDIC = .TRUE., ANGLE IS IN QUADRANT 1 OR 4
C
R = Y/X
Z = ABS(R)
DO 17 I = 1,6
IF (Z-AA(I).LT. 0.0) GO TO (18,12,11,11,11,11), I
10 CONTINUE
GO TO 17
11 I = I - 2
J = 5 - I
P = PH(I)
Z = A(I) - B(I)/(Z + AA(J))
GO TO 13
12 Z = Z*L
J = 5 - I
P = 2*P
13 ATAN2 = ATAN2 + C3 - C2/((Z**2) + C1)
14 ATAN2 = SIGN(ATAN2, R)
15 IF (.NOT. INDIC) RETURN
IF (ATAN2.GT. 3.0) GO TO 23
ATAN2 = ATAN2 - ONEPI
RETURN
16 ATAN2 = SIGN(PIOV2, Y)
RETURN
17 ATAN2 = PIOV2
GO TO 14
18 ATAN2 = R
GO TO 19
22 ATAN2 = 0.0
RETURN
23 ATAN2 = ATAN2 - ONEPI
RETURN
END
SUBROUTINE ERRRC(LOCT)
GENERAL TABLE ERROR ROUTINE
COMMON /DIRCOM/ DM(5), SW(641), INDSTE, DM1(1244), DM2(2068)
DATA IBL / 2H /
INDSTC = J
CALL LINES (2)
CALL ASRCH(LOCT, NAME)
IF (NAME.EQ. IBL) GO TO 5
WRITE (6,1) NAME
RETURN
5 WRITE (6,2)
1 FORMAT (14H, TABLE ERROR, A6)
2 FORMAT (12H, TABLE ERROR/1H, 47H...LOCATION OF TABLE NOT LISTED IN
1 DIRECTORY...)
RETURN
END
SUBROUTINE EXERR(NUM)
COMMON /DIRCOM/ DM(5), SW(641), INDSTE, DM1(1244), DM2(2068)

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O  INSTE = 4, 0) RETURN
   IF (NOM.EQ. 0) RETURN
   CALL STFL(1, 1, 00)
   CALL LINES 13)
   WRITE (6, J) NUM
3  FORMAT (1HA, 15X, 12HSTOF NUMBER I3)
   RETURN
   END
   SUBROUTINE NOTLU (ND, NA, X, Z, XA, ZR, IE)
      N-DIMENSION TABLE LOOK-UP ROUTINE
      ND DIM. OF LOOK-UP
      NA NUMBERS OF VALUES OF EACH TABLE
      X TABLES OF EACH X IN ORDER
      Z FUNCTION VALUES
      XA ARRAY OF ARGUMENTS
      ZR RESULT
      IE ERROR RETURN
      C NO ERROR
      -1 X ARRAY TOO SMALL
      1 X ARRAY TOO LARGE
      2 ARRAY NOT ASCENDING ORDER

   MJ(2**MAX(N))
   DIMENSION X(1), Z(1), NA(1), XA(1), NS(8), MJ( 32)
   IE=0
   L1=2
   LF=ND-1
   DO 3 I=1, LF
      L2=L1+NA(I)-2
      FINU=0
      (J=J=L1, L2
      IF (X(J).GT.X(J-1)) GO TO 6
      IE=2
   RETURN
6  IF (FINU.NE.0) GO TO 4
   IF (XA(I)-X(J-1)) 8, 4, 4
8  IF (J.GT.L1) GO TO 10
   IE=1
   RETURN
10 FINU=1
   NS(I)=J-2
4  CONTINUE
   IF (FINU) 11, 12, 11
12 IF (XA(I)-X(L2)) 13, 13, 14
14 IE=1
   RETURN
13 NS(I)=L2-1
11 L1=L2+2
   CONTINUE
   KF=2**LF
   MW=-2
   DO 18 I=1, KF, 2
      L1=J
      IZ=J
      MW=MW+2
      NPT=1
      DO 19 J=1, LF
      MH=2**J-1
      IF (AND(MH, MW).EQ.0) GO TO 22
      N=NS(J)+1
      GO TO 23
22 N=NS(J)
23 N=N-L1
      L1=L1+NA(J)
      IZ=NPT*(I-1)+IZ
      NPT=NPT+NA(J)

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48  WJ(I)=Z(I2+1)
    WJ(I+1)=Z(I2+2)
    L1=1
    DO 32 I=1,LF
      M=NS(I)
      P=K*(XA(I)-X(M))/(X(M+1)-X(M))
      JF=KF/C
32  DO 32 J=1,JF
      WJ(J)=WJ(2*J-1)+(WJ(2*J)-WJ(2*J-1))*PER
      Z2=WJ(1)
      RETURN
    END
C   SUBROUTINE ATMS (HGC7F)
      ATMOSPHERE CALCULATION ROUTINE
      LOGICAL HGT9, EVEN
      DIMENSION HH(11), RH0H(11), PB(11), TB(11), AK1(11), AK2(11), AK3(11),
1A(2), B(2), C(2), D(2)
      COMMON /CLXCLM/
      10M(159), AMUA7F, DM1(324), INDATH, DM2(132), PA77P,
      20M3(95), CHDAS, DM4(89), TA77R, DM5(8), VS77F,
      30M6(946), DM7(2368)
C   ALTITUDE, DENSITY, PRESSURE, TEMPERATURE, /
      DATA (HJ(I), I=1, 11)/0., 1.1E4, 2.5E4, 4.7E4, 5.3E4, 7.9E4,
      C9.E4, 10.2E4, 16.E4, 17.E4, 2.E5/
      DATA (RH0H(I), I=1, 11)/2.7E-4, 7.7E-4, 7.7E-5,
      C2.88E-5, 1.3E-6, 3.9E-7, 4.1E-8, 4.26E-9, 2.23E-10,
      C1.8E-12, 1.3E-14, 1.1E-13/
      DATA (PB(I), I=1, 11)/2116, 21699, 472.73, 51.979, 2.5155,
      C1.2161, 2.161E-2, 1.8E-4, 1.5E-5, 7.5E-7,
      C3E-9, 7E-7/
      DATA (TB(I), I=1, 11)/518.688, 389.988, 389.988, 508.788,
      C508.188, 298.188, 298.188, 46.188, 2386.188,
      C2566.188, 2836.188/
      DATA (AK1(I), I=1, 11)/-225569E-4, 0., 1.38466E-4, 0.,
      C-1.59E-5, 0., 4149E-4, 886289E-4, 754341E-5,
      C3.2E-5, 2.22124E-5/
      DATA (AK2(I), I=1, 11)/-5.25612, 0., 11.3883, 0., -7.59218,
      C0.8E-12, 1.7E-24, 3.41648, 6.83E-6, 9.76137/
      DATA (AK3(I), I=1, 11)/0., 157689E-3, 0., 120869E-3,
      C0., 200234E-5, 0./
      DATA A(1), A(2), B(1), B(2), C(1), C(2), D(1), D(2)/.759511, .935787,
      C.17416, .273966, 220., 18., 25., 140./
C   IF ((INDATH.EQ.0).OR.(HGC7F.GE.2.5E6)) GO TO 470
      IF (HGC7F.LT.0.) GO TO 460
      THP=.349*HGC7F
      HGP=THP/(1.+THP/6306766.)
      HGT=HGP*TRUL
      M=2
      IF (HGP.GT.1E0000.) GO TO 49
      M=1
      IF (HGP.GT.90000.) GO TO 49
      HGT9=.FALSE.
C   SEARCH FOR LAYER
49  IF (HGP.LT.HB(11)) GO TO 50
      LAY=11
      GO TO 50
50  DO 55 I=2, 11
      IF (HGP.GT.HB(I)) GO TO 55
      LAY=I-1
      GO TO 50
55  CONTINUE
60  THP=HGP-HB(LAY)
      THP2=1.+AK1(LAY)*THP

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O IF (LAY.GT.6) GO TO 69
IF (2*(LAY/2).NE.LAY) GO TO 69
EVEN=.TRUE.
GO TO 71
69 EVEN=.FALSE.
70 TA77R= T0(LAY)*TMP2
IF (EVEN) GO TO 72
PA77P=PB(LAY)*TMP2*(-AK2(LAY))
RHOAS=RHO0(LAY)*TMP2*(-1.-AK2(LAY))
GO TO 80
72 TMP3=EXP(-AK3(LAY)*TMP)
PA77P=PB(LAY)*TMP3
RHOAS=RHO0(LAY)*TMP3
80 IF (HGT.9.) GO TO 85
STA77R=SQRT(TA77R)
VS77F= 49.2576*STA77R
ANUA7F= .226988E-6*(TA77R*STA77R/((TA77R+198.72)*RHOAS))
RETURN
85 VS77F=.
ANUA7F=.
TA77R=TA77R*(A(H)-B(H)*ATAN(HGP-C(H)/D(H)))
RETURN
460 VS77F=1.11643372
TA77R=TB(1)
PA77P=PB(1)
ANUA7F=1.5723288E-4
RHOAS=RHO0(1)
RETURN
47J VS77F=.
TA77R=.
PA77P=.
ANUA7F=.
RHOAS=.
RETURN
END
C SUBROUTINE INVR3(A,B,INDER)
A 3 X 3 MATRIX INVERSION ROUTINE
DIMENSION A(3,3),B(3,3)
B(1,1)=A(2,2)*A(3,3)-A(2,3)*A(3,2)
B(1,2)=A(1,1)*A(3,3)-A(1,3)*A(3,1)
B(1,3)=A(1,2)*A(3,3)-A(1,3)*A(3,2)
B(2,1)=A(1,2)*A(2,3)-A(2,2)*A(1,3)
B(2,2)=A(1,1)*A(2,3)-A(2,2)*A(1,1)
B(2,3)=A(1,1)*A(2,2)-A(2,2)*A(1,1)
B(3,1)=A(1,2)*A(2,1)-A(2,2)*A(1,1)
B(3,2)=A(1,1)*A(2,1)-A(2,2)*A(1,1)
B(3,3)=A(1,1)*A(2,2)-A(2,2)*A(1,1)
IF (ABS(D).LE.1.E-18) GO TO 19
B(2,1)=A(3,1)*A(2,3)-A(3,3)*A(2,1)
B(2,2)=A(1,1)*A(3,3)-A(3,1)*A(1,3)
B(2,3)=A(1,2)*A(3,3)-A(3,1)*A(1,2)
B(3,1)=A(2,1)*A(3,2)-A(3,1)*A(2,2)
B(3,2)=A(1,1)*A(3,2)-A(3,1)*A(1,2)
B(3,3)=A(1,1)*A(3,3)-A(3,1)*A(1,3)
DO 17 J=1,3
DO 17 I=1,3
17 B(I,J)=B(I,J)/D
INDER=1
RETURN
19 INDER=2
RETURN
END
C SUBROUTINE MULT31(A,B,C)
A MATRIX MULTIPLICATION ROUTINE
DIMENSION A(3,3),B(3,3),C(3)
DO 1 I=1,3
C(I)=.
DO 1 J=1,3

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C(I)=C(I)+A(I,J)*R(J)
RETURN
END
SUBROUTINE MULT33(A,B,C)
C MATRIX MULTIPLICATION ROUTINE
C DIMENSION A(3,3),B(3,3),C(3,3)
DO 1 J=1,3
DO 1 K=1,3
C(I,J)=0.
DO 1 I=1,3
C(I,J)=C(I,J)+A(I,K)*B(K,J)
RETURN
END
SUBROUTINE TRNPOS(A,B)
A J X J MATRIX TRANSPOSE ROUTINE
C DIMENSION A(3,3),B(3,3)
DO 1 I=1,3
DO 1 J=1,3
B(I,J)=A(J,I)
RETURN
END
SUBROUTINE HIHC(N,LOCT,NX1,NX2,NX3,NX4,X1ARG,X2ARG,
* X3ARG,X4ARG,A)
C TABLE SETUP ROUTINE
COMMON/TA3DUP/TABLE(1)
DIMENSION XA(4),NA(4)
11 FORMAT (1H,15X,4HAN ARGUMENT EXCEEDS LOWER LIMIT OF TABLE)
12 FORMAT (1H,15X,4HAN ARGUMENT EXCEEDS UPPER LIMIT OF TABLE)
13 FORMAT (1H,15X,4HAN INDEPENDENT VARIABLES NOT IN ASCENDING ORDER)
XA(1)=X1ARG
XA(2)=X2ARG
XA(3)=X3ARG
XA(4)=X4ARG
NA(1)=NX1
NA(2)=NX2
NA(3)=NX3
NA(4)=NX4
NAT=NX1
IF (N-4) 3,4,5
3 NAT=NAT+NA(2)
GO TO 6
4 NAT=NAT+NA(2)+NA(3)
GO TO 6
5 NAT=NAT+NA(2)+NA(3)+NA(4)
6 II=NAT+LOCT
CALL NOTLJ(N,NA,TABLE(LOCT),TABLE(II),XA,A,IERROR)
IF (IERROR.EQ.0) RETURN
CALL STFL(,1,0UM)
CALL EHROX(LOCT)
CALL LINES(2)
IF (IERROR-1) 7,14,15
7 WRITE(5,11)
13 RETURN
14 WRITE(5,12)
15 RETURN
16 WRITE(5,10)
RETURN
END
SUBROUTINE TLU(X,LOCT,Y)
C TWO DIMENSIONAL TABLE LOOK-UP ROUTINE
COMMON/TA3DUP/C(1)
EQUIVALENCE (N,Z)
LOCTM1=LOCT-1
N=Z
Z=C(LOCT)

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C DO 1, I=1,N
  J=2+I+LOCTH1
  IF (C(J)-X) 1,5,2
1 CONTINUE
  GO TO 5
2 IF (J.GT. (LOCTH1+2)) GO TO 4
  J=3+LOCTH1
5 CALL ERROR(LOCT)
4 Y=C(J-1)+(C(J+1)-C(J-1))*(X-C(J-2))/(C(J)-C(J-2))
  RETURN
6 Y=C(J+1)
  RETURN
END
SUBROUTINE TFFS1

      ENGINE THRUST

      INPUT REQUIRED (FROM DIRCOM)
      ALT77F, AMACH, AMASS, AMASS1, AMASZS, AMT77F,
      ANT77F, INUTFF, TXB7P, TYB7P, TZO7P, IN, N(5),
      ITLW, ITLX, ZN(5), YN(5)

      COMMON/DIRCOM/DM1(126), ALT77F, DM2(6), AMACH, DM3(2),
      *AMASS, AMASS1, AMASZS, DM4(5), AMT77F, DM5(13), ANT77F,
      *DM6(495), INUTFF, DM7(45), TXB7P, DM8(2), TYB7P, DM9(2),
      *TZB7P, DM10(2), ITLW, ITLX, DM11(2), IT1W, IT1X, DM12(21),
      *AMASFS(2), AMASF1(2), DM13(444), IN, ZN(5), YN(5), N(5), DM14(295),
      *DM15(2.68)

      IN      = NUMBER OF ENGINES
      N(1)    = THROTTLE POSITION FOR 1 ENGINE
      YN(1)   = ENGINE POSITION FOR 1 ENGINE
      ZN(1)   = ENGINE POSITION FOR 1 ENGINE
      MT(1)   = ENGINE PITCH MOMENT FOR 1 ENGINE
      NT(1)   = ENGINE YAW MOMENT FOR 1 ENGINE
      T(1)    = ACTUAL ENGINE THRUST FOR 1 ENGINE

      DIMENSION S(2)
      COMMON/FLXUP/DF1(3,6), T(5), BH2(303)
      COMMON/TABSPC/LOC(2), OUMH1(108)
      REAL N, MT(5), NT(5)
      DATA FMT1/BH, TFFS/,
      CS(1), S(2)/2HMT, 2HNT/

      INITIALIZATION BEFORE DATA READ IN

      TXB7P=J.
      TYB7P=J.
      TZB7P=U.
      ALT77F=J.
      AMT77F=J.
      ANT77F=U.
      RETURN

      THRUST COMPUTATION SECTION

      ENTRY TFFS3
      TXB7P=U.
      TYB7P=U.
      TZB7P=U.
      ALT77F=U.
      AMT77F=U.
      ANT77F=U.
      IF (INDTFF.EQ.U) RETURN

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DO 10 I=1,IN
CALL HIRU(3,LCC(1),IT1W,IT1X,DU,DU,N(I),AMACH,
C DU,DU,T(I))
NT(I)=T(I)*ZN(I)
NT(I)=-T(I)*YN(I)
TXB7P=TXB7P+T(I)
AMT77F=AMT77F+NT(I)
AMT77F=AMT77F+NT(I)
10 CONTINUE
RETURN

COC INITIAL PRINT
COC ENTRY TFFS4
COC RETURN
COC COMPUTE AND PRINT CODES
COC ENTRY TFFS5
COC IF(INOTFF.EQ.1)RETURN
COC CALL STFL(3,1,FMT1)
COC CALL STFL(2,2,5)
COC RETURN
COC TIME HISTORY PRINT
COC ENTRY TFFS6
COC IF(INOTFF.EQ.1)RETURN
COC CALL STFL(3,1,FMT1)
COC CALL STOVAK(2,AMT77F,DU,DU,DU,DU,DU,DU)
COC CALL STFL(6,2,DU)
COC CALL LINES(2)
60 WRITE(6,6) (T(I),I=1,IN)
FORMAT(1HJ,63X,4HT(I)/(14X,5E20.8))
RETURN

COC UPDATE INTEGRATION
COC ENTRY TFFI7
COC RETURN
COC END
COC SUBROUTINE TFFS6(IG,TN)
COC SEARCH THROUGH RANGES OF N TO FIND THE N
COC THAT CORRESPONDS WITH THRUST IG AND CURRENT
COC MACH NUMBER
COC INPUT = IG (THRUST) AND MACH (CURRENT AMACH NO.)
COC OUTPUT = TN (THROTTLE SETTING)
COC COMMON/DIRCOM/DM1(26),ALT77F,DM2(6),AMACH,DM3(2),
COC *AMAS5,AMAS51,AMASZ5,UM4(5),AMT77F,DM5(13),ANT77F,
COC *DM6(44),INOTFF,DM7(246),TXB7P,UM8(2),TYB7P,DM9(2),
COC *IZB7P,UM10(2),IT1W,IT1X,DM11(2),IT1W,IT1X,DM12(221),
COC *AMASFS(2),AMASFS1(2),DM13(44),IN,ZN(5),YN(5),N(5),DM14(290),
COC *UM15(2,68)
COC COMMON/TAHDIR/C(1)
COC COMMON/TAJSRC/LOC(2),DUMM1(108)
COC IF(INOTFF.NE.1)GO TO 26
COC TN=.
COC RETURN
26 LOC=LOC(1)-1
COC DO 20 I=1,IT1W

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O K=LOC+1
  CALL HIHQ(3,LOC(1),IT1W,IT1GX,DU,DU,C(K),AMACH,DU,DU,TH2)
  IF (C(K).GT.(-2.))GO TO 21
  IF (TC.GT.TH2)GO TO 19
  TN=-2.
  RETURN
21 IF (C(K).GT.(-1.))GO TO 22
  IF (TC.GT.TH2)GO TO 19
25 TN=C(K-1)+(TH1-TC)* (C(K)-C(K-1))/(TH1-TH2)
  RETURN
22 IF (C(K).EQ.1.)GO TO 27
  IF (C(K).GT.1.)GO TO 23
  IF (TC.GT.TH2)GO TO 19
  TN=-1.
  RETURN
27 IF (TC.GT.TH2)GO TO 19
  TN=1.
  RETURN
23 IF (C(K).GT.2.)GO TO 24
  IF (TC.GT.TH2)GO TO 19
  GO TO 25
24 TN=2.
  RETURN
19 TH1=TH2
20 CONTINUE
  RETURN
  END
  SUBROUTINE TIF39(THRSET,THRUST)
C
C COMPUTE THRUST AS A FUNCTION OF CURRENT MACH NO.,
C AND DESIGNATED THROTTLE SETTING
C
  INPUT - THRSET(THROTTLE SETTING)
  INPUT - AMACH(MACH NO. FROM DIRCOM)
  OUTPUT - THRUST
C
  COMMON/DIRCOM/UM1(126),ALT77F,DM2(6),AMACH,DM3(2),
  *AMASS,AMASS1,AMASS2,DM4(5),ANT77F,DM5(13),ANT77F,
  *UM6(495),INDIFF,DM7(246),TAC7P,DM8(2),TYB7P,DM9(2),
  *TZB7P,UM11(2),IT1W,IT1GX,UM11(2),IT1W,IT1GX,UM12(221),
  *AMASF5(2),AMASF1(2),DM13(444),IN,ZN(5),YN(5),N(5),DM14(290),
  *UM15(2,68)
C
  COMMON/TABSRC/LOC(2),DUMH1(168)
C
  IF (INDIFF.NE.0)GO TO 30
  THRUST=0.
  RETURN
30 CALL HIHQ(3,LOC(1),IT1W,IT1GX,DU,DU,THRSET,AMACH,
  DU,DU,THRUST)
  RETURN
  END
  SUBROUTINE VFCS1
C VEHICLE PHYSICAL CHARACTERISTICS
  DIMENSION A(4)
  COMMON /DIRCOM/
  1DM(29)
  2AIXXUS ,AIXXS1 ,AIXYBS ,AIXYS1 ,AIXZBS ,AIXZS1 ,
  3OM1 ,AIYYOS ,AIYYS1 ,AIYZBS ,AIYZS1 ,DM2 ,
  4AIZZBS ,AIZZS1 ,DM3(68) ,
  5ALLJOF ,ALMJOF ,DM4(2) ,ALNJOF ,DM5(11) ,
  6ALYJOF ,ALZJOF ,DM6(7) ,
  7AMASS ,DM7(25) ,
  8AREFF ,DM8(187) ,
  9DXCGF ,DM9(5) ,

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10DRFF      ,DM1      ,DRFF      ,DM11(15) ,EPS21      ,EPS22      ,
2EPS18      ,EPS19      ,DM12      ,EPS22      ,EPS21      ,EPS22      ,
3EPS23      ,EPS24      ,DM13(215) ,
4INDIOT      ,DM14(3)      ,
5DM15(53)      ,
6INDISO      ,INDVPC      ,DM16(2)      ,
7DM17(223)      ,
8TIMES      ,DM18(74)      ,
9XCGFF      ,XCGFF      ,DM19( 93) ,DM20(2,66)
COMMON/TAB,PC/DUMH1(8) ,LOC(18) ,DUMH2(1)
EQUIVALENCE (BS11XX,A1XXS1) , (BS11YY,A1YYS1) , (BS11ZZ,A1ZZS1) ,
* (BS11XY,A1XYS1) , (BS11XZ,A1XZS1) , (BS11YZ,A1YZS1)
DATA
1(A(1) ,I=1,4) /5HXCGFF,5HAREFF,5HD1RFF,5HD2RFF/,
2,5HDC1/5HAMASS,6H VPCS/
2          FORMAT (2H,10X,26HINITIAL PRINT OUT FOR VPCS)
C          RETURN
C          *****
C          INITIALIZATION AFTER DATA READ IN
C          ENTRY VPCS2
C          IF (INDVPC .EQ. 0) RETURN
C          *****
173      BS11XX=.
        BS11YY=.
        BS11ZZ=.
        BS11XY=.
        BS11XZ=.
        BS11YZ=.
        ALLJDF=.
        ALMJDF=.
        ALNJDF=.
        ALYJDF=.
        ALZJDF=.
        IF (INDXZS.EQ.0) GO TO 212
        A1XYBS=.
        A1YZBS=.
212      IF (INDXYS.NE.0) A1XZBS=0.
        RETURN
C          *****
C          VEHICLE PHYSICAL CHARACTERISTICS SUBPROGRAM SECTION
C          *****
C          ENTRY VPCS3
C          IF (INDVPC .EQ. 0) RETURN
C          *****
216      IF (INDISO.EQ.0) GO TO 451
223      CALL TLU(AHASS,LOC(1),XCGBF)
        CALL TLU(AHASS,LOC(2),A1XXBS)
        CALL TLU(AHASS,LOC(3),A1YYBS)
        CALL TLU(AHASS,LOC(4),A1ZZBS)
        XCGBF=XCGBF+EPS18
        A1XXBS=A1XXBS+EPS19
        A1YYBS=A1YYBS+EPS20
        A1ZZBS=A1ZZBS+EPS21
        IF (INDXZS.NE.0) GO TO 335
        CALL TLU(AHASS,LOC(5),A1XYBS)
        CALL TLU(AHASS,LOC(7),A1YZBS)
        A1XYBS=A1XYBS+EPS22
        A1YZBS=A1YZBS+EPS24
335      IF (INDXYS.NE.0) GO TO 353
        CALL TLU(AHASS,LOC(6),A1XZBS)
        A1XZBS=A1XZBS+EPS23
353      IF (INDJJP.EQ.0) GO TO 451
        CALL TLU(XCGBF,LOC(8),ALYJDF)
        CALL TLU(XCGBF,LOC(9),ALZJDF)
        CALL TLU(XCGBF,LOC(10),ALLJDF)

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C CALL TLU(XCGF,LOC(11),ALNJB)
451 IF (INDIUT.EQ.0) GO TO 567
CALL TLU(TIMES,LOC(13),BS1IX)
CALL TLU(TIMES,LOC(14),BS1IY)
CALL TLU(TIMES,LOC(15),BS1IZ)
503 IF (INDXZ.NE.0) GO TO 551
CALL TLU(TIMES,LOC(16),BS1IX)
CALL TLU(TIMES,LOC(18),BS1IY)
551 IF (INDXZ.NE.0) GO TO 567
CALL TLU(TIMES,LOC(17),BS1IXZ)
567 DXCGF=XCGF-XCGF
      XTUPN
      *****
C      INITIAL PRINT
C      ENTRY VPC34
      IF (INDVPC.EQ.0) RETURN
C      *****
27 CALL STFL(0,1,DU)
   WRITE (6,2)
   CALL STFL(2,4,A)
   CALL STOVAR(4,XCGF,AREFF,D1RFF,D2RFF,DU,DU,DU,DU)
   RETURN
C      *****
C      COMPUTE AND PRINT CODES
C      ENTRY VPC35
      IF (INDVPC.EQ.0) RETURN
C      *****
64 CALL STFL(3,1,HBCI)
   CALL STFL(2,1,B)
   RETURN
C      *****
C      TIME HISTORY PRINT
C      ENTRY VPC36
      IF (INDVPC.EQ.0) RETURN
C      *****
103 CALL STFL(3,1,HBCI)
   CALL STFL(1,1,AMAS)
   RETURN
C      *****
C      ENTRY VPC37
C      *****
   RETURN
END
SUBROUTINE SACS1
EXTERNAL ALIN
C      AERODYNAMIC FORCES AND MOMENTS
LOGICAL INDAFC
DIMENSION D(3),D(3),TMP(20),INC(79),TC(79)
COMMON /DIRCCM/
1DM(22)
2AA77F,DM1(81)
3ALA77F,DM2(3)
4ALPHU,DM4(3),ALPHR1,DM5(3),ALIFTP,DM3(7)
5ALPTD,DM6(8)
6AMACH(3),DM7(4),AMA77F
7DM8(3),AMT77F,DM56(5)
8ANA77F,ANA77P,DM9(6),ANT77F,
9ANUA7F,DM13(2),AREFF,DM11(11)
10ETAD,DM12(3),ELTAR1,DM13(22),CAMNU,DM15(6)
2CA,DM14(2),COMNU,DM17(6),CL
3CD,DM16(2),CLMNU,CM
4DM18(3)
5CM2MNU,CN1MNU,DM19,CPIA,DM24(9),
C      5CRM,DM21(7)

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7CY	DM22	GYM	GYMNU	DM23 (49)	
8UCU1	DCV1	DCW1	UCU2	DCV2	DCW2
9UCU3	UCV3	DCW3	DM24 (15)		
COMMON /DIR COM/					
1 DELPO	DM25	DELQO	DM26	DELPO	DM27 (17)
2 ORAGP	DM28	DXCGF	DM29 (3)		
3 OYNPP	DM31	DIRFF	DM31	DIRFF	DM32 (6)
4 EPS1	EPS2	EPS11	EPS12	DM33 (7)	
5 EPS2	DM34 (7)				
6 EPS3	EPS4	EPS5	EPS6	EPS7	EPS8
7 EPS9	DM35 (43)	HGC7F, DM31 (44)			
8 INDAER	DM37 (2)		INDARC	DM38 (3)	
9 COMMON /DIR COM/					
1 INDA1	INDA12	INDA13	INDA14	INDA15	INDA16
2 INDA17	INDA18	INDA19	INDA20	INDA21	INDA22
3 INDA23	INDA24	INDA25	INDA26	INDA27	INDA28
4 INDA29	INDA30	INDA31	INDA32	INDA33	INDA34
5 INDA35	INDA36	INDA37	INDA38	INDA39	INDA40
6 INDA41	INDA42	INDA43	INDA44	INDA45	INDA46
7 INDA47	INDA48	INDA49	INDA50	INDA51	INDA52
8 INDA53	INDA54	INDA55	INDA56	INDA57	INDA58
9 INDA59	INDA60	INDA61	INDA62	INDA63	INDA64
1 INDA65	INDA66	INDA67	INDA68	INDA69	INDA70
2 INDA71	INDA72	INDA73	INDA74	INDA75	INDA76
3 INDA77	INDA78				
4 INDA81	DM52 (13)	INDBAU	DM39 (7)		
5 COMMON /DIR COM/					
6 INDFLT	DM41 (55)				
7 INDSOF	DM41 (23)				
8 NSYMU	DM42 (14)				
9 SIOEP	DM43 (11)				
1 SP4IA	DM44 (11)				
2 VA77F, DM45 (1)					
3 VS77F	DM45 (35)				
4 Y477P	DM47 (8)	GW7F1, DM59 (179)			
5 PI77P, DM43 (7)					
6 PI77P, DM43 (7)					
7 RI77P, DM43 (13)	TS77P, DM51 (420)	IAP, DM57 (3)			
* ALPHDS, ALPHDL, FCG, DM53 (94)	DELQN, DM54 (7)				
* DELQL, DELJU, DM55 (7)	DELRL, DELRU, DM61 (78)	HP, DM58 (54)	DDM77 (2068)		
COMMON /TALSRC/DUMH1 (2)	LDC (73)	DUMH2 (29)			

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C  
C

COMMON/AUTSAC/ALPHK1, QDESP, CLRR, ALPOLS, CDR, DELRN

COMMON/LG/FXM, FYH, FZM, LM, MM, NM, EPSLOC

REAL LM, MM, NM

EQUIVALENCE (INDA1, INC (1)),

• (TC (1), CAALPH), (TC (2), CAALSQ), (TC (3), CABETA), (TC (4), CAHTS),

• (TC (5), CAULTQ), (TC (6), CAULSQ), (TC (7), CAALDT), (TC (8), CAALDL),

• (TC (9), CAUTDL), (TC (10), CHIZER), (TC (11), CHIALP), (TC (12), CHIASQ),

• (TC (13), CH1HLT), (TC (14), CH1HSQ), (TC (15), CH1DLQ), (TC (16), CH1DSQ),

• (TC (17), CH1ALH), (TC (18), CH1ALD), (TC (19), CH1HDL), (TC (20), CH1AUL),

• (TC (21), CH1AOX), (TC (22), CH1Q ), (TC (23), CH1QX ), (TC (24), CYZERO),

• (TC (25), CYALPH), (TC (26), CYALSQ), (TC (27), CYRETA), (TC (28), CYNTSQ),

• (TC (29), CYDLRR), (TC (30), CYORSQ), (TC (31), CYALHT), (TC (32), CYALUL),

• (TC (33), CYDTLP), (TC (34), CYDTDT), (TC (35), CYDTDX), (TC (36), CYR ),

• (TC (37), CYRX ), (TC (38), CLZERO), (TC (39), CLALPH), (TC (40), CLALSQ),

• (TC (41), CLBETA), (TC (42), CLBTSQ), (TC (43), CLDLTP), (TC (44), CLDLST),

• (TC (45), CLALPT), (TC (46), CLALDL), (TC (47), CLBTDL), (TC (48), CLP ),

• (TC (49), CLH ), (TC (50), CLRX ), (TC (51), CHZERO), (TC (52), CHALPH),

• (TC (53), CHALSQ), (TC (54), CHBETA), (TC (55), CHRTSQ), (TC (56), CHDLTQ),

• (TC (57), CHULSQ), (TC (58), CHALHT), (TC (59), CHALDL), (TC (60), CHDTUL),

• (TC (61), CHALDT), (TC (62), CHADTX), (TC (63), CHQ ), (TC (64), CHQX ),

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C * (TC(66),CN2B58),(TC(66),CN2DLP),(TC(67),CN2DS8),(TC(68),CN2RET),
EQUIVALENCE
* (TC(73),CN2ALD),(TC(74),CN2BDL),(TC(75),CN2BT0),(TC(76),CN2BDX),
* (TC(77),CN2R ),(TC(78),CN2RX),(TC(79),CAVAH)
EQUIVALENCE (CY,CYA),(DYNPL,DYNPP)
DATA DEGRAD,31745329/
DATA
*HJCI,C/6H SAC1,6HCAVAH /,
1 (H(I),I=1,3)/2HCA,2HCH,2HCY/,
2 (U(I),I=1,3)/2HCL,2HCM,3HCNN/
1 FORMAT (1H,15X,26HINITIAL PRINT OUT FOR SAC1)
1267 ANA77P=U.
ALA77F=U.
AMA77F=U.
ANA77F=U.
AA77P=U.
YA77P=U.
RETURN
C *****
C ENTRY SAC33
C *****
IF (INDAER.EQ. ) RETURN
IF (INDARC) GO TO 1267
IF (VS77F.NE.U.) GO TO 1470
CA =CAMNU
CH =CN1MNJ
CY =CYMNU
CRM=CLMNU
C1 =CM1NJ
CY1=CN1NNJ
1401 TMP(1)=EPS5*CY+EPS6
TMP(2)=DYNPP*AREFF
YA77P=TMP(1)*TMP(2)
ALA77F=(EPS7*CRM+EPS8)*TMP(2)*D2RFF
ANA77F=(EPS11*CYM+EPS12)*TMP(2)*D2RFF
TMP(1)=EPS3*CA+EPS4
TMP(2)=DYNPP*AREFF
AA77P=TMP(1)*TMP(2)
AA77P=(EPS1*CN+EPS2)*TMP(2)
AA77F=(EPS9*CH+EPS11)*TMP(2)*D1RFF
RETURN
1470 IGO1=1
IGO2=1
IGO3=1
DO 71 I=1,79
71 TC(I)=U.
50 HG=HGC7F
IF (IAP.GC.3) HG=HR
C EPSLO2 IS COMPUTED IN SUBROUTINE LGEA3C
TMP(1)=EXP(-4.6*(HG-EPSLO2-HCG)/(D2RFF-HCG)) ,
DO 79 I=1,6
IF (INC(I).NE.U) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
79 CONTINUE
DO 80 I=15,16
IF (INC(I).NE.U) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
80 CONTINUE
DO 81 I=10,12
IF (INC(I).NE.U) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
81 CONTINUE
DO 85 I=20,22,2
IF (INC(I).NE.U) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
85 CONTINUE
IF (INDA83.NE.U) CAVAH =(AERO1(LOC(79),AERO2)-AERO2)*TMP(1)+AERO2
GO TO (1,20,33),IGO1

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1  DO 62 I=71,53
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
62  CONTINUE
   DO 63 I=29,63
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
63  CONTINUE
   GO TO (11,46), IGO2
11  DO 64 I=27,26
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
64  CONTINUE
   DO 70 I=24,71
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
70  CONTINUE
   GO TO (12,66), IGO3
12  DO 72 I=3,9
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
72  CONTINUE
   DO 73 I=3,14
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
73  CONTINUE
   DO 74 I=7,24
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
74  CONTINUE
   DO 75 I=3,51
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
75  CONTINUE
   DO 76 I=24,55
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
76  CONTINUE
   DO 77 I=24,67
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
77  CONTINUE
   DO 78 I=72,78
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
78  CONTINUE
   TMP(2)=A35(ALPHD)
   TMP(4)=A35(BETAD)
   TMP(3)=0.1AU**2
   TMP(5)=A35(DELDQ)
   TMP(6)=ALPHD*ALPHD
   TMP(7)=A35(DELRD)
   TMP(8)=.5*DEFF/VA77F
   CJ=CAYAH+TMP(2)*CAALPH+ALPHD**2*CAALSD+TMP(4)*CABETA+TMP(3)*
   * CABTS+TMP(5)*CADLIQ+DELDQ**2*CAOLSD+ARS(ALPHD*DELDQ)*CAALDL+
   * ARS(ALPHD*BETAD)*CAALBT+ARS(BETAD*DELDQ)*CABTDL
   CL=CN1Z1+ALPHD*CN1ALP+ALPHD*TMP(2)*CN1ASQ+TMP(4)*CN1BET+
   * TMP(3)*CN1BSQ+DELDQ*CN1DLQ+TMP(5)*DELDQ*CN1DS2+TMP(2)*DELDQ*
   * CN1ALQ+TMP(4)*ALPHD*CN1ALB+TMP(4)*DELDQ*CN1BDL+
   * 0.1(FF/VA77F*ALPHD**2*(CN1AQX*DXCGF+CN1ADL)+
   * 0.1FF/VA77F*CI77P/2*(CN1QX*DXCGF+CN1Q ))
   TMP(9)=ALPHD*.174534
   CA=CO*CO5(TMP(3))-CL*SIN(TMP(9))
   CN=CL*CO5(TMP(3))+CO*SIN(TMP(9))
   CY=CYZLRD+TMP(2)*CYALPH+TMP(6)*CYALSD+BETAD*CYBETA+BETAD*TMP(4)*
   * CYBTS+DELRD*CYDELR+TMP(7)*DELRD*CYDRSQ+TMP(2)*DELRD*CYALDL+
   * TMP(2)*BETAD*CYALBT+TMP(4)*DELRD*CYBTDL+
   * BETAR1*TMP(8)*(CYRDX*DXCGF+CYBTDT)+
   * R17/R *TMP(8)*(CYRX *DXCGF+CYR )
   TMP(8)=A35(ALPHD)
   TMP(1)=ALPHD**2
   TMP(9)=A35(BETAD)
   TMP(10)=A35(DELRD)
   TMP(2)=0.1FF/VA77F*2.
   TMP(3)=BETAD*BETAD
   TMP(4)=ARS(DELDQ)

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C  CRH=CLZERO+TMP(8)*CLALPH+TMP(11)*CLALSO+TMP(9)*CLBETA+BTAD**2*
  CLDT50+DELPD*CLDLTP+ABS(DELPO)*DELPD*CLDLSQ+TMP(8)*DELPD*
  CLALDL+ABS(ALPHD*BTAD)*CLALHT+TMP(9)*DELPD*CLBTOL+
  TMP(2)*PI77R*CLP+PI77R*TMP(2)*(CLRX*DXCGF+CLR)
C  CM=CNZER+ALPHD*CHALP+TMP(8)*ALPHD*CHALSO+TMP(9)*CHBETA+TMP(3)*
  CHUTS+DELQD*CHDLTQ+TMP(4)*DELQD*CHDLSQ+TMP(8)*CHALDL*DELQD+
  TMP(3)*ALPHD*CHALHT+TMP(4)*DELQD*CHBTOL+
  D1KFF/VA77F*ALPHD/2*(CHADIX*DXCGF+CHALDT)+
  D1KFF/VA77F*Q177R/2*(CHQX*DXCGF+CHQ)-
  DXCGF/D1RFF*CN
C  CYM=CNZER+TMP(8)*CN2ALP+TMP(11)*CN2ASQ+BTAD*CN2BET+TMP(9)*BTAD*
  CN2DS+DELRO*CN2DLT+TMP(10)*CN2DSQ*DELRO+TMP(8)*DELRO*CN2ALD+
  TMP(8)*BTAD*CN2ALB+TMP(9)*CN2BOL*DELRO+
  TMP(2)*BTAR1*(CN2DIX*DXCGF+CN2BTD)+
  TMP(2)*RI77R*(CN2RX*DXCGF+CN2R)-CY*DXCGF/D2RFF
GO TO 141
C  *****
C  ENTRY SAC34
C  *****
C  IF (INDAER.EQ.0) RETURN
C  RETURN
C  *****
C  ENTRY SAC35
C  *****
C  IF (INDACK.EQ.0) RETURN
63  CALL STFL(3,1,HBCI)
  IF (INDABU.NE.0) CALL STFL(2,1,C)
  CALL STFL(2,3,U)
123  CALL STFL(2,3,U)
  RETURN
C  *****
C  ENTRY SAC36
C  *****
C  IF (INDAER.EQ.0) RETURN
326  CALL STFL(3,1,HBCI)
  IF (INDABU.NE.0) CALL STFL(1,1,CAVAH)
  CALL STOVAK(3,CA,CN,CY,DU,DU,DU,DU,DU)
37J  CALL STOVAK(3,CRH,CM,CYM,DU,DU,DU,DU,DU)
  RETURN
C  *****
C  ENTRY SAC37
C  *****
C  RETURN
C  *****
C  DETERMINE THE ALPHA THAT MAKES CL=CLRR AND THE
  ASSOCIATED CUR
C  ENTRY SAC38
C  *****
C  INPUT FROM CALLING PROGRAM
C  CLRR
C  OUTPUT
C  ALPDES, CUR
C  *****
C  INPUT FROM DIRCOM
C  DELQN, ALPHDS, ALPHDL, HCGD2RFF, INDAU1, INDAU2, HR,
  INDA15, INDA16, INDA18, INDA39, INDA40, INDA80
  INDA20, INDA22, D1KFF, VA77F, PI77F, ALPHR1
C  IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6)) GO TO 20
  IG01=2
  GO TO 50
20  TMP(2)=CN1ZER+CN1DLQ*DELQN+CN1DSQ*ABS(DELQN)*DELQN-CLRR
  C+.5*CN1Q*QUESR*D1RFF/VA77F
  ALPDES=AQUAD(CN1ASQ,CN1ALP,TMP(2),ALPHDS,ALPHDL)

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COR=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
RETURN

DETERMINE THE CL1 AND C01 FOR ALPHA=A1
ENTRY SACJ9

      INPUT FROM CALLING PROGRAM
ALPDES
      OUTPUT
CLRR,COR
      INPUT FROM DIRCOM
DELQN, HG, DZREF, INDAJ1, INDA02, INDA15, INDA16, HR,
INDA38, INDA39, INDA46, INDA80, INDA2L, INDA22,
D1REF, VA77F, Q177R, ALPHR1

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 3J
IG01=1
GO TO 5J
36 CLRR=CN1ZER+CN1ALP*ALPDES+CN1ASQ*ABS(ALPDES)*ALPDES+CN1OLQ
C*DELQN+CN1USQ*ABS(DELQN)*DELQN
C+.5*CN1Q*Q177R*D1REF/VA77F
COR=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
RETURN

EVALUATE NOMINAL DELQN
ENTRY SACJ10

      INPUT FROM CALLING PROGRAM - ALPDES
      OUTPUT - DELQN
      INPUT FROM DIRCOM
DELQL, DELQU, PCG, D1REF, D2REF, DYNPP, AREFF, DXCGF, HR,
ANT77F, INDA11, INDA12, INDA15, INDA16, INDA38, INDA39, INDA46,
INDA82, INDA81, INDA82, INDA83, INDA85, INDA87,
INDA81, INDA83, VA77F, ALPHR1, Q177R

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 4J
IG01=1
IG02=2
GO TO 5J
40 TMP(2)=CN1ZER+ALPDES*(CN1ALP+CN1ASQ*ABS(ALPDES))
C+CN1OLQ*DELQN+CN1USQ*ABS(DELQN)*DELQN
C+.5*CN1Q*Q177R*D1REF/VA77F
TMP(3)=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
TMP(4)=TMP(2)*COS(ALPDES*DEGRAD)+TMP(3)*SIN(ALPDES*DEGRAD)
TMP(5)=DYNPP*AREFF*D1REF
TMP(6)=-1*TMP(4)*DXCGF*TMP(5)/D1REF
TMP(7)=CMULTG*TMP(5)
TMP(8)=(CM2ESQ+ALPDES*(CHALPH+CHALSQ*ABS(ALPDES)))
C*TMP(5)+ANT77F*TMP(2)+MM
C+.5*CMQ*Q177R*D1REF*TMP(5)/VA77F
TMP(9)=TMP(5)*CMULSQ
DELQN=AQUAD(TMP(2),TMP(3),TMP(4),DELQL,DELQU)
RETURN

EVALUATE NOMINAL DELRN
ENTRY SACJ11

      INPUT FROM DIRCOM
IAP, DZREF, LYNPP, AREFF, ANT77F, YGW7F1, VA77F
DELRL, DELRU

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 6J

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C GOJ=2
GO TO 11
60 BETADE=C
IF (IAP.GE.3) BETADE=ASIN(-YGH7F1/VA77F)*57.2957795
TMP(5)=OY1PP*AXEFF*OZPFF
TMP(6)=OXGUF/OZRF
TMP(3)=CNZULT*TMP(5)
TMP(2)=CNZUSQ*TMP(5)
TMP(4)=ANT77F*BETADE*(CNZBET-CYBETA*TMP(6)
C+ABS(BETA1E)*(CNZBSQ-CYBTSQ*TMP(6)))*TMP(5)
DELRN=AQUAD(TMP(2),TMP(3),TMP(6),DELR,DELRU)
RETURN
END
FUNCTION AEROC1(LOCT,AERO2)
COMMON/TABOIP/C(1)
ACPO1=C(LOCT)
AERO2=C(LOCT+1)
RETURN
END
FUNCTION AQUAD(A,B,C,XLLIM,XULIM)
IF (ABS(A).GT.1.E-10) GO TO 4
X=0
IF (ABS(B).LE.1.E-10) GO TO 11
X=-C/B
GO TO 11
4 TMP=0+4.*A*C
IF (TMP.LT.0) GO TO 3
TMP1=SQRT(TMP)
X=(-B+TMP1)*.5/A
IF (X.LT.0) GO TO 5
IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
5 X=(-B-TMP1)*.5/A
IF (X.LT.0) GO TO 3
IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
30 TMP=0+4.*A*C
IF (TMP.LT.0) GO TO 10
TMP1=SQRT(TMP)
X=(-B+TMP1)*.5/(-A)
IF (X.GT.0) GO TO 10
IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
15 X=(-B-TMP1)*.5/(-A)
IF (X.GT.0) GO TO 10
IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
11 FX1=XLLIM*(A*AUS(XLLIM)+B)+C
FX2=XULIM*(A*AUS(XULIM)+B)+C
X=XLLIM
IF (ABS(FX1).GT.AUS(FX2)) X=XULIM
20 AQUAD=X
RETURN
END
SUBROUTINE OPT1
EXTERNAL ASIN,ATAN2
C SIX-DEGREE-OF-FREEDOM OVER FLAT PLANET
DIMENSION
* TMP(27),D(17),D(2),E(2),DRAGG(4),
* F (1),H (2),J (3),K (3),
* L(3),G(2),LA(14)
LOGICAL INARC, SW
COMMON /JIRCOM/
* DM(22),AA77P,AE77F,DM2(4),AIXH7S,AIXXBS,
* AIXXS1,AIXYBS,AIXYS1,AIXZBS,AIXZS1,DM3,
* AIYYBS,AIYYS1,AIYZBS,AIYZS1,DM4,AIZZBS,
* AI7ZS1,DM5(7),AKL1,AKL2,AKL3,
* AKL4,AKL5,AKL6,AKMT,AKM1,
* AKM2,AKM3,AKM4,AKM5,AKM6

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C 5D(1),D(2),5HALPHD,5HBLTAD/,E(1),E(2),6HALPHD1,6HBETAD1/,
5F(1),5HG77F7,G(1),G(2),5HGM70,5HSIG7U/,
6H(1),H(2),6HGAM7R1,6HSIG7R1/,J(1),J(2),5HTHTPD,5HPSIPD,
75HPH1PU/,K(1),I=1,3/5HAXP7F,5HAYP7F,5HAZP7F/,
8(L(1),I=1,3/5HAX77F,5HAY77F,5HAZ77F/,
P/6HTHTRD/
* DATA
* HBGI, C M
* 6H 2SDF,5HRG77N,5HMT7P/,
* (ORAGC(I),I=1,4)/3HFC,3HFCX,3HFCY,3HFCZ/
FORMAT (1H,15X,36HPRINT CODES IDENTIFYING TIME HISTORY)
PRE DATA INITIAL PRINT OUT FOR 2SDF)
INOSDF=2
RETURN
*****
ENTRY OPT2
*****
* (AL17S1,AL1,AL27S1,AL2,AL37S1,AL3,AM17S1,AM1,
* AM27S1,AM2,AM37S1,AM3,AN177S,AN1,AN277S,AN2,
* AN377S,AN3,U777F1,U777F,V777F1,V777F,W777F1,
* W777F,PI77R1,PI77R,QI77R1,QI77R,RI77R1,RI77R,
* XG77F1,XG77F,YG77F1,YG77F,ZG77F1,ZG77F)
62 CALL INUPD (1,LA)
CALL LGEAR4
CALL VPC3
CALL TFF3
CALL SACS4
CALL FLEX4
CALL STFL(1,1,DU)
CALL LINES (2)
WRITE (0,1)
CALL STFL(2,1,HBGI)
CALL STFL(2,2,H)
IF (INDOCR.NE.1) CALL STFL(2,1,G)
IF (INDAPC.NE.1) CALL STFL(2,2,D)
IF (INDAON.NE.1) CALL STFL(2,2,E)
IF (INDCSR.NE.1) CALL STFL(2,1,F)
236 IF (INUPA.EQ.1) GO TO 25
CALL STFL(2,2,G)
IF (INDOPR.NE.1) CALL STFL(2,2,H)
250 IF (INDORT.NE.1) CALL STFL(2,3,J)
IF (INDACH.EQ.1) CALL STFL(2,3,K)
IF (INDACH.EQ.2) CALL STFL(2,3,L)
IF (INDWGT.NE.1) CALL STFL(2,1,M)
IF (INDRMC.EQ.1) GO TO 335
CALL STFL(2,1,P)
C (HTRR1,HTRR)
335 CALL INUPD (1,LHTRR)
CALL STFL(1,4,ORAGC)
CALL LGEAR5
CALL VPC3
CALL TFF3
CALL SACS3
CALL FLEX3
CALL STFL(1,1,DU)
CALL DEF
C367 2SDF
367 ZG77F = -HG77F
SIGDD = SIG7D
GAMDD = GAM7D
SIGUR = SIGDD*.01745329
GAMDR = GAMDD*.01745329
SIGL1 = SIGDR
GAML1 = GAMDR

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SGAMU = SIN(GAMU)
CSIGU = SIN(SIGU)
THTBR = THBR*.1745329
PSIBR = PSIB*.1745329
PHIBR = PHIB*.1745329
SPHIB = SIN(PHIB)
CPHIB = COS(PHIB)
STHBR = SIN(THBR)
CTHBR = COS(THBR)
SPSIB = SIN(PSIB)
CPSIB = COS(PSIB)
DCL1 = CPSIB*CTHBR
DCL2 = SPSIB
DCL3 = -CPHIB*STHBR
UCH1 = SPHIB*STHBR - CPHIB*SPSIB*CTHBR
UCH2 = CPHIB*CPSIB
UCH3 = SPHIB*CTHBR + CPHIB*STHBR*SPSIB
UCH4 = CPHIB*STHBR + CTHBR*SPSIB*SPHIB
UCH5 = -SPHIB*CPSIB
UCH6 = CPHIB*CTHBR - SPHIB*STHBR*SPSIB
AL1 = DCL1
AL2 = DCL2
AL3 = DCL3
AM1 = UCH1
AM2 = UCH2
AM3 = UCH3
AN1 = UCH4
AN2 = UCH5
AN3 = UCH6
XG77F1 = CSIGU*CGAMU*VG77F
YG77F1 = CSIGU*CGAMU*VG77F
ZG77F1 = -SGAMU*VG77F
TMP(1) = XG77F1
TMP(2) = YG77F1
TMP(3) = ZG77F1
CALL INTEG (LA(16), XG77F1)
CALL INTEG (LA(17), YG77F1)
CALL INTEG (LA(18), ZG77F1)
CALL MULT31 (DCL1, TMP(1), TMP(4))
U777F = TMP(4)
V777F = TMP(5)
W777F = TMP(6)
TNOSKP=1
GO TO 702
*****
ENTRY OPT4
*****
SOF
DCL1 = AL1
DCL2 = AL2
DCL3 = AL3
UCH1 = AM1
UCH2 = AM2
UCH3 = AM3
UCH4 = AN1
UCH5 = AN2
UCH6 = AN3
TMP(1) = U777F
TMP(2) = V777F
TMP(3) = W777F
CALL TRNF31 (DCL1, TMP(4))
CALL MULT31 (TMP(4), TMP(1), TMP(13))
XG77F1 = TMP(13)

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C  
C621  
621

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O YG77F1= TMP(14)
  ZG77F1= TMP(15)
  CALL INTCG (LA(16) , XG77F1 )
  CALL INTCG (LA(17) , YG77F1 )
  CALL INTCG (LA(18) , ZG77F1 )
C7.2 SQF2
762 GX87F = DCL3*GREFF
  GY87F = DCM3*GREFF
  GZ87F = UCN3*GREFF
  HGC7F = -ZG77F
  CALL ATMS (HGC7F+RWHGR)
  IF (INDGCR.NE.) RG77N =
    * SURT((XG77F-XGZ7F)**2+(YG77F-YGZ7F)**2)*1.6457925E-4
  IF (INDWIN.NE.) GO TO 754
  UW77F = Y.
  VW77F = J.
  WW77F = J.
  GO TO 752
754 GO TO (752,757,761), INDWIN
755 TMP(1)=TIME
  GO TO 752
757 TMP(1)=HGC7F
  GO TO 762
761 TMP(1)=RG77F
762 CALL TLU(TMP(1),LOC(2),XGW7F1)
  CALL TLU(TMP(1),LOC(3),YGW7F1)
  CALL TLU(TMP(1),LOC(4),ZGW7F1)
  TMP(1)=XGW7F1
  TMP(2)=YGW7F1
  TMP(3)=ZGW7F1
  CALL MULT11 (DCL1,TMP(1),TMP(4))
  UW77F = TMP(4)
  VW77F = TMP(5)
  WW77F = TMP(6)
1035 VA77F = SURT((UW77F-UW77F)**2+(VW77F-VW77F)**2+(WW77F-WW77F)**2)
  OYNFP = .2*RHOAS*VA77F**2
  AMACH = J.
  IF (VS77F.NE.) AMACH=VA77F/VS77F
  TMP(1)=UW77F-UW77F
  ALPHR = ATAN2(W77F-WW77F,TMP(1))
  BETAR = ATAN2(V77F-VW77F,TMP(1))
  ALPHD = ALPHR*57.2957795
  BETAU = BETAR*57.2957795
  IF (INDSKP.EG.) GO TO 1134
  ALPL1 = ALPHR
  BETL1 = BETAR
1134 IF (INDADD.EQ.) GO TO 1163
  DELT1 = TIME-TL1
  IF (ABS(DELT1).LT.ULIM1) GO TO 1163
  ALPHR1 = (ALPHR-ALPL1)/DELT1
  BETAR1 = (BETAR-BETL1)/DELT1
  ALPL1 = ALPHR
  BETL1 = BETAR
  TL11 = TIME
C1163 ZSQF9
1163 VG77F = SURT(XG77F1**2+YG77F1**2+ZG77F1**2)
  IF (VG77F.EQ.0.) GO TO 1314
C1231 ZSD10
1231 TMP(1)=-ZG77F1/VG77F
  IF (ABS(TMP(1)).LT.1.) GO TO 1211
  GAM7R=1.57079632*TMP(1)/ABS(TMP(1))
  GO TO 1212
1211 GAM7R=ASIN(TMP(1))
1212 GAM7U = GAM7R*57.2957795
  GAMOR = GAM7P

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      GAMDD = GAM7D
      SIG7R = ATAN2(YG77F1,XG77F1)
      SIGOR = SIG7R
      SIG7D = SIG7R*57.2957795
      SIGOD = SIG7D
C1236 25011
1236 25010 = SIN(GAMOR)
      GAMD = COS(GAMOR)
      SIGO = SIN(SIGOR)
      SIGD = COS(SIGOR)
      IF (INDFPA.EQ.1) GO TO 1314
      UCLT = TIME-TCLC
      IF (ABS(UCLT).GT.1) GO TO 1314
      GAM7F1 = (GAMDD-GAM1)/UCLT
      SIG7F1 = (SIGOR-SIG1)/UCLT
      TCLC = TIME
      GAM1 = GAMD
      SIG1 = SIGOR
1314 IF (INDWIN.EQ.1) GO TO 1315
      SGAMA = SGAMU
      GO TO 1315
1315 IF (VA77F1.EQ.1) GO TO 1316
      SGAMA = (ZG77F1-ZG77F1)/VA77F
1316 IF (INDPLA.EQ.1) GO TO 1754
C1517 25015
1517 IF (INDGRT.EQ.1) GO TO 1541
1524 IF (OCL1.EQ.1) GO TO 1536
      TMP = ATAN2(-OCL1,OCL1)
      TMPD = TMP*57.2957795
1536 IF (ABS(OCL2).GT.1) GO TO 1546
      PSIPR = ASIN(OCL2)
      GO TO 1546
1546 PSIPR = 57.79632*OCL2/ABS(OCL2)
1554 PSIPD = PSIPR*57.2957795
      IF (OCM2.EQ.1) GO TO 1701
      PHIPR = ATAN2(-OCM2,OCM2)
      PHIPD = PHIPR*57.2957795
1701 IF (INDACH.EQ.1) GO TO 1754
      IF (AMASS.EQ.1) CALL EXERR (14)
      AX77F = F(X77F/AMASS-GXB7F)
      AY77F = F(Y77F/AMASS-GYB7F)
      AZ77F = F(Z77F/AMASS-GZB7F)
      IF (INDACH.EQ.1) GO TO 1754
      TMP(1) = AX77F
      TMP(2) = AY77F
      TMP(3) = AZ77F
      CALL TRNPOS (OCL1,TMP(1))
      CALL MULT31 (TMP(1),TMP(1),TMP(4))
      AX77F = TMP(4)
      AY77F = TMP(5)
      AZ77F = TMP(6)
1754 CALL VPCST
      CALL TFFST
      WTR7P = AMASS*GREFF
C
CCCC
      CHUTE DRAG COMPUTATION
      ICS=1 (FROM LANDING ROLL COMPUTATION,AUTS)
      ICS=0 (INPUT)
      CDCH DRAG COEFFICIENT
      SCH REFERENCE AREA
      XCH, YCH, ZCH = CHUTE ATTACH POINTS
2061 IF (ICS.EQ.1) GO TO 2056
      FCX=C
      FUC=C

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FCY=C.  
FCZ=L.  
MOX=L.  
MOY=.  
MOZ=.  
GO TO 2352  
2050 FJC=CDCH\*SSH\*QYNRP  
FCX=-FUC\*(U777F-UH77F)/VA77F  
FCY=-FUC\*(V777F-VH77F)/VA77F  
FCZ=-FUC\*(W777F-WH77F)/VA77F  
MOX=YCH\*FCZ-ZCH\*FCY  
MOY=ZCH\*FCX-XCH\*FCZ  
MOZ=XCH\*FCY-YCH\*FCX  
2062 CALL SAC53  
2125 CALL LGEA-3  
CALL FLEX3  
FX07P = TX07P-AA77P +AMASS\*GX07F+DLFXP+FXM+FCX  
FY07P = TY07P-YA77P +AMASS\*GY07F+DLFYF+FYH+FCY  
FZ07P = TZ07P-ANA77P+AMASS\*GZ07F+DLFZP+FZH+FCZ  
AL077F = AL177F+DL17F+ALA77F+LM+MOX  
AM077F = AM177F+DLMTF+AMA77F+MM+MOY  
AN077F = AN177F+DLNTF+ANA77F+NM+MOZ  
IF (AMASS.EQ.0) CALL EXERR (14)  
TMP(1) = 2.\*AMASS1/AMASS  
V777F1 = FX07P/AMASS-QI77R\*W777F+RI77R\*V777F  
U777F1 = FY07P/AMASS-KI77R\*U777F+PI77R\*W777F+TMP(1)\*RI77R\*ALYJDF  
W777F1 = FZ07P/AMASS-PI77R\*V777F+QI77R\*U777F-TMP(1)\*QI77R\*ALZJDF  
AKL1 = AL077F+(AIYYBS-AIZZBS)\*QI77R\*KI77R  
AKM1 = AM077F+(AIZZBS-AIXXBS)\*PI77R\*RI77R  
AKN1 = AN077F+(AIXXBS-AIYYBS)\*PI77R\*QI77R  
IF (INXZS.EQ.0) GO TO 2317  
AKL3 = J.  
AKM3 = U.  
AKN3 = J.  
AKL4 = U.  
AKM4 = L.  
AKN4 = U.  
GO TO 237.  
C2317 23021  
2317 TMP(1) = QI77R\*\*2  
TMP(2) = KI77R\*PI77R  
AKL3 = -AIYYBS \*TMP(2)  
AKM3 = -AIYYBS \*KI77R\*QI77R  
AKN3 = -AIYYBS \*(TMP(1)-PI77R\*\*2)  
AKL4 = AIYZBS \*(TMP(1)-PI77R\*\*2)  
AKM4 = -AIYZBS \*PI77R\*QI77R  
AKN4 = AIYZBS \*PI77R\*PI77R  
C2376 23022  
2370 IF (INXYS.EQ.J) GO TO 2376  
AKL2 = J.  
AKM2 = J.  
AKN2 = J.  
GO TO 2422  
C2376 23023  
2376 AKL2 = AIYZBS\*PI77R\*QI77R  
AKM2 = AIYZBS\*(KI77R\*\*2-PI77R\*\*2)  
AKN2 = -AIYZBS\*QI77R\*RI77R  
C2422 23024  
2422 AKL5 = -AIXXS1\*PI77R+AIXYS1\*QI77R+AIXZS1\*RI77R+AMASS1\*ALLJDF\*\*2\*  
PI77R  
AKM5 = -AIYYS1\*QI77R+AIXYS1\*PI77R+AIYZS1\*RI77R+AMASS1\*ALMJDF\*\*2\*  
QI77R  
AKN5 = -AIZZS1\*RI77R+AIYZS1\*QI77R+AIXZS1\*PI77R+AMASS1\*ALNJDF\*\*2\*  
KI77R  
C2422 23026

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316 IF (INDRPG.NE..1) GO TO 2524
AKL5 = V.
AKM5 = V.
AKN5 = V.
GJ TO 2615
C2524 2524
THTRR = THTRR*1745329
STHTR = JIL(THTRR)
CTHTR = COS(THTRR)
CALL ILU (TIMES,LOC(1),THTRR1)
CALL INTEG (LTHTRR, THTRR1)
THTRD = THTRR*57.2957795
OMGRH = OMGRH*1.4719754
AKL6 = AIXR75*OMGRH*(QI77R+THTRR1)*STHTR
AKM6 = AIXR75*OMGRH*(PI77R+STHTR+RI77R*CTHTR)
AKN6 = AIXR75*OMGRH*(QI77R+THTRR1)*CTHTR
C2615 2615
AKLT = AKL1+AKL2+AKL3+AKL4+AKL5+AKL6
AKMT = AKM1+AKM2+AKM3+AKM4+AKM5+AKM6
AKNT = AKN1+AKN2+AKN3+AKN4+AKN5+AKN6
TMP(1) = AIXXPS
TMP(2) = -AIXYPS
TMP(3) = -AIXZPS
TMP(4) = -AIXYPS
TMP(5) = AIYYPS
TMP(6) = -AIYZPS
TMP(7) = -AIXZPS
TMP(8) = -AIYZPS
TMP(9) = AIZZPS
CALL INVM (TMP(1),TMP(10),INDEP)
IF (INDEP.NE..1) CALL EXCPH (16)
TMP(1) = AKLT
TMP(2) = AKMT
TMP(3) = AKNT
CALL MULT31 (TMP(1),TMP(1),TMP(4))
PI77R1 = TMP(4)
QI77P1 = TMP(5)
RI77P1 = TMP(6)
CALL INTEG (LA(1), U777F1)
CALL INTEG (LA(11), V777F1)
CALL INTEG (LA(12), W777F1)
CALL INTEG (LA(13), PI77R1)
CALL INTEG (LA(14), QI77P1)
CALL INTEG (LA(15), RI77P1)
PI77U = PI77R*57.2957795
QI77U = QI77P*57.2957795
RI77U = RI77P*57.2957795
AL17S1 = PI77R*UCN1-QI77R*UCN2
AL27S1 = RI77R*UCN2-QI77R*UCN3
AL37S1 = RI77R*UCN3-QI77R*UCN1
AM17S1 = PI77R*UCN1-RI77R*UCL1
AM27S1 = PI77R*UCN2-RI77R*UCL2
AM37S1 = PI77R*UCN3-RI77R*UCL3
AN177S = RI77R*UCL1-PI77R*UCM1
AN277S = QI77P*UCL2-PI77R*UCM2
AN377S = QI77P*UCL3-PI77R*UCM3
CALL INTEG (LA(1), AL17S1)
CALL INTEG (LA(2), AL27S1)
CALL INTEG (LA(3), AL37S1)
CALL INTEG (LA(4), AM17S1)
CALL INTEG (LA(5), AM27S1)
CALL INTEG (LA(6), AM37S1)
CALL INTEG (LA(7), AN177S)
CALL INTEG (LA(8), AN277S)
CALL INTEG (LA(9), AN377S)
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O DCL1 = AL1
  DCL2 = AL2
  DCL3 = AL3
  DCM1 = AM1
  DCM2 = AM2
  DCM3 = AM3
  DCN1 = AN1
  DCN2 = AN2
  DCN3 = AN3
  CALL INVR3 (DCL1,TMP(1),INDER)
  IF (INDER.NE.1) CALL EXERR (17)
  CALL TRNPG (TMP(1),TMP(10))
  AL1 = .5*(AL1+TMP(1))
  AL2 = .5*(AL2+TMP(13))
  AL3 = .5*(AL3+TMP(16))
  AM1 = .5*(AM1+TMP(11))
  AM2 = .5*(AM2+TMP(14))
  AM3 = .5*(AM3+TMP(17))
  AN1 = .5*(AN1+TMP(12))
  AN2 = .5*(AN2+TMP(15))
  AN3 = .5*(AN3+TMP(18))
  INDSKP=
  INDCRC = HGC7F,GT, AMAXH
  CALL STGJT (INDSTG)
  IF (SM,OR, HGC7F,GT, J.) RETURN
  INDSKE =
  WRITE (6,1)
  FORMAT (1H,15X,10HSTOP-HGC7F)
  RETURN
C *****
C ENTRY OPT5
C *****
3340 CALL STFL(3,1,HQCI)
  CALL STVAR (A,TIME,TIMES,XG77F,YG77F,HGC7F,U777F,V777F,W777F)
  CALL STVAR (A,PI77R,QI77R,RI77R,AMACH,VA77F,DYNPP,XG77F1,YG77F1)
  CALL STFL(1,1,ZG77F1)
  IF (INDAPC.NE.1) CALL STVAR (2,ALPH0,BETA0,DU,DU,DU,DU,DU,DU)
  IF (INDADJ.EQ.1) GO TO 3341
  ALPH01=ALPH0*.57.2457745
  BETA01=BETA0*.57.2457745
  CALL STVAR (2,ALPH01,BETA01,DU,DU,DU,DU,DU,DU)
3341 IF (INDGSP.NE.0) CALL STFL(1,1,VG77F)
  IF (INDFPA.NE.0) CALL STVAR (2,GAM70,SIG70,DU,DU,DU,DU,DU,DU)
  IF (INDFPD.NE.0) CALL STVAR (2,GAM7R1,SIG7R1,DU,DU,DU,DU,DU,DU)
  IF (INDGRT.NE.0) CALL STVAR (3,THTR0,PSIP0,PHIP0,DU,DU,DU,DU,DU)
  IF (INDACH.EQ.1) CALL STVAR (3,AXP7F,AYP7F,AZP7F,DU,DU,DU,DU,DU)
  IF (INDWGT.NE.0) CALL STFL(1,1,WTR7P)
  IF (INDRMC.NE.0) CALL STFL(1,1,THTR0)
  CALL STVAR (4,FUC,FCX,FCY,FCZ,DU,DU,DU,DU)
  CALL LGEARD
  CALL VPC55
  CALL TFF55
  CALL SAC55
  CALL FLEX5
  CALL STFL(.,1,DU)
  RETURN
C *****
C ENTRY OPT7
C *****
  TIME = DM(3)
  TIMES= DM(3) - TIMSX
  CALL UPDAT (5,LA(1),AL1,AL2,AL3,AM1,AM2)
  CALL UPDAT (5,LA(6),AM3,AN1,AN2,AN3,U777F)
  CALL UPDAT (5,LA(11),V777F,W777F,PI77R,QI77R,RI77R)

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CALL UPDAT (3,LA(16),*GZ7F,YG7F,ZG7F,DU,DU)
IF (INDHMC.NE.0) CALL UPDAT (1,LT,TRQ,THRP,DU,DU,DU,CUI)
CALL LGCA7
CALL VPCS7
CALL TFF7
CALL SACS7
CALL FLEX7
RETURN
END
SUBROUTINE LGCA7
COMMON/DIRCOM/OM1(136),AMASS,OM2(147),OCL1,OCM1,
COCN1,OCL2,OCM2,OCN2,OCL3,OCM3,OCN3,OM3(99),FX07F,
CUMH4(3),FY07F(4),FZ07F,IM5(17),GX07F,UM6(8),GZ07F,
CUM7(218),INOUTE(235),
CTIME,OM8(287),PI77R(2),PI77R1(2),OM9(4),
CQI77R(2),RI77R1(2),OM1(4),RI77R(2),RI77R1(2),OM11(48),
CXG77F(2),YG77F(2),YG77F1(2),YG77F2(2),
CZG77F(2),ZG77F1(2),DUM(3(5)),
CNSTRUT,MASS(5),RX(5),RY(5),RZ(5),THETAU(5),ERDEG,RGR,
CNTIRES(5),ZLR0(5),W(5),DELTAM(5),MOMENT(5),
CRF(5),VZ,IFD,PZCNO(5),VZLFO(5),A(5),PZL(5),VZL(5),
CAL(5),ILL(5),SLT(5),SL2(5),CLL(5),HASS2(5),MUS(5),
CCL(5),CL(5),C2C(5),CZL(5),NVGPT,NRP,MD(5),PLT,NDELTA,
C(5),S(5),S01(2),S021(2),S022(2),S023(2),S024(2),S025(2)
COMMON/DIRCOM/
CSU1(2),S1(2),S013(2),S014(2),S015(2),
CS2(2),S2(2),S3(2),S4(2),S5(2),
CS021(2),S022(2),S023(2),S024(2),S025(2),
CS2011(2),S2012(2),S2013(2),S2014(2),S2015(2),
CS22(2),S22(2),S23(2),S24(2),S25(2),
CMTU11(2),CMTU12(2),CMTU13(2),CMTU14(2),CMTU15(2),
CMT1(2),CMT2(2),CMT3(2),CMT4(2),CMT5(2),
CAI(5),U1(5),ULLFA1,ULLFA2,ULLFA3,ULLFA4,DELTAS,
CDELT1,DOELT2,DOELT3,DOELT4,DOELT5,ISTAGE,
CPRTH1,PLT,ISUP,ISTPL1,ISTPL2,ISTPL3,ISTPL4,ISTPL5,
CUM14(22),I0(5),OM10(127),INULG,OM15(117),CASK(44),
*OM17,NMODL,UM14(4),SXMOD(166),SYMOD(166),SZMOD(166),OM19(1686),
*GJ02(2),OLMR(2)
REAL MASS,MOMENT,MASS2,MUS,NTIRES,MR
DIMENSION ULGAUT(1),ULGDE(47),OLL(7),OLGE(299)
COMMON/LGAUTSZ/ARG1,ARG13,ARG31,ARG33,AMA(5),VAXLE(5)
COMMON/LGJL/LA(25),FC2(5),PC(5),PRES(5),C(5),IPPT,LTF
COMMON/LGZ/FX,FY,FZ,LH,MH,NH,EPSLO2
COMMON/LGZ/A11(5),A12(5),A31(5),A33(5),RRGX(5),
CRL(5,3),X1(3,3,5),YAX(5),YAY(5),RAZ(5),TMP(3),ZZERO(5),
CX(5),YR(5),EPSLUN(5),PA(5),FDELTA(5),
CFTRZ(5),RJA(5),RUY(5),R07(5),RUXG(5),RUYG(5),RUZG(5),
CVTX(5),VTY(5),VTZ(5),LZ(5),VGPT(5),FTRX(5),FTRY(5),
CDX(5),DY(5),DZ(5),F1(5),FOX(5),FDY(5),FF(5),AA(5),C2(5),
CJX(5),SF(5),PSKD(5),HUVF(5),MTRX(5),MTRY(5),
CMT7(5),MA(5),RG11,RG13,PG31,PG33,IPRT,
CFTR,MTRY,MTZ,SFTRX,SFTRY,SFTRZ,FTRA,
CFTRA,FTRC,SMTRX,SMTRY,SMTRZ
COMMON/ELKUPZ/GEORC(100),GEORC3(100),GEORC4(100),BH1(308)
EQUIVALENCE (ULGAUT(1),ARG11),(ULGDE(1),LA(1)),
*(3LG(1),FKM),(OLGE(1),A11(1))
COMMON/TABZ/PC/QUH4(1,3),LOC(7)
COMMON/HTCOM/HT,HT2,HT3
REAL HUVF,MTRX,MTRY,MTRZ,MA,
CMTX,MTRY,MTZ,LH,MH,FM
DIMENSION DELTA(5),DOELTA(5),P(5),
C(S02(2,5),S01(2,5),S(2,5),S202(2,5),S201(2,5),S2(2,5),
COMETD1(2,5),OMET(2,5)
EQUIVALENCE (P(1),PRES(1))
EQUIVALENCE (DELTA(1),DELTA1),(DOELTA(1),DOELT1)

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C EQUIVALENCE
C (SD21(1),SD2(1,1)),(SD11(1),SD1(1,1)),(S1(1),S(1,1)),
C (SZ21(1),SZ2(1,1)),(SZD11(1),SZD1(1,1)),(S21(1),S2(1,1)),
C (OMT1(1),OMT(1,1)),(OMT1(1),OMT(1,1))
C PRE DATA INITIALIZATION
DO 1 I=1,4
  OLGAUT(I)=0.
DO 2 I=1,4
  OLGUE(I)=0.
DO 3 I=1,7
  OLC(I)=0.
DO 4 I=1,299
  OLG(I)=0.
I=STAGE=J
IPLT=0
IPPT=0
LTPT=1
ISDF=0
ISTPL1=0
ISTPL2=0
ISTPL3=0
ISTPL4=0
ISTPL5=0
CPSLO2=J.
RETURN
*****
C ENTRY LGEAR2
C *****
FXH=0.
FYH=0.
FZH=0.
LM=J.
MM=J.
NM=J.
ERR=J1745329*ERDEG
RG11=COS(ERR)
RG13=-SIN(ERR)
RG31=-RG13
RG33=RG11
ARG11=RG11
ARG13=RG13
ARG31=RG31
ARG33=RG33
IF (INDLG.EQ.1) RETURN
INITIALIZATION AFTER DATA READ IN
VARIABLES TO BE INTEGRATED
      (OMT11,OMT1 )
      (OMT12,OMT2 )
      (OMT13,OMT3 )
      (OMT14,OMT4 )
      (OMT15,OMT5 )
      (SU21 ,SU11 )
      (SU22 ,SU12 )
      (SU23 ,SU13 )
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      (SU23 ,SU13 )
      (SU24 ,SU14 )
      (SU25 ,SU15 )
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      (SD13 ,S3 )
      (SD14 ,S4 )
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DO 10 I=1,NSTRUT
  THETAR=.1745329*THETAD(I)
  A11(I)=COS(THETAR)
  A13(I)=-SIN(THETAR)
  A31(I)=A13(I)
  A33(I)=A11(I)
10  RCGX(I)=A11(I)*RX(I)+A13(I)*RZ(I)
  IPRT=
  RETURN
*****
C
C  INITIAL PRINT
C  ENTRY LG 3-4
C  *****
C
C  RETURN
C  *****
C
C  ENTRY LG 4-5
C  *****
C
C  MAIN COMPUTATIONAL AREA
C  RL MATRIX ELEMENTS
C  IF (INULG.EQ.1) RETURN
C  RL(1,1)=JCL1*RG11+JCL3*RG13
C  RL(1,2)=JCL2
C  RL(1,3)=JCL1*RG31+JCL3*RG33
C  RL(2,1)=JCN1*RG11+JCN3*RG13
C  RL(2,2)=JCN2
C  RL(2,3)=JCN1*RG31+JCN3*RG33
C  RL(3,1)=JCN1*RG11+JCN3*RG13
C  RL(3,2)=JCN2
C  RL(3,3)=JCN1*RG31+JCN3*RG33
C
C  CALL LG 4-5
C  CALCULATION OF S201, AND S2
C  DO 10 I=1,NSTRUT
C  IF (INULG.EQ.2) GO TO 2.
C  IF (IL.NE.1) GO TO 59
C  TMP(1)=S201(1,I)-A2(I)*S201(1,I)/A(I)
C  S202(1,I)=(P(I)-PL(I))*A2(I)+C/I)*TMP(1)*ABS(TMP(1))
C  S201(1,I)=(C2(I)*ABS(S201(1,I))+C2L(I)))
C  MASS2(1,I)*C2(I)-SR(I)+S202(1,I)
C  HT2=HT
C  IF (S201(1,I).GE.87.88
C  TTIME=S2(1,I)/ABS(S201(1,I))
C  IF (TTIME.GE.HT) GO TO 87
C  HT2=TTIME
C  GO TO 87
C  TTIME=(S2(I)-S2(1,I))/S201(1,I)
C  GO TO 89
C  CONTINUE
C  IF (S2(1,I).GT.(-ES2(I))) GO TO 59
C  WRITE(6,57) I, S2(1,I)
C 57  FORMAT(58X,5H-ES2(,I,4H) EXCEEDED/
C 58X,3HS2(,I,4H) = E16.7)
C  IF (S2(1,I).LE.ES2(I)) GO TO 61
C  IF (S2(1,I).LE.(S2(I)-ES2(I))) GO TO 141
C  IF (S2(1,I).LE.(S2(I)+ES2(I))) GO TO 62
C  WRITE(6,55) I, S2(1,I)
C 55  FORMAT(58X,5H-ES2(,I,4H) EXCEEDED/
C 58X,3HS2(,I,4H) = E16.7)
C  IF (S201(1,I).GT.0.) S201(1,I)=0.
C  IF (S202(1,I).LT.0.) GO TO 141
C  GO TO 141
C  IF (S201(1,I).LT.0.) S201(1,I)=0.
C  IF (S202(1,I).LT.0.) GO TO 141
C  FC2(I)=0.
C  GO TO 60
C  FC2(I)=-MASS2(I)*S202(1,I)

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O  S202(1,I)=..
GO TO 65
59 S202(1,I)=..
S201(1,I)=..
S2(1,I)=..
FC2(1)=-P(I)-P2(I))*A2(I)-C(I)*S01(1,I)*ABS(S01(1,I))
GO TO 94
60 CONTINUE
I1=2*I+J*NSTRUT-1
I2=I1+1
CALL INTEG(LA(I1),S202(1,I))
CALL INTEG(LA(I2),S201(1,I))
94 CONTINUE
C COMPUTATION OF AA(I)
TMP(1)=..
IF(S01(1,I).NE.0.)TMP(2)=S01(1,I)/ABS(S01(1,I))
SF(I)=-P(I)*A(I)-A2(I))-P2(I)*A2(I)+FC2(I)-S201(1,I)*
C(C2(I)*ABS(S201(1,I))+C2L(I))-FF(I)*TMP(2)
AA(I)=(FY(I)+SF(I))/MASS(I)
C CALCULATION OF S02, S01, AND S
C CALCULATION OF OME1(I) AND OME2(I)
S02(1,I)=SK(I)+AA(I)-GZ(I)
HT1=HT
IF(S01(1,I)176,77,78)
76 TTIME=S(1,I)/ABS(S01(1,I))
79 IF(TTIME.GE.HT)GO TO 77
HT1=TTIME
GO TO 77
78 TTIME=(S(I)-S(1,I))/S01(1,I)
GO TO 73
77 CONTINUE
IF(S(1,I).GT.(-ES(1)))GO TO 50
WRITE(6,44)I,I,S(1,I)
49 FORMAT(58X,4H-ES(1,1)H) EXCEEDED/
C58X,4H-ES(1,1)H) = E15.7)
50 IF(S(1,I).LE.-ES(1))GO TO 51
IF(S(1,I).LE.(SH(I)-ES(1)))GO TO 55
IF(S(1,I).LE.(SH(I)+ES(1)))GO TO 52
WRITE(6,53)I,I,S(1,I)
53 FORMAT(58X,4H-ES(1,1)H) EXCEEDED/
C58X,4H-ES(1,1)H) = E15.7)
52 IF(S01(1,I).GT.0.)S01(1,I)=0.
IF(S02(1,I).LT.0.)GO TO 55
S02(1,I)=..
GO TO 55
51 IF(S01(1,I).LT.0.)S01(1,I)=..
IF(S02(1,I).LT.0.)S02(1,I)=0.
55 CONTINUE
I2=2*I+NSTRUT-1
I1=I2+1
CALL INTEG(LA(I2),S02(1,I))
CALL INTEG(LA(I1),S01(1,I))
20 TMP(1)=42*PU(I)-DELTA(I)
IF(CASK(I).GT.1.E-15)GO TO 200
MA(I)=-FTRY(I)*TMP(1)*RI(2,1,I)+FTRX(I)*TMP(1)
C*41(2,2,I)
GO TO 201
200 MA(I)=TMP(1)*SQRT(FTRY(I)*FTRY(I)+FTRX(I)*FTRX(I))
MA(I)=SIGN(MA(I),-VAXLE(I)-OMET(1,I)*TMP(1))
201 MA(I)=MA(I)
IF(INULG.EQ.2)GO TO 100
IF(IB(I).NE.(-1))GO TO 48
OMET(1,I)=..
OMET(1,I)=..
GO TO 21

```



```

1  TMP(1)=J.
   IF (OR(T11, I).NE.L.) TMP(1)=OMET(1, I)/ABS(OMET(1, I))
   OMETU(1, I)=(MA(I)-MB(I)*TMP(1))/NTIRES(I)*MOMENT(I)
21  CALL INTL(LA(I), OMETU(1, I))
100 CONTINUE
C  CALCULATION OF FTRA, FTRB, AND FTRC
   SFTX=.
   SFTY=.
   SFTZ=.
   DO 70 I=1, NSTRUT
   SFTX=SFTX+FTHX(I)
   SFTY=SFTY+FTHY(I)
   SFTZ=SFTZ+FTHZ(I)
70  FTRA=RL(1,1)*SFTX+RL(1,2)*SFTY+RL(1,3)*SFTZ
   FTRB=RL(2,1)*SFTX+RL(2,2)*SFTY+RL(2,3)*SFTZ
   FTRC=RL(3,1)*SFTX+RL(3,2)*SFTY+RL(3,3)*SFTZ
C  CALCULATION OF MTX, MTY, AND MTZ
   SMTX=.
   SMTRY=.
   SMTRZ=.
   DO 75 I=1, NSTRUT
   SMTX=SMTX+MTX(I)
   SMTRY=SMTRY+MTY(I)
   SMTRZ=SMTRZ+MTZ(I)
75  MTX=RL(1,1)*SMTX+RL(1,2)*SMTRY+RL(1,3)*SMTRZ
   MTY=RL(2,1)*SMTX+RL(2,2)*SMTRY+RL(2,3)*SMTRZ
   MTZ=RL(3,1)*SMTX+RL(3,2)*SMTRY+RL(3,3)*SMTRZ
C  CALCULATION OF FXM, FYM, FZM, LHM, MM, AND NM
   FYM=.
   FZM=.
   FXM=.
   LHM=.
   MM=.
   NM=.
   BFX=.
   BFY=.
   BFZ=.
   BLM=.
   BMM=.
   BNM=.
   DO 80 I=1, NSTRUT
   OFXM=.
   OFYM=.
   OFZM=.
   OLM=.
   OMM=.
   ONM=.
   DO 14 IL4=1, NMODE
   NBB=(IL4-1)*NSTRUT+1
   OFXM=OFXM+MASS(I)*SXMOD(NBB)*GQD2(IL4)
   OFYM=OFYM+MASS(I)*SYMOD(NBB)*GQD2(IL4)
   OFZM=OFZM+MASS(I)*SZMOD(NBB)*GQD2(IL4)
   NBM=(I-1)*NMODE+IL4
   OLM=OLM+MASS(I)*GFOPC2(NBM)*GQD2(IL4)
   OMM=OMM+MASS(I)*GFOPC3(NBM)*GQD2(IL4)
   ONM=ONM+MASS(I)*GFOPC4(NBM)*GQD2(IL4)
14  BFX=OFX+OFXM
   BFY=OFY+OFYM
   BFZ=OFZ+OFZM
   BLM=OLM+OLM
   BMM=OMM+OMM
   BNM=ONM+ONM
   TMP(1)=MASS(I)*GDZ(1, I)
   FXM=FXM+TMP(1)*A31(I)
   FYM=FYM

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FZH=FZH+TMP(1)*A33(I)
LH=LH+TMP(1)*A11(I)*RY(I)
MH=MH+TMP(1)*RRCGX(I)
NH=NH+TMP(1)*A13(I)*RY(I)
FXM=FXM+BFX+FTRA
FYM=FYM+IFY+FTRB
FZM=FZM+BFZ+FTRC
LH=LH+ULH+MTX
MH=MH+UHH+MTY
NH=NH+UHH+MTZ
RETURN
END
SUBROUTINE LGFA3C
COMMON/DIRCOM/CM1(136),AMASS,DM2(147),DCL1,DCM1,
COCN1,DCL2,UCH2,DCN2,DCL3,UCH3,DCN3,DM1(199),FX07P,
COUM4(13),FY07P(4),FZ07P,UM5(17),GX07F,DM6(8),GZ07F,
COM7(186),INDC1,INDC2,INDC3,INDC4,DM15(28),INOSTE,DM18(234),
CTIME,CM8(287),PI77K,DM10,PI77Z,DM9(5),
QI77R,DM4,QI77R1,DM1(5),PI77C,DM17,R177R1,DM11(49),
CXG77F,DM1,XG77F,DM2(11),YG77F,DM21,YG77F1,DM22(11),
CZG77F,DM3,ZG77F1,DM13(46),NSMAIN,NSNDY(6),
CMTHUT,MASS(5),RX(5),RY(5),RZ(5),THETA(5),ERDEC,RGR,
CNTIRES(5),ZZERO(5),M(5),DELTA(5),MOMENT(5),
CPF(5),VZ,IFD,PZERO(5),VZERO(5),A(5),P2(5),V2(5),
GA2(5),IL,S2(5),ESC(5),C2L(5),MASS2(5),MUS(5),
CCC(5),CE(5),C2C(5),CE(5),NVGPT,NPP,MB(5),RLT,NDELTA,
CES(5),SB(5),SU2(2),SU22(2),SD23(2),SD24(2),SD25(2)
COMMON/DIRCOM/
CSD11(2),SD12(2),SD13(2),SD14(2),SD15(2),
CS1(2),SS2(2),SS1(2),SS4(2),SS5(2),
CS2D21(2),SD22(2),SD23(2),SD24(2),SD25(2),
CS2011(2),SD22(2),SD23(2),SD24(2),SD25(2),
CS2(2),SD2(2),SD3(2),SD4(2),SD5(2),
COMTJ11(2),OMT012(2),OMT013(2),OMT014(2),OMT015(2),
COMT1(2),OMT2(2),OMT3(2),OMT4(2),OMT5(2),
CAI(5),UL(5),DELTA1,DELTA2,DELTA3,DELTA4,DELTA5,
DOELT1,DOELT2,DOELT3,DOELT4,DOELT5,ISTAGE,
CPMTMIN,IPL1,ISCF,ISTPL1,ISTPL2,ISTPL3,ISTPL4,ISTPL5,
COM14(262),CASK(5),DM25(39),DM26,NMODE,DM27(40),SXMOU(100),
*SYMOU(100),SZMOD(1,1),DM28(164),GQ(20),GQD1(2),GQD2(20),
*DM29(2)
REAL MASS,MOMENT,MASS2,MUS,NTIRES,MB
COMMON/LGAUTS/ARG11,ARG13,ARG31,ARG33,AMA(5),VAXLE(5)
COMMON/LGDE/LA(29),FC2(5),P2(5),PRES(5),C(5),IPPT,LIPT
COMMON/LG/FXP,FYM,FZM,LH,MH,NH,EPSLO2
COMMON/LG/A1(5),A13(5),A31(5),A33(5),RRCGX(5),
CRL(3,3),RI(3,3,5),WAX(5),RAY(5),RAZ(5),TMP(3),ZZERO(5),
CX(5),YR(5),EPSLOM(5),PA(5),FDELTA(5),
CFTRZ(5),ROX(5),ROY(5),ROZ(5),ROXG(5),ROYG(5),ROZG(5),
CVTX(5),VTY(5),VTZ(5),GZ(5),VGPT(5),FTRX(5),FTRY(5),
CDX(5),UY(5),DZ(5),FT(5),FDX(5),FDY(5),FF(5),AA(5),C2(5),
CSR(5),SF(5),PSKO(5),HUV(5),MTX(5),MTY(5),
CMTRZ(5),MA(5),RG11,RG13,RG31,RG33,IPRT,
CMTX,MTY,MTZ,SFTRX,SFTRY,SFTRZ,FTRA,
CFTRB,FTRC,SMTRX,SMTRY,SMTRZ
COMMON/TAJPC/DOUMH1(1,3),LOC(7)
REAL HUV,MTX,MTY,MTZ,MA,
CMTX,MTY,MTZ,LH,MH,NH
DIMENSION DELTA(5),ODELTA(5),P(5),
CSD2(2,5),SD1(2,5),S(2,5),SD2(2,5),SD1(2,5),S2(2,5),
COMETD1(2,5),OMET(2,5)
DIMENSION TEMP1(3),TEMP2(3)
EQUIVALENCE (P(1),PRES(1))
EQUIVALENCE (DELTA(1),DELTA1),(ODELTA(1),ODELT1)
EQUIVALENCE

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C(S202(1,1),S202(1,1)),(S011(1,1),S011(1,1)),(S1(1,1),S1(1,1)),
C(S202(1,1),S202(1,1)),(S2011(1,1),S2011(1,1)),(S21(1,1),S21(1,1)),
C(OMT01(1,1),OMT01(1,1)),(OMT1(1,1),OMT1(1,1))
DO 11 I=1,NSTRUT
  FI=1
  RI MATRIX ELEMENTS
  DO 2 J=1,3
    TEMP1(J)=0.
    TEMP2(J)=0.
    RI(1,J,I)=A11(I)*RL(1,J)+A13(I)*RL(3,J)
    RI(2,J,I)=RL(2,J)
    RI(3,J,I)=A31(I)*RL(1,J)+A33(I)*RL(3,J)
  2J POSITION DEPENDENT CALCULATIONS
  DO 11 ILP=1,NMCOL
    MOD=ILP-1,NSTRUT+1
    TEMP1(1)=TEMP1(1)+SX*MOD(MOD)*GQ(ILP)
    TEMP1(2)=TEMP1(2)+LY*MOD(MOD)*GQ(ILP)
    TEMP1(3)=TEMP1(3)+SZ*MOD(MOD)*GQ(ILP)
  11 TEMP(1)=RF(1)-S(1,I)
    TEMP(2)=RX(1)+A11(I)*TEMP(1)+TEMP1(1)
    TEMP(3)=RX(1)+A13(I)*TEMP(1)+TEMP1(3)
    RAX(I)=JCL1*TEMP(2)+DCN1*(RY(I)+TEMP1(2))+DCN1*TEMP(3)
    RAY(I)=JCL2*TEMP(2)+JCM2*(PY(I)+TEMP1(2))+DCN2*TEMP(3)
    RAZ(I)=JCL3*TEMP(2)+DCN3*(KY(I)+TEMP1(2))+DCN3*TEMP(3)
    TMP(1)=(X/77F-RGP+RAX(I))
    TMP(2)=Z/77F+RAY(I)
    ZZERO(I)=TMP(1)*RG31+TMP(2)*RG13
    XR(I)=TMP(1)*DU1+TMP(2)*RG13
    YR(I)=Y/77F+RAY(I)
    IF(XR(I).LE.0.)GO TO 25
    IF(XR(I).GE.0.)GO TO 25
    CALL TLU(XR(I),LOC(2),EPSLON(I))
    GO TO 24
  25 EPSLON(I)=0.
  24 DELTA(I)=ZZERO(I)+ZZERO(I)+EPSLON(I)
    DDDELTA(I)=DELTA(I)
    IF(DELTA(I).LE.0.)GO TO 26
    IF(DELTA(I).LE.DELTA(I))GO TO 27
  26 FORMAT(36X,24HTIME DEFLECTION EXCEEDED,10X,6HDELTA(,I1,4H) = ,
  26 C(1,5,7)
    CALL LEASP
    INDSY=0
    RETURN
  26 DELTA(I)=0.
  27 CONTINUE
    P(I)=PZERO(I)*VZERO(I)/(VZERO(I)+A2(I)*S2(1,I)-
    CS(1,I)*u(I))
    P2(I)=0.
    TMP(1)=V2(I)-A2(I)*S2(1,I)
    IF(TMP(1).EQ.0.)GO TO 31
    P2(I)=P2(I)*V2(I)/TMP(1)
  31 IF(IFO.0.)GO TO 32
    FDELTA(I)=0.
    IF(DELTA(I).NE.0.)FDELTA(I)=AI(I)*(DELTA(I))*BI(I)
    GO TO 33
  32 CALL HINC(3,LOC(1),NDELTA,NSTRUT,DU,DU,DELTA(I),FI,DU,DU,FDELTA(I))
  33 FTRZ(I)=-RTIFES(I)*FDELTA(I)
  C CALCULATION OF COMPONENTS OF GROUND PLANE
  C VELOCITIES VTX(I) AND VTY(I)
    TMP(1)=(RF(1)-S(1,I))
    DO 12 IL2=1,NMCOL
      NO=(IL2-1)*NSTRUT+1
      TEMP2(1)=TEMP2(1)+(Q177R*SZMOD(NO)-R177R*SYMOD(NO))*GQ(IL2)

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C+SYMOD(ND)*GQD1(IL2)
TEMP2(2)=TEMP2(2)+RI77R*SYMOD(ND)-PI77R*SZMOD(ND)*GQ(IL2)
C+SYMOD(ND)*GQD1(IL2)
12 TEMP2(3)=TEMP2(3)+(PI77R*SYMOD(ND)-QI77R*SYMOD(ND))*GQ(IL2)
C+SZMOD(ND)*GQD1(IL2)
RDX(I)=-SU1(1,I)*A31(I)+QI77R*(TMP(1)*A33(I)+RZ(I))-RI77R
C*RY(I)+TEMP2(1)
ROY(I)=TMP(1)*(RI77R*A31(I)-PI77R*A33(I))+RI77R*RX(I)-PI77R
C*RZ(I)+TEMP2(2)
RDZ(I)=-SU1(1,I)*A33(I)-TMP(1)*QI77R*A31(I)+PI77R*RY(I)-QI77R
C*RX(I)+TEMP2(3)
RDXG(I)=XG77F1+UCL1*ROX(I)+DCM1*ROY(I)+DCN1*RDZ(I)
RJOY(I)=YG77F1+UCL2*ROX(I)+DCM2*ROY(I)+DCN2*RDZ(I)
RDZG(I)=ZG77F1+UCL3*ROX(I)+DCM3*ROY(I)+DCN3*RDZ(I)
TMP(1)=RZLRO(I)-DELTA(I)
TMP(2)=OMET(1,I)*RI(2,2,I)*TMP(1)
TMP(3)=OMET(2,I)*RI(2,1,I)*TMP(1)
VTX(I)=RG11*ROXG(I)+RG13*RDZG(I)+TMP(2)
VTY(I)=ROYG(I)-TMP(3)
VTZ(I)=RG31*ROXG(I)+RG33*RDZG(I)
C CALCULATION OF GROUND PLANE FORCES FTRX(I) AND FTRY(I)
TMP(1)=RG11*ROXG(I)+RG13*RDZG(I)
VAXLE(I)=SQRT(TMP(1)*TMP(1)+ROYG(I)*ROYG(I))
IF(CASK(I).GT.1.E-10)GO TO 34
VGPT(I)=SQRT(VTX(I)*VTX(I)+VTY(I)*VTY(I))
GO TO 35
34 TMP(1)=VAXLE(I)+OMET(1,I)*(RZLRO(I)-DELTA(I))
VGPT(I)=ABS(TMP(1))
35 IF(VGPT(I).LE.VZ)GO TO 40
PSKL(I)=J.
IF(ABS(VAXLE(I)).LE.1.E-8)GO TO 42
PSKL(I)=VGPT(I)/VAXLE(I)
42 CALL FLU(PSKL(I),LOC(3),MUVP(I))
FTRX(I)=MUVP(I)*FTRZ(I)/VGPT(I)
IF(CASK(I).GT.1.E-10)GO TO 50
TMP(3)=VTY(I)
GO TO 51
50 TMP(3)=(VTY(I)+TMP(3))/VAXLE(I)*TMP(1)
51 FTRY(I)=FTRX(I)*TMP(3)
IF(CASK(I).GT.1.E-10)GO TO 52
TMP(2)=VTX(I)
GO TO 53
52 TMP(2)=(VTX(I)+TMP(2))/VAXLE(I)*TMP(1)
53 FTRX(I)=FTRX(I)*TMP(2)
GO TO 41
40 FTRX(I)=J.
FTRY(I)=J.
41 CONTINUE
C CALCULATION OF MTRX(I), MTRY(I), AND MTRZ(I)
OX(I)=RG11*ROX(I)+RG13*RAZ(I)
OY(I)=RAY(I)
OZ(I)=RG31*ROX(I)+RG33*RAZ(I)+RZLRO(I)-DELTA(I)
MTRX(I)=OY(I)*FTRZ(I)-OZ(I)*FTRY(I)
MTRY(I)=OZ(I)*FTRX(I)-OX(I)*FTOZ(I)
MTRZ(I)=OX(I)*FTRY(I)-OY(I)*FTRX(I)
C CALCULATION OF FT(I)
FT(I)=-FTRX(I)*RI(3,1,I)-FTRY(I)*RI(3,2,I)
C-FTRZ(I)*RI(3,3,I)
C CALCULATION OF FF(I)
FDX(I)=RI(1,1,I)*FTRX(I)+RI(1,2,I)*FTRY(I)+RI(1,3,I)*FTRZ(I)
FDY(I)=RI(2,1,I)*FTRX(I)+RI(2,2,I)*FTRY(I)+RI(2,3,I)*FTRZ(I)
FF(I)=MUS(I)*SQRT(FDX(I)*FDX(I)+FDY(I)*FDY(I))
C CALCULATION OF GZ(I)
TMP(3)=-AZ(I)/A(I)
C(I)=0.

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O 1 DO 1 I=1,40
    GMASS(I)=J.
    DO 2 I=1,25
    SMASS(I)=J.
    RZA11(I)=J.
    RXA11(I)=J.
    2 RKSY(I)=J.
    DO 15 I=1,40
    15 LA(I)=J.
    NMODE=1
    RETURN

C
C ENTRY FLEX2

C
C IF(INDFLEX.EQ.0.OR.INDLG.EQ.0) RETURN
HT=AMINER
NVAR=2*NMODE
CALL INUPD(NVAR,LA)

C
C FORMULATE TIME INVARIANT ARRAYS
C FORM COUPLED GENERALIZED MASS MATRIX

DO 30 K=1,NMODE
NA=(K-1)*NMODE+K
30 GMASS(NA)=GMASS1(K)
DO 31 N=1,NSTRUT
LLA=(N-1)*NSTRUT+N
31 SMASS(LLA)=MASS(N)
CALL GTPRO(SXMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GMPRO(SXMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GHAUJ(GSMOD,GMASS,GMASS,NMODE,NMODE)
CALL GTPRO(SYMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GMPRO(SYMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GHAUJ(GSMOD,GMASS,GMASS,NMODE,NMODE)
CALL GTPRO(SZMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GMPRO(SZMOD,SMASS,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GHAUJ(GSMOD,GMASS,GMASS,NMODE,NMODE)
CALL AXY(1,NMCUE,NMODE,2L,2J,GMASS,COPHAS)
CALL DECOMP(NMCUE,COPHAS,COEF)

C
C FORM CONSTANT COMPONENTS OF TANGENTIAL ACCELERATION

CALL GTPRO(SXMOD,MASS,QS,NSTRUT,NMODE,1)
CALL GTPRO(SYMOD,MASS,QS,NSTRUT,NMODE,1)
CALL CTIE(QS,QS1,CTMP1,NMODE,1,0,0,1)
CALL GTPRO(SZMOD,MASS,QS,NSTRUT,NMODE,1)
CALL CTIE(CTMP1,QS,GFORC1,NMODE,2,0,0,1)
DO 33 L=1,NSTRUT
DIFF(L)=KF(L)-SKC(L)
MA=(L-1)*NSTRUT+L
RZA11(MA)=RZ(L)+DIFF(L)*A11(L)
RXA11(MA)=RX(L)-DIFF(L)*A11(L)
33 RKSY(MA)=RY(L)
CALL GTPRO(SZMOD,RKSY,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GTPRO(SYMOD,RZA11,GSMOD,NSTRUT,NMODE,NSTRUT)
CALL GMSUB(CTMP1,GSMOD,GFORC2,NMODE,NSTRUT)
CALL GTPRO(SXMOD,RZA11,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GTPRO(SZMOD,RXA11,GSMOD,NSTRUT,NMODE,NSTRUT)
CALL GMSUB(CTMP1,GSMOD,GFORC3,NMODE,NSTRUT)
CALL GTPRO(SYMOD,RXA11,CTMP1,NSTRUT,NMODE,NSTRUT)
CALL GTPRO(SXMOD,RKSY,GSMOD,NSTRUT,NMODE,NSTRUT)
CALL GMSUB(CTMP1,GSMOD,GFORC4,NMODE,NSTRUT)

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# FORM INITIAL DISPLACEMENTS

```

SUM1=0.
SUM3=0.
DO 34 I=1,NSTRUT
  SUM1=SUM1+A31(I)*SUD((I-1)*2+1)
  SUM3=SUM3+A33(I)*SUD((I-1)*2+1)
34 VARY1(I)=AX77F-SUM1
  VARY1(I)=AY77F
  VARY1(I)=AZ77F-SUM3
  CALL GMPRO1(GFONC1,VARY1,QS,NMODE,3,1)
  DO 35 I=1,NSTRUT
    OMXD1M(I)=PI77F1*MASS(I)
    OMYD1M(I)=PI77F1*MASS(I)
    OMZD1M(I)=PI77F1*MASS(I)
35 CALL GMPRO1(GFONC2,OMXD1M,GF,NMODE,NSTRUT,1)
    CALL GMAJ1(QS,GF,2S,NMODE,1)
    CALL GMPRO1(GFONC3,OMYD1M,GF,NMODE,NSTRUT,1)
    CALL GMAJ1(QS,GF,2S,NMODE,1)
    CALL GMPRO1(GFONC4,OMZD1M,GF,NMODE,NSTRUT,1)
    CALL GMAJ1(QS,GF,2S,NMODE,1)
    CALL GTPRO1(TXMC0,T,GF,IN,NMODE,1)
    CALL GMSU1(GF,QS,QS,NMODE,1)
    FOC(1)=FCX
    FOC(2)=FCY
    FOC(3)=FCZ
    CALL GTPRO1(GCHQUE,FOC,GF,3,NMODE,1)
    CALL GMAJ1(GF,2S,QS,NMODE,1)
    DO 36 I=1,NMODE
      NH=(I-1)*5+1
      CTMP1(NH)=-ARMODE(NH)*AA77P
      CTMP1(NH+1)=ARMODE(NH+1)*YA77P
      CTMP1(NH+2)=-ARMODE(NH+2)*ANA77P
      CTMP1(NH+3)=ARMODE(NH+3)*ALA77F
      CTMP1(NH+4)=ARMODE(NH+4)*AMA77F
      CTMP1(NH+5)=ARMODE(NH+5)*ANAZ7F
36 DO 37 II=1,NMODE
      GF(II)=0.
      DO 37 JJ=1,5
        MJ=(II-1)*5+JJ
        GF(II)=GF(II)+CTMP1(MJ)*PF(MJ)
37 CALL GMAJ1(GF,QS,QS,NMODE,1)
      DO 38 IG=1,NMODE
        GTF(IG)=GMASS1(IG)*GFREQ(IG)**2.
38 GJ(IG)=QS(IG)/GTF(IG)
      SKIPUP=.7RUE
      DO 39 I=1,NMODE
        NZZ=2*1
        CALL UPDAT(1,LA(NZZ),GQ(I),DU,DU,DU,DU)
39 CONTINUE
      SKIPUP=.FALSE.
      RETURN
C
C ENTRY FLEX3
C
C IF(INOFLX.EQ.2.OR.INOIG.EQ.0)RETURN
C
C FORM VARYING COMPONENTS OF TANGENTIAL ACCELERATION
C
SUM1=0.
SUM3=0.
DO 40 I=1,NSTRUT
  SUM1=SUM1+A31(I)*SUD((I-1)*2+1)
  SUM3=SUM3+A33(I)*SUD((I-1)*2+1)
40 VARY1(I)=AX77F-SUM1

```



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C VARY1(1)=AY77F
  VARY1(3)=AZ77F-SUM3
  CALL GMPRJ(GFORC1,VARY1,GTF,NMODE,3,1)
  DO 46 I=1,NMODE
46  QS(I)=0.
    CALL GMSUB(QS,GTF,QS,NMODE,1)
    DO 41 I=1,NSTRUT
      OMXD1M(I)=PI77R1*MASS(I)
      OMYD1M(I)=QI77R1*MASS(I)
41  OMZD1M(I)=R177R1*MASS(I)

C    CALL GMPRJ(GFORC2,OMXD1M,GTF,NMODE,NSTRUT,1)
    CALL GMSUB(QS,GTF,QS,NMODE,1)
    CALL GMPRJ(GFORC3,OMYD1M,GTF,NMODE,NSTRUT,1)
    CALL GMSUB(QS,GTF,QS,NMODE,1)
    CALL GMPRJ(GFORC4,OMZD1M,GTF,NMODE,NSTRUT,1)
    CALL GMSUB(QS,GTF,QS,NMODE,1)

COC FORM GENERALIZED THRUST MATRIX
  CALL GTPRJ(TXMOD,T,GTF,IN,NMODE,1)
  CALL GHADU(QS,GTF,QS,NMODE,1)

COC FORM GENERALIZED DRAG CHUTE FORCES
  FDC(1)=FCX
  FDC(2)=FCY
  FDC(3)=FCZ
  CALL GTPRJ(UCMODE,FDC,GTF,3,NMODE,1)
  CALL GHADU(QS,GTF,QS,NMODE,1)

COC FORM GENERALIZED AERO FORCES
  DO 42 I=1,NMODE
    NN=(I-1)*2+1
    CTMP1(NN)=-APMODE(NN)*AA77P
    CTMP1(NN+1)=APMODE(NN+1)*YA77P
    CTMP1(NN+2)=-ARMODE(NN+2)*ANA77P
    CTMP1(NN+3)=ARMODE(NN+3)*ALA77F
    CTMP1(NN+4)=ARMODE(NN+4)*AMA77F
42  CTMP1(NN+5)=ARMODE(NN+5)*ANA77F
    DO 43 II=1,NMODE
      GTF(II)=0.
      DO 43 JJ=1,5
        MJ=(II-1)*2+JJ
43  GTF(II)=GTF(II)+CTMP1(MJ)*PF(MJ)
      CALL GHADU(QS,GTF,QS,NMODE,1)

COC FORM GENERALIZED STIFFNESS
  DO 44 IG=1,NMODE
    GTF(IG)=GQ(IG)*GMASS1(IG)*GFREQ(IG)**2.
44  QS(IG)=QS(IG)-GTF(IG)

COC SOLVE FOR THE GENERALIZED ACCELERATION
  CALL SOLVE(NMODE,COEF,QS,GQD2)
  DO 45 I=1,NMODE
    NCON=(I-1)*2+1
    MCON=NCON+1
    CALL INTEG(LA(NCON),GQD2(I))
    CALL INTEG(LA(MCON),GQD1(I))
45  CONTINUE
  RETURN
C

```



```

C ENTRY FLEX7
IF (INDFLX.EQ.1.OR.INDLG.EQ.0) RETURN
RVAR=2.*FLOAT(NMODL)/4.
K=IFIX(RVAR)
IF (K.EQ.3) GO TO 71
DO 70 I=1,K
N=4*I-3
MJ1=2*I-1
MDL=2*I
70 CALL UPDAT(4,LA(N),GQD1(MD1),GQ(MD1),GQD1(MD0),GQ(MD0),DU)
CONTINUE
L=2*K
IF (L.EQ.NMODE) RETURN
71 M=4*K+1
MP=2*K+1
CALL UPDAT(2,LA(M),GQD1(MP),GQ(MP),DU,DU,DU)
RETURN
END
SUBROUTINE DECCMP (NN,A,UL)
DIMENSION A(20,20), UL(20,20), SCALES(20), IPS(20)
COMMON IPS
IF (NN.GT.1) GO TO 20
UL(1,1)=A(1,1)
RETURN
20 N=NN
C INITIALIZE IPS, UL AND SCALES
DO 5 I=1,N
IPS(I)=1
ROWNRM=1.
DO 2 J=1,N
UL(I,J)=A(I,J)
IF (ROWNRM-ABS(UL(I,J))) 1,2,2
1 ROWNRM=ABS(UL(I,J))
2 CONTINUE
3 IF (ROWNRM) 3,4,3
SCALES(I)=1./ROWNRM
4 GO TO 5
CALL SING(1)
SCALES(I)=L.G
5 CONTINUE
C GAUSSIAN ELIMINATION WITH PARTIAL PIVOTING
NM1=N-1
DO 17 K=1,NM1
BIG=0.
DO 11 I=K,N
IP=IPS(I)
SIZE=ABS(UL(IP,K))*SCALES(IP)
IF (SIZE-BIG) 11,11,10
10 BIG=SIZE
IOXPIV=I
11 CONTINUE
IF (BIG) 13,12,13
12 CALL SING(2)
GO TO 17
13 IF (IOXPIV-K) 14,15,14
14 J=IPS(K)
IPS(K)=IPS(IOXPIV)
IPS(IOXPIV)=J
15 KP=IPS(K)
PIVOT=UL(KP,K)
KP1=K+1
DO 16 I=KP1,N

```

```

      IP=IPS(I)
      LM=UL(IP,K)/PIVOT
      UL(IP,K)=-LM
      DO 16 J=KP+1,N
      UL(IP,J)=UL(IP,J)+LM*UL(KP,J)
16  CONTINUE
17  CONTINUE
      KP=IPS(N)
      IF (UL(KP,N)) 19,18,14
18  CALL SING(2)
19  RETURN
      END
      SUBROUTINE SOLVE (NN,UL,B,X)
      DIMENSION UL(20,20), B(20), X(20), IPS(20)
      COMMON IPS
      IF (NN.GT.1) GO TO 5
      X(1)=B(1)/UL(1,1)
      RETURN
5     N=NN
      NP1=N+1
C
      IP=IPS(1)
      X(1)=B(IP)
      DO 2 I=2,N
      IP=IPS(I)
      IM1=I-1
      SUM=0.0
      DO 1 J=1,IM1
1     SUM=SUM+UL(IP,J)*X(J)
2     X(I)=B(IP)-SUM
C
      IP=IPS(N)
      X(N)=X(N)/UL(IP,N)
      DO 4 IBACK=N,N
      I=NP1-IBACK
C
      I GO TO (N-1),.....,1
      IP=IPS(I)
      IP=I+1
      SUM=0.0
      DO 3 J=IP,N
3     SUM=SUM+UL(IP,J)*X(J)
4     X(I)=(X(I)-SUM)/UL(IP,I)
      RETURN
      END
      SUBROUTINE SING (IWHY)
11  FORMAT(54H,MATRIX WITH ZERO ROW IN DECOMPOSE. )
12  FORMAT(54H,SINGULAR MATRIX IN DECOMPOSE. ZERO DIVIDE IN SOLVE. )
      NOUT=6
      NOUT=STANDARD OUTPUT UNIT
      GO TO (1,2),IWHY
1     WRITE (NOUT,11)
      GO TO 1
2     WRITE (NOUT,12)
10  CALL EXERR(0)
      RETURN
      END
      SUBROUTINE ARAY (MODE,I,J,N,M,S,D)
      IDENT ARAY
      TITLE ARAY
      ADAPTED FROM 5/366 SCIENTIFIC SUBROUTINE PACKAGE.
      (J6.A-CM-23X) VERSION III
      R. A. GARMOL. 08/16/69.
      .....

```

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# SUBROUTINE ARAY

## PURPOSE

CONVERT DATA ARRAY FROM SINGLE TO DOUBLE DIMENSION OR VICE  
VERSA. THIS SUBROUTINE IS USED TO LINK THE USER PROGRAM  
WHICH HAS DOUBLE DIMENSION ARRAYS AND THE SSP SUBROUTINES  
WHICH OPERATE ON ARRAYS OF DATA IN A VECTOR FASHION.

```
.....
DIMENSION S(1),D(1)
IF (I.GT.1) GO TO 98
IF (MODE.EQ.1) D(1)=S(1)
IF (MODE.EQ.2) S(1)=D(1)
RETURN
```

```
98 NI=N-I
```

## TEST TYPE OF CONVERSION

```
IF(MODE-1) 100, 110, 120
```

## CONVERT FROM SINGLE TO DOUBLE DIMENSION

```
100 IJ=I*J+1
NM=N*J+1
DO 110 K=1,J
NM=NM-NI
O) 110 L=1,I
IJ=IJ-1
NM=NM-1
110 O(NM)=S(IJ)
GO TO 140
```

## CONVERT FROM DOUBLE TO SINGLE DIMENSION

```
120 IJ=0
NM=0
DO 130 K=1,J
DO 125 L=1,I
IJ=IJ+1
NM=NM+1
125 S(IJ)=D(NM)
130 NM=NM+NI
```

```
140 RETURN
```

```
END
SUBROUTINE CTIE(A,B,R,N,M,MSA,MFB,L)
```

```
IDENT CTIE
```

```
TITLE CTIE
```

```
ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
(360A-CM-33X) VERSION III
R. A. GARMOE. 10/16/69.
```

## SUBROUTINE CTIE

## PURPOSE

ADJOIN TWO MATRICES WITH SAME ROW DIMENSION TO FORM ONE  
RESULTANT MATRIX (SEE METHOD)



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```

10 R(I)=A(I)+U(I)
RETURN
END
SUBROUTINE GMAOU(A,B,R,N,M)
  IDENT GMAOU
  TITLE GMAOU
  ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
  (36-A-CM-33X) VERSION III
  R. A. GARMOL. 8/16/69.
  .....
  SUBROUTINE GMAOU
  PURPOSE
    ADD TWO GENERAL MATRICES TO FORM RESULTANT GENERAL MATRIX
  .....
  DIMENSION A(1),B(1),R(1)
  CALCULATE NUMBER OF ELEMENTS
  NM=N*M
  ADD MATRICES
  DO 10 I=1,NM
10 R(I)=A(I)+U(I)
RETURN
END
SUBROUTINE GMPRO(A,B,R,N,M,L)
  IDENT GMPRO
  TITLE GMPRO
  ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
  (36-A-CM-33X) VERSION III
  R. A. GARMOL. 8/16/69.
  .....
  SUBROUTINE GMPRO
  PURPOSE
    MULTIPLY TWO GENERAL MATRICES TO FORM A RESULTANT GENERAL
    MATRIX
  .....
  DIMENSION A(1),B(1),R(1)
  IR=0
  IK=-M
  DO 10 K=1,L
  IK=IK+M
  DO 10 J=1,N
  IK=IR+1
  JI=J-N
  IB=IK
  R(IR)=0
  DO 10 I=1,M
  JI=JI+N
  IB=IB+1
10 R(IR)=R(IR)+A(JI)*U(IB)
RETURN
END

```

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SUBROUTINE SDFLGP
COMMON/DIRCOM/CH1(74),TIMER,UM2(61),AMASS,DM23(27),AX77F,DM21(4),
*AZ77F,UM22(114),OCL1,OCM1,
*OCN1,OCL2,OCM2,OCN2,OCL3,OCM3,OCN3,DM3(99),FXB7P,
*DM4(13),FYB7P,DM23(13),FZB7P,UM5(17),GXU7F,DM6(8),
*GZB7F,DM24(6),HGC7F,DM25(211),INDSTE,DM12(47),PHIPU,DM26(23),
*PSTPD,
*DM27(156),THTPC,DM28(5),TIME,DM29(12),TMAX,DMA(274),
*PI77R,DM31,PI77R1,UM4(51),Q177R,DM31,Q177R1,UM11(51),
*RI77R,DM32,RI77R1,DM11(49),XG77F,DM33,XG77F1,
*DM34(11),YG77F,DM35,YG77F1,DM36(11),
*ZG77F,DM37,ZG77F1,DM13(53),
CNSTRUT,MASS(5),RX(5),RY(5),GZ(5),THETA(5),CRDEG,RGR,
CNTIRES(5),KZERO(5),W(5),DELTAM(5),MOMENT(5),
CMF(5),VZ,IFD,PZERO(5),VZERO(5),A(5),P2C(5),V20(5),
CA2(5),IL,SLT(5),ES2(5),C2L(5),MASS2(5),MUS(5),
CCG(5),CE(5),C2C(5),C2L(5),NVGPT,NPP,MB(5),RLT,NDELTA,
CE(5),S2(5),SD21(2),SD22(2),SD23(2),SD24(2),SD25(2)
COMMON/DIRCOM/
CSJ1(2),SD12(2),SD13(2),SD14(2),SD15(2),
CS1(2),SS2(2),S2(2),S4(2),S5(2),
CS2021(2),S2022(2),S2023(2),S2024(2),S2025(2),
CS2011(2),S2012(2),S2013(2),S2014(2),S2015(2),
CS21(2),S22(2),S23(2),S24(2),S25(2),
COMT01(2),OMT012(2),OMT013(2),OMT014(2),OMT015(2),
COMT1(2),OMT2(2),OMT3(2),OMT4(2),OMT5(2),
CAI(5),OI(5),DELTA1,DELTA2,DELTA3,DELTA4,DELTA5,
COUDEL1,COUDEL2,COUDEL3,COUDEL4,COUDEL5,ISTAGE,
CPTMIN,IPL1,ISUP,ISTPL1,ISTPL2,ISTPL3,ISTPL4,ISTPL5,
COM14(154),INDLG,DM15(151),DM15(6,7),NPTS,DPH17(144),IFLX(20)
COMMON/FLXUP/DM17(338),XO2F(20),XO2T(20),YO2F(20),YO2T(20),
*ZO2F(20),ZO2T(20),XO1F(20),XO1T(20),YO1F(20),YO1T(20),
*ZO1F(20),ZO1T(20),XO,F(20),YO,F(20),ZO,F(20)
REAL MASS,MOMENT,MASS2,MUS,NTIRES,MB
COMMON/LGGE/LA(25),FC2(5),P2(5),PRES(5),C(5),IPPT,LTPT
COMMON/LGGE/FX,FY,FZ,LH,MH,NH
COMMON/LGGE/A11(5),A13(5),A31(5),A33(5),RRCGX(5),
CRL(3,3),RI(3,3,5),RAX(5),RAY(5),RAZ(5),TMP(3),ZZERO(5),
CXR(5),YR(5),EPSLON(5),PA(5),FDELTA(5),
CFTRZ(5),RDX(5),RDY(5),RDZ(5),RDXG(5),RDYG(5),RDZG(5),
CVTX(5),VTY(5),VTZ(5),GZ(5),VGPT(5),FTRX(5),FTRY(5),
COX(5),OY(5),OZ(5),FX(5),FOY(5),FF(5),AA(5),C2(5),
CSR(5),SF(5),PSKO(5),MUVP(5),HTAX(5),MTRY(5),
CMTRZ(5),MA(5),PG11,PG13,PG32,PG33,IPRT,
CMTX,MTY,MTZ,SFTRX,SFTRY,SFTRZ,FTRA,
CFTRD,FTRC,SHTRX,SHTRY,SHTRZ,
REAL MUVP,MTRX,MTRY,MTRZ,MA,
CMTX,MTY,MTZ,LH,MH,NH
DIMENSION ULLTA(5),DOELTA(5),P(5),
C(SD21(1),SD2(1,1)),(SD11(1),SD1(1,1)),(S1(1),S(1,1)),
C(S2021(1),S202(1,1)),(S2011(1),S201(1,1)),(S21(1),S2(1,1)),
C(OMT01(1),OMT01(1,1)),(OMT1(1),OMT(1,1))
DIMENSION OP16(8),OP17(8),OP18(8),OP19(4),OP20(8),OP21(8),
*DAT2(15),DAT3(6),DAT4(15)
DATA
* (OP16(1),I=1,8)/3HDELTA,1HP,2HF2,2HFT,2HSR,2HSF,2HAA,3HFC2/,
* (OP17(1),I=1,8)/3HSD2,3HSD1,1HS,4HS202,4HS201,2HS2,
* 6HOMETD1,4HOMET/,
* (OP18(1),I=1,8)/4HFTRA,4HFTRB,4HFTRC,3HMTX,3HMTY,
* 3HMTZ,3HFXM,3HFYM/,

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*{JP19(1),I=1,5}/3HFZM,2HLM,2HMM,2HNM,5HQI77R,
*{JP1(1),I=1,5}/4HMOVA,4HUCPY,4AFTRX,4HFTRY,4HFTRZ,
*2HMA,2H41,6HDELTA/,
*{OP2(1),I=1,5}/2HDELTA,2HFT,4HMVP,4HFTRX,4HFTRY,
*4HFTWZ,64DELTA,1H5/,
DATA HUCI/5HLCAN /
DATA DAT1/4HTIME/, (DAT2(I),I=1,15)/2HLM,2HMM,2HNM,5HQI77R,
*5HTHPU,PHPSID,5HHPID,3HFZM,5HAZ77F,6HZG77F1,5HMGCF,
*5HXG77F,5HYG77F,5HAX77F,5HXG77F1/,
*{DAT4(I),I=1,5}/2HFT,2H5F,5HDELTA,1HP,2HP2,2HMA/,
*{DAT4(I),I=1,15}/4HXO2F,4HXO2T,4HYO2F,4HYO2T,4HZO2F,4HZO2T,
*4HXO1F,4HXO1T,4HYO1F,4HYO1T,4HZO1F,4HZO1T,4HXO0F,4HYO0F,4HZO0F/,
DATA DAT5/6HLCSTPTZ, N1/1/, N15/15/, N14/14/
SAVE DATA ON TAPE
IF (IPLT.EQ.0) RETURN
LASTPT=
IF (IPLT.GT.1) GO TO 2.1

NHL=2
IF (ISOF.NE.C) NHL=NHL+1
ISUM1=ISTPL1+ISTPL2+ISTPL3+ISTPL4+ISTPL5
IF (ISUM1.NE.) NHL=NHL+1
ISUM2=
DO 1/5 I=1,NPTS
105 ISUM2=ISUM2+IFLX(I)
IF (ISUM2.NE.) NHL=NHL+1
WRITE(13) NHL
WRITE(13) N1,N1,DAT1
IF (ISOF.NE.C) WRITE(13) N15,N1,DAT2
IF (ISUM1.NE.) WRITE(13) N14,ISUM1,DAT3,OP17
IF (ISUM2.NE.) WRITE(13) N15,ISUM2,DAT4
WRITE(13) N1,N1,DAT5
IPLT=IPLT+1
2.1 WRITE(13) TIME
IF (ISOF.NE.C) WRITE(13) LH,HH,NM,7I77R,THFPU,PSIDP,PHIPD,FZH,
*AZ77F,ZG77F1,HGCF, XG77F,YG77F,AX77F,XG77F1
IF (IPLT.NE.0) WRITE(13) FT(1),SF(1),DELTA(1),P(1),P2(1),MA(1),
*SD2(1,1),SD1(1,1),S(1,1),S2D2(1,1),S2D1(1,1),S2(1,1),OMETO1(1,1),
*OMET(1,1)
IF (ISTPL.NE.C) WRITE(13) FT(2),SF(2),DELTA(2),P(2),P2(2),MA(2),
*SD2(1,2),SD1(1,2),S(1,2),S2D2(1,2),S2D1(1,2),S2(1,2),OMETO1(1,2),
*OMET(1,2)
IF (ISTPL3.NE.C) WRITE(13) FT(3),SF(3),DELTA(3),P(3),P2(3),MA(3),
*SD2(1,3),SD1(1,3),S(1,3),S2D2(1,3),S2D1(1,3),S2(1,3),OMETO1(1,3),
*OMET(1,3)
IF (ISTPL4.NE.C) WRITE(13) FT(4),SF(4),DELTA(4),P(4),P2(4),MA(4),
*SD2(1,4),SD1(1,4),S(1,4),S2D2(1,4),S2D1(1,4),S2(1,4),OMETO1(1,4),
*OMET(1,4)
IF (ISTPL5.NE.C) WRITE(13) FT(5),SF(5),DELTA(5),P(5),P2(5),MA(5),
*SD2(1,5),SD1(1,5),S(1,5),S2D2(1,5),S2D1(1,5),S2(1,5),OMETO1(1,5),
*OMET(1,5)
DO 1/5 I=1,NPTS
IF (IFLX(I).NE.C) WRITE(13) XO2F(I),XO2T(I),YO2F(I),YO2T(I),
*ZO2F(I),ZO2T(I),XO1F(I),XO1T(I),YO1F(I),YO1T(I),ZO1F(I),ZO1T(I),
*XO0F(I),YO0F(I),ZO0F(I)
17 CONTINUE
GO TO 2.4
ENTRY LGCA6P
IF (IPLT.EQ.0) RETURN
IF (LASTPT.EQ.0) RETURN
LASTPT=
LASTPT=1
BACKSPACE 13
24 WRITE(13) LASTPT
IF (LASTPT.EQ.C) RETURN
END FILE 13
RETURN
ENTRY LGAR6
TIME HISTORY PRINT
IF (INDLG.EQ.L) RETURN
CALL STFL(3,1,HUCI)

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O IF (INDLG.EQ.2) GO TO 30
  CALL STFL(2,8,OP16)
  DO 121 I=1,NSTRUT
    CALL STOVAR(6,DELTA(I),P(I),P2(I),FT(I),SR(I),SF(I),AA(I),FG2(I))
121 CONTINUE
  CALL STFL(2,8,OP20)
  DO 123 I=1,NSTRUT
    CALL STOVAR(8,MUVP(I),VGPT(I),FTRX(I),FTRY(I),FTRZ(I),
    *MA(I),MB(I),DOELTA(I))
123 CONTINUE
  CALL STFL(2,8,OP17)
  DO 122 I=1,NSTRUT
    CALL STOVAR(8,SD2(I,I),SD1(I,I),S(1,I),S2D2(1,I),
    CS2D1(1,I),S2(1,I),OMETD1(1,I),OMET(1,I))
122 CONTINUE
  GO TO 32
30 CALL STFL(2,8,OP21)
  DO 31 I=1,NSTRUT
    CALL STOVAR(8,DELTA(I),FT(I),MUVP(I),FTRX(I),FTRY(I),
    CFTRZ(I),DOELTA(I),S(1,I))
31 CONTINUE
32 CALL STFL(2,8,OP18)
  CALL STOVAR(8,FTRA,FTRB,FTRC,MTX,MTY,MTZ,
  CFXM,FYM)
  CALL STFL(2,4,OP19)
  CALL STOVAR(4,FZH,LX,MH,NH,DU,DU,DU,DU)
  RETURN
  *****
  ENTRY LGEAR5
  *****
  COMPUTE AND PRINT CODES
  RETURN
  ENTRY LGEAR7
  IF (INDLG.EQ.0) RETURN
  IF (INDLG.EQ.2) RETURN
  DO 6 I=1,NSTRUT
    IF (IL.NE.J) GO TO 5
    I1=2*I+J*NSTRUT-1
    CALL UPDAT(2,LA(I1),S2D1(1,I),S2(1,I),DU,DU,DU)
5    I1=2*I+NSTRUT-1
    CALL UPDAT(2,LA(I1),SD1(1,I),S(1,I),DU,DU,DU)
    CALL UPDAT(1,LA(I),OMET(1,I),DU,DU,DU,DU)
6    CONTINUE
  RETURN
  END
  OVERLAY(TOLA,1,0)
  PROGRAM TOLAN1
  COMMON/CONTR/ICONT,CONTR1,ICONT2,ICONT3
  IF (ICONT-2) 1,2,3
1  CALL READ
  GO TO 19
2  CALL TFFS2
  GO TO 19
3  IF (ICONT-4) 4,5,6
4  CALL SAC32
  GO TO 19
5  CALL VPCTAB
  GO TO 19
6  IF (ICONT-6) 7,8,9
7  CALL OPTTAB
  GO TO 19
8  CALL LGTAB
  GO TO 19
  )

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19 CALL DSEARCH(CONTR1, ICONT2, ICONT3)
   CONTINUE
END
SUBROUTINE TFFS2
COMMON/TABSRC/LOCTFF(2), LOCSAC(79), LOCVPC(18), LOCSDF(4), LOCLG(7)
   SETTING UP TABLES FOR TFFS
CALL TSEARCH(6HTTAB1, LOCTFF, 2, IER)
RETURN
   SETTING UP TABLES FOR SACS
ENTRY SACS2
CALL TSEARCH(6HATABJ1, LOCSAC(1), 79, IER)
RETURN
   SETTING UP TABLES FOR VPCS2
ENTRY VPC2AB
CALL TSEARCH(6HVTABU1, LOCVPC(1), 18, IER)
RETURN
   SETTING UP TABLES FOR OPT2
ENTRY OPTTAB
CALL TSEARCH(6HUTABJ1, LOCSDF(1), 4, IER)
RETURN
   SETTING UP TABLES FOR LGEAR
ENTRY LGTAB
CALL TSEARCH(6HFTABJ1, LOCLG(1), 3, IER)
CALL TSEARCH(6HCTABJ1, LOCLG(4), 4, IER)
RETURN
END
SUBROUTINE READ
COMMON /READ/ F(16), ITABLE, IID, IOD,
* IBC, K, IBCRW, INX, SLISYM, JBC, INXD
JIN=NSION MSG(58), RA(55), RA1(6)
EQUIVALENCE (MSG( 1), SYM), (MSG( 2), OP)
EQUIVALENCE (MSG( 3), RA), (MSG(58), INC)
REAL F(16), MRG, INXD
LOGICAL STWCH, TABST
COMMON /, TUPIT/ STWCH, TABST
DATA ICD, AINT, STCASE, TRA, MRG, NOREQ, OCT, COMMA/
* 3HBC, 3HINT, 3HSTCASE, 3HTRA, 3HMRG, 1HN, 3HOCT, 1H,/
DATA BLANK, PCINT, ET/ 1H, 1H., 1HE
DATA TABLED / 3HTAB /
FORMAT (11L12, /)
FORMAT (5X, 10, 10E12, /)
FORMAT (1, 1012)
FORMAT (A6, 1X, A3, 1X, 55A1, 6A1)
FORMAT (2, 1H, ERROR, THE SYMBOL **A6, 26H** IS NOT IN THE DIPECTORY/
1H)
FORMAT (22A6)
FORMAT (1, 16)
FORMAT (14, 1H, ERROR, AN STCASE MRG CARD HAS BEEN ENCOUNTERED,
* 42H FOR WHICH NO BASE CASE IS AVAILABLE, ERROR)
FORMAT (52H, ERROR, INPUT DECK NOT STARTED WITH STCASE CARD, ERROR)
FORMAT (18X, A6, 1X, A3, 1X, 55A1, 16)
FORMAT (25H, ERROR, COLUMN 12 IS BLANK/1H, /)
FORMAT (27H, NO-EXECUTE OPTION SELECTED)
FORMAT (1112)
FORMAT (55A1)

```

```

C   FORMAT (I1, 9A6)
K = 1
DO 16 I=1,2
DO 16 J=1,28
16  FU(I,J)=J.
100 READ(15,4) SYM,OP,RA,RA1
IF (OP,5) 18,19
18  REWIND 15
STOP 22
19  CALL DIPLAC(RA1,INC,BLANK)
C
20  IF (SYM .NE. STCASE) GO TO 150
21  STSWCH = .FALSE.
CALL DEF
101  IF (OP .NE. MRG ) GO TO 115
IF (JBC .LT. 0) GO TO 700
IF (IBC .EQ. 0) GO TO 110
C TERMINATE BASIC CASE AUXILIARY FILE
IID = -1
WRITE (16) IID,IID,FI,SYM,OP,RA,INC,ITABLE
ENOFIL 16
110  IBC = 0
REWIND 16
IBC=0
K = 1
GO TO 120
115  IBC = 1
INX = 1
JBC = 1
K = 1
IF (OP .NE. TABLED) GO TO 120
CALL TABSC
IF (TABSTP) GO TO 306
120  INX = 2
IF (RA(1) .NE. NOXEQ) GO TO 124
INX = 0
CALL LINES (2)
WRITE (6,12)
124  IF (IBC .EQ. 0) GO TO 130
REWIND 16
IBCRW = 0
GO TO 150
130  IF (INX .EQ. 0) GO TO 801
IF (IBC .EQ. 0) CALL READA (IBCRW)
GO TO 150
150  IF (JBC .NE. 1) GO TO 705
IF (STSWCH) GO TO 306
IF (K .EQ. 0) GO TO 170
152  IF (OP .NE. TRA) GO TO 200
CALL LINES (1)
WRITE (6,10) SYM,OP
IF (IBC .EQ. 0) GO TO 160
IID = -1
WRITE (16) IID,IID,FI,SYM,OP,RA,INC,ITABLE
160  IF (INX .EQ. 0) GO TO 100
IF (INX .NE. 1) GO TO 100
SLTSYM = SYM
RETURN
170  IF (IBC .NE. 0) GO TO 152
175  CALL READA (IBCRW)
K = 1
GO TO 152
200  IF (K .NE. 0) GO TO 300
IF (INX .EQ. 0) GO TO 295
IF (IBC .EQ. 0) CALL READA (IBCRW)

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305 K = 1
306 CALL WHCARD (MSG)
307 IF (RA(1) .NE. BLANK) GO TO 302
308 CALL LINES (2)
309 WRITE (6,11)
310 GO TO 304
302 IF (SYM .EQ. SLTSYM) GO TO 310
303 CALL DSEARCH (SYM,IUD,ITABLE)
304 IF (ITABLE .LT. 1) GO TO 310
305 CALL LINES (3)
306 WRITE (6,9) SYM
307 IF (IRC.NC. 1) GO TO 307
308 INX = 1
309 JDC = -1
310 INX = J
311 GO TO 301

DECODE CARD SECTION
312 IF (OP .NE. HCC) GO TO 430
313 DATA IS HCC
314 DECODE (1,1,1,RA)N
315 FORMAT(11)
316 K1 = 1
317 KK = 7
318 DO 1000 I=1,N
319 ENCODE (1,888,FI(I))(RA(L),L=K1,KK)
320 K1=K1+1
321 KK=KK+1
322 1000 CONTINUE
323 FORMAT(5A1)
324 CALL STORE(N,INC,INX,1)
325 IF (IRC .EQ. 3) GO TO 350
326 WRITE (10,110,N,FI,SYM,OP,RA,INC ,ITABLE)
327 SLTSYM = SYM
328 GO TO 111

NUMERIC TYPE DATA
400 IFI = 0
401 OCTAL TYPE
402 IF (OP .EQ. OCT) IFI=1
403 INTEGER TYPE
404 IF (OP .EQ. AINT) IFI=4
405 IQ = 1
406 LQ = 1
407 JJ = 1
408 KJ = LJ + 1
409 LQ = LQ + 1
410 IF (LQ .GT. 99) GO TO 418
411 IF (RA(LQ) .EQ. COMMA) GO TO 420
412 IF (RA(LQ) .NE. BLANK) GO TO 415
413 IQ = 1
414 MU = LQ - 1
415 IF (IFI .NE. 0) GO TO 500
416 JJ = KJ - 1
417 JQ = JQ + 1
418 IF (RA(JQ) .EQ. POINT) GO TO 435
419 IF (RA(JQ) .NE. EE) GO TO 440
420 IFI = 0
421 GO TO 500
422 IF (JQ .LT. MQ) GO TO 430
423 IFI = 0

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03 CALL PACKRW(RA(KQ),EQ(1,JJ),HQ-KQ+1)
520 IF(IQ.NE.0)GO TO 525
    JJ=JJ+1
    GO TO 410
525 CALL RITE(IFI,FU,FI,JJ)
600 CALL STOPZ(JJ,INC,INX,0)
    IF (IBC,NE.0) WRITE (16) IID,JJ,FI,SYM,OP,RA,INC,ITABLE
    GO TO 350
700 CALL LINES (1)
    WRITE (5,6)
    GO TO 810
705 CALL LINES (1)
    CALL DEF
    WRITE (6,3)
801 SLTSYM = SYM
802 READ (5,4) SYM,OP,RA,INC
    IF (EOF,5) 25,26
25 R=IND 13
    STOP 25
26 IF (SYM.EQ.STCASE)GO TO 21
    CALL WRCARD (MSG)
    IF (OP .EQ. TRA ) GO TO 802
    IF (RA(1) .EQ. BLANK ) GO TO 24
    IF (SYM .EQ. SLTSYM) GO TO 802
    CALL DSEARCH (SYM,IUD,ITABLE)
    IF (ITABLE.LT. 1) GO TO 801
    CALL LINES (1)
    WRITE (6,5) SYM
    GO TO 801
    END
    SUBROUTINE DIPLAC(RA1,INC,BLANK)
    DIMENSION RA1(6)
    DIMENSION RC(2)
    .....
PICK UP COLUMN 67 TO 72 AND
RIGHT JUSTIFY FOR USE IN THE INPUT ROUTINE
.....
00 7 I=1,6
    IF (RA1(I) .NE. BLANK) GO TO 2
    DO 1 N=1,6
    N1=7-N
    N2=6-N
    RA1(N1)=RA1(N2)
    RA1(1)=BLANK
    INC=0
1
2
6
IF EXIT THROUGH GO STATEMENT 2
THEN A VALID NUMBER EXIST.

    GO TO 6
    CALL PACKRW(RA1,RC,6)
    CALL RITE(3,RC,INC,1)
    RETURN
END
SUBROUTINE TABRE
COMMON/TABDIR/TABLE(1)
COMMON /STOPIT/ STSWCH , TABSTP
COMMON/TABCOF/LOCS(115),STABLE(115)
DIMENSION IS(115),RA1(6)
LOGICAL STSWCH , TABSTP
DATA BLANK , BCOTRA / 1H ,3HTRA /

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```

DATA MAXT, MAXTAB / 115,800/
TAUSTP = .FALSE.
DO 2 I=1,MAXT
5  IS(1) = 'BLANK'
   SYMTRA = 'BLANK'
   NSUM = 0
   NTR = 0
   WRITE (6,3)
3  FORMAT (3X,43HTABLE SIZES FOR EACH TABLE USED IN THIS RUN)
10  READ(5,11) SYM,SYMTWA,RA1
11  FORMAT(A5,1X,A3,1X,A1)
   CALL DIPLAC(RA1,NTSIZE,BLANK)
   CALL LINES (1)
   IF (SYMTRA .EQ. UCUTRA) GO TO 21
   WRITE (6,4) SYM,SYMTRA,NTSIZE
4  FORMAT (14X,A5,1X,A3,1X,I4)
   JJ = 0
   DO 15 J=1,MAXT
   IF (SYM .NE. STABLE(J)) GO TO 15
   IS(J)=NTSIZE
   NSUM = NSUM+NTSIZE
   NTR=NTR+1
15  CONTINUE
   TABSTP = .TRUE.
   CALL LINES (2)
   WRITE (6,24) SYM
24  FORMAT (14X,36X,A6,29H DOES NOT EXIST IN TABLE LIST)
   GO TO 15
21  CALL LINES (2)
   WRITE (6,4) BLANK,SYMTRA
   NSUM=NSUM+MAXT-NTR
   WRITE (6,22) NSUM
22  FORMAT(3X,39HTOTAL NUMBER OF CELLS FOR ALL TABLES = I4)
   IF (NSUM .LE. MAXTAB) GO TO 200
   TABSTP = .TRUE.
   CALL LINES (2)
   WRITE(6,23) MAXTAB, NSUM
23  FORMAT(14X,1X,25HTOTAL TABLE SIZES EXCEED I4,4H . ,
* 35HCHANGE MAXIMUM TOTAL TABLE SIZES TO ,I4/
* 25H IN THE MAIN PROGRAM TOLA)
200  KONT=1
   DO 25 I=1,MAXT
   LOC(I)=KONT
25  KONT = KONT+IS(I)
   RETURN
END
SUBROUTINE READA (ICRW)
COMMON/READ1/FI(56),ITABLE,IID,IID,OH(7)
INTEGER MSG(58)
IF (ICRW .NE. 0) RETURN
100 READ (16) IID,J,FI,MSG,ITABLE
IF (IID .GE. -1) GO TO 105
ICRW = 1
RETURN
105 CALL WRDARD (MSG)
IF (IID .LT. 0) RETURN
CALL STORE(J,IIDUM1,IIDUM2,1)
GO TO 100
END
SUBROUTINE STORE(N,INC,INX,STAPE)
INTEGER STAPL
COMMON/READ1/FI(56),ITABLE,IID,IID,OH(7)
COMMON/DIACOM/DATA(3959)
COMMON/TAGCIR/TABLE(1)
IF (STAPL.NE.0) GO TO 50

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O      M1OR0 = J
      IF (INC.GT.C) M1OR0 = -1
      IIO = IOU+INC+M1OR0
      IF (INX.EQ.C) RETURN
50     J=IIO
      IF (TABLE.LT.0) GO TO 2
      DO 1 I=1,N
      DATA (J) = FI(I)
1      J = J+1
      RETURN
2      DO 3 I=1,N
      TABLE(J) = FI(I)
3      J = J+1
      RETURN
      END
      SUBROUTINE WPCARD(MSG)
      INTEGER MSG(58)

C      CALL LINES (1)
      J = 58
      IF (MSG(58).LE.J) J=57
      WRITE (0,1) (MSG(I),I=1,J)
10     FORMAT (18X,A6,1X,A3,1X,55A1,I6)
      RETURN
      END
      SUBROUTINE PACK (I1,I2,N)
      DIMENSION I1(1)
      DATA IUL / 6H /
1      FORMAT (6A1)
2      FORMAT (A6)
      REWIND 31
      IF (N.GE.6) GO TO 3
      K = 6 - N
      WRITE (31,1) (IOL, I = 1,K), (I1(I), I = 1,N)
      GO TO 4
3      WRITE (31,1) (I1(I), I = 1,6)
4      REWIND 31
      READ (31,2) I2
      RETURN
      END
      SUBROUTINE DSEARCH (SYM,IOC,IER)
      COMMON/FIXDIP/ANAME(900),LOC(900),NCCOUNT
      DO 50 I=1,NCCOUNT
      IF (SYM.NE. ANAME(I) ) GO TO 53
      IER = I
      IOC = LOC(I)
      RETURN
50     CONTINUE
      CALL TSEARCH (SYM,IOC,1,IER)
      RETURN

C      END
      SUBROUTINE PACKRK(I1,I2,NNN)
      DIMENSION I1(1)
1000    FORMAT (1H(I2,2HX,I2,3HA1))
      K=2-NNN
      ENCODE(10,IOC,XMAT)K,NNN
      ENCODE(20,XMAT,I2)(I1(I),I=1,NNN)
      RETURN
      END
      SUBROUTINE WITE(IFI,FJ,FI,JJ)
      DIMENSION FI(56),FJ(56)
      GO TO (100,200,300,400),IFI
100     II=1
      DO 101 I=1,JJ

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* 6HEPS11 6HEPS16 6HEPS17 6HEPS18 6HEPS19 6HEPS20 6HEPS21 6HEPS22
* 6HEPS23 6HEPS24 6HEPS25 6HEPS26 6HEPS27 6HEPS28 6HEPS29 6HEPS30
* 6HEPS31 6HEPS32 6HEPS33 6HEPS34 6HEPS35 6HEPS36 6HEPS37 6HEPS38
* 6HEPS39 6HEPS40 6HEPS41 6HEPS42 6HEPS43 6HEPS44 6HEPS45 6HEPS46
* 6HEPS47 6HEPS48 6HEPS49 6HEPS50 6HEPS51 6HEPS52 6HEPS53 6HEPS54
* 6HEPS55 6HEPS56 6HEPS57 6HEPS58 6HEPS59 6HEPS60 6HEPS61 6HEPS62
* 6HEPS63 6HEPS64 6HEPS65 6HEPS66 6HEPS67 6HEPS68 6HEPS69 6HEPS70
* 6HEPS71 6HEPS72 6HEPS73 6HEPS74 6HEPS75 6HEPS76 6HEPS77 6HEPS78
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* 6HEPS95 6HEPS96 6HEPS97 6HEPS98 6HEPS99 6HEPS100 6HEPS101 6HEPS102
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* 6HEPS111 6HEPS112 6HEPS113 6HEPS114 6HEPS115 6HEPS116 6HEPS117 6HEPS118
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* 
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DATA (LOC 1), 1-1, 126)	6H1A84X	6H1A84Y	6H1A85X	6H1A85Y	6H1A86X	6H1A86Y	6H1A87X
23	11	11	24	25	29	30	31
32	13	13	34	35	39	40	41
40	42	43	44	45	49	50	51
48	49	72	73	74	75	76	77
77	74	78	80	81	82	83	84
84	85	86	87	88	89	90	91
91	94	95	99	100	101	102	103
105	106	108	109	110	111	112	113
113	116	117	120	121	122	123	124
128	129	130	131	132	133	134	135
138	140	137	138	139	140	141	142
141	142	9	148	146	147	148	149
150	151	152	153	154	155	156	157
158	159	160	161	162	163	164	165
166	167	168	169	170	171	172	173
17	175	179	181	183	184	185	186
187	188	189	190	191	192	193	194
194	195	196	197	198	199	200	201

DATA	194	195	196	197	198	199	200
(LOC)	J	K	L	M	N	O	P
127,	128,	129,	130,	131,	132,	133,	134,
135,	136,	137,	138,	139,	140,	141,	142,
143,	144,	145,	146,	147,	148,	149,	150,
151,	152,	153,	154,	155,	156,	157,	158,
159,	160,	161,	162,	163,	164,	165,	166,
167,	168,	169,	170,	171,	172,	173,	174,
175,	176,	177,	178,	179,	180,	181,	182,
183,	184,	185,	186,	187,	188,	189,	190,
191,	192,	193,	194,	195,	196,	197,	198,
199,	200,	201,	202,	203,	204,	205,	206,
207,	208,	209,	210,	211,	212,	213,	214,
215,	216,	217,	218,	219,	220,	221,	222,
223,	224,	225,	226,	227,	228,	229,	230,
231,	232,	233,	234,	235,	236,	237,	238,
239,	240,	241,	242,	243,	244,	245,	246,
247,	248,	249,	250,	251,	252,	253,	254,
255,	256,	257,	258,	259,	260,	261,	262,
263,	264,	265,	266,	267,	268,	269,	270,
271,	272,	273,	274,	275,	276,	277,	278,
279,	280,	281,	282,	283,	284,	285,	286,
287,	288,	289,	290,	291,	292,	293,	294,
295,	296,	297,	298,	299,	300,	301,	302,
303,	304,	305,	306,	307,	308,	309,	310,
311,	312,	313,	314,	315,	316,	317,	318,
319,	320,	321,	322,	323,	324,	325,	326,
327,	328,	329,	330,	331,	332,	333,	334,
335,	336,	337,	338,	339,	340,	341,	342,
343,	344,	345,	346,	347,	348,	349,	350,
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ORIGINAL PAGE IS  
OF POOR QUALITY

DATA NCOUNT 7894/

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DATA (NAME) (M) (H) (S) 63777
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DATA (LOC(M), M=505,637)/

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914	922	927	928	929	1214	1206
933	1218	1212	437	934	942	1216
945	1221	1224	1225	952	956	1228
1231	950	461	465	981	1232	967
963	1238	1242	375	981	983	984
985	1246	799	392	1252	1256	999
1006	1260	1109	1266	1266	1270	1117
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DATA (NAME (N), N=638, 759) /

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ORIGINAL PAGE 18  
OF POOR QUALITY

IF (ICONT-2) 1,2,2  
CALL AUTS  
GO TO 19  
CALL AUTSPR  
CONTINUE  
END  
SUBROUTINE AUTS

# AUXILIARY COMPUTATIONS

INPUT REQUIRED (FROM DIRCOM)  
XG77F, YG77F, ZG77F - LOCAL GEODETIC DISPLACEMENTS  
XG77F1, YG77F1, ZG77F1, AL2, AL27S1, AN2, AN277S, AM2, AM27S1  
RGR

COMMON/DIRCOM/DM1(73),THR,DM2(42),ALPHD,DM3(3),ALPHR1,DM3(15),  
\*AMASS,DM4(5),ARLEF,DM5(11),DLTA(1),DM6(3),HCTAR1,DM7(147),  
\*DELPO,DM8,DELOC,DM9,DELXD,DM10,DM11(61),FX07P,DM12(23),  
\*GHEFF,DM13(17),HGC7F,DM14(11),NDSTE,DM15(47),PHIPD,  
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\*SGAMA,DM16(75),TIME,DM17(5),VA77F,  
\*DM18(3),VG77F,DM37(23),XGW7F1,DM19(22),  
\*YGW7F1,DM21(18),ZGW7F1,DM36(12),AL2,DM65,  
\*AL27S1,DM32(13),AM,DM69,AM27S1,DM33(9),  
\*AN2,DM66,AN277S,DM34(43),  
\*U777F,DM24(33),XG77F,DM63,XG77F1,DM61(11),  
\*YG77F,DM62,YG77F1,DM63(11),ZG77F,DM64,ZG77F1,DM25(53)  
COMMON/DIRCOM/INSTRUT,DM26(26),RGR,NTIRC(5),  
\*RZCRO(5),DM27(1),MOMENT(5),DM28(85),MB(5),DM29(82),  
\*DM1(2),DM12(2),DM13(2),DM14(2),DM15(12),  
\*DLTA1,DLTA2,DLTA3,DLTA4,DLTA5,DM30(14)  
COMMON/DIRCOM/  
1IN,ZN(5),YN(5),N(5),ICS,COCH,SSH,XCH,YCH,ZCH,  
2IJ(5),ITU,HF,NF,XRF,HRF,DELTAH,KP,ITI,NLH1,VS,XS,TS,  
3VATG,ALPHD,MS,ALPOS,IAP,VO,DELVE,EPSGS,ALPHD3,ALPHOL,  
4HGC,DELEP3,RFH,PGS,DELSIG,HFY,PHIC,ITD,XTD,HTD,VXTD,  
5VATD,ITR,LN,CA,TL,TU,KE(5),PM,TSP,TRV,TCH,TBK,ISS,  
6ILR,IBJ,IC(5),XRF1,IT1(5),XRF2,IT2(5),H1,IH1(5),  
7H2,IH2(5),HR1,IHR1(5),HR2,IHR2(5),TR1,ITA1(5),  
8TR2,ITK(5),TJK1,TJK1(5),TJK2,ICK2(5),DELQ1,  
9RFALPH,DELALA,PSH,TST,DELOF,DELF01,DELQTO,DELQOL,DELQUL,INOLG  
COMMON/DIRCOM/  
1RFB,DELGA,PSF,RFPSI,DPSIA,PSPSI,DELR1,DELRU,RFPHI,OPHIA,  
2PSA,DELPL,DELPUL,TF(5),NOF(5),IR(5),NG(5),NLR(5),NTO(5),K2,  
3K3(5),K4(11),MBC(5),PD,DELTAH,DMECO1,DM67(4),MBL(5),MBU(5),  
4DELNS,DELXD,DELA,NED1,HR,DELOC,DM68,RFALP2,PSH2,  
\*DELOC,DELOC2,ALPOL,DM31(9),XR,XR01,HRD1,DELQ1,DM39(44),  
\*DM46(12568)

INPUT REQUIRED FROM LGEAR  
RG11, RG13, RG31, RG33

COMMON/LGAUTS/RG11, RG13, RG31, RG33, MA(5), VAXLE(5)

## OUTPUT GENERATED

XR, YR, ZR - C.G. POSITION RELATIVE TO RUNWAY COORDINATE SYSTEM  
XR01, YR01, ZR01 - VELOCITY IN RUNWAY COORDINATE SYSTEM  
HR, HRD1 - ALTITUDE AND ALT. RATE IN RUNWAY COORDINATE SYSTEM  
PSIPD1 - YAW RATE IN EARTH AXES FOR P-Y-R SEQUENCE  
PHIPD1 - ROLL RATE IN EARTH AXES FOR P-Y-R SEQUENCE

COMMON/AUTSC/TR,TC,TDX,  
1TUA,TDB,TD(5),IRA,IRH,IRC,ICA,ICB,  
2KA,KD,KEA,KEB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,  
3NLRA,NLRH,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC

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C      REAL KA, KB, NA, NNB, NC, ND, NNA, NNB, NNC, NLRA,
1      NLRB, NLRC, NDA, NDB, NDC, NTOA, NTOB, NTOC,
2      NJC, NUL, NLU, MU, NTIMES, MOMENT, MA, LR, N, NED1,
3      NU1, ISS

C      COMMON/ANTHFC/YH, ZI, YF01, ZR01, PSIP01, PHIP01,
1      VC, VAD, GAMPRL, OH, CLP, COR, LR, UR, HGS, RW, HEA, HE,
2      HCT, HPA, HPT, PHIDES, TX, TH, XRF01, PRF01, AXR, AHR,
3      ALPHAC, ALQ01, ALPHET, DELRN, HCTAST, UELR02, OH,
4      PHIE, PHIT, DELR01, UELQ01, DELR01, DELP01,
5      SNO1(5), OMEGTR(5), OMTRO1(5), OMEGE(5), PSIE, PSICT
COMMON/EXC/AUT/ADDIM1, SWT1, TIME1, ALP001, PNOES(5)
COMMON/AUTSAC/ALP001, QDESR, CLRR, ALPD, CORR, DELRNN

C      POSITION AND VELOCITY RELATIVE TO RUNWAY COORDINATE SYSTEM

LOGICAL SWT1, SWT2
DIMENSION DELTA(2), OMET(2,5)
EQUIVALENCE (DELTA, DELTA1), (OMET(1,1), OMET(1,1))
DATA RADDEG, DEGRAD/57.2957795, .01745329/
IPR=1
GO TO 4
ENTRY AUTSPH
IPR=1
2      DELTS=TIME-TIME1
TIME1=TIME
XR=RG11*(XG77F-RGR)+RG13*ZG77F
YR=YG77F
ZR=RG31*(XG77F-RGR)+RG33*ZG77F
XRD1=RG11*XG77F1+RG13*ZG77F1
YRD1=YG77F1
ZRD1=RG31*XG77F1+RG33*ZG77F1
HR=-ZR
HRD1=-ZRD1

C      EULER ANGLE DER. FOR PITCH, YAW, ROLL SEQUENCE

PSIP01=0.
IF((1.-AL2*AL2).LT.0.)GO TO 1
PSIP01=AL2751/3047(1.-AL2*AL2)
1      PHIP01=(AL4*AN2751/3047-AN2775)/(AN2*(1.+(AN2/AN2)**2))
IF(IPR.EQ.1)CALL AUTPR1

C      LOGIC TO DETERMINE PROBLEM PHASE

INPUT REQUIRED(FROM DIRCOM)
ITO = 0 FOR LANDING
ITO = NOT 0 FOR TAKE OFF
MF = FLARE ALTITUDE
NF = INDICATOR TO STOP AT END OF GLIDE SLOPE(NF=1)
XRF, HRF = INITIAL VALUES OF DESIRED TOUCHDOWN POINT
IN RUNWAY COORDINATE SYSTEM
DELTAH = ALTITUDE ABOVE HRF FOR HOLD MODE
KP = IMPACT INDICATOR
TI = IMPACT TIME SET, IF KP=0, NO TI NEEDED
NLRI = INDICATOR TO STOP AT IMPACT
=1, STOP AT IMPACT
VS, XS, TS = RUNWAY STOPPING CONDITIONS
VATO = AIRSPEED FOR TAKEOFF
ALPATO = ANGLE OF ATTACK FOR TAKEOFF
HS = ALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF

INPUT REQUIRED FROM LGEAR(DIRCOM)
DELTA1, DELTA2, DELTA3, DELTA4, DELTA5 = TIRE DEFLECTION FOR EACH GEAR

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8      INPUT FROM SDF2 (DIRCOM)
      TIME, HGC7F, NSTRTUT
      IF (ITO.NE.0) GO TO 2J
      IF (HGC7F.GE.HF) GO TO 7L
      IF (NF.EQ.1) GO TO 14
      IF ((XN.GT.XMF).OR.(HR.LE.(HRF+DELTAH))) GO TO 13
      CALL FLARE (ENTRY 1)
      CALL FLARE1 (IPR)
      CALL ENGINE FAILURE LOGIC
      CALL ENGFL
      GO TO PITCH AUTOPILOT
      GO TO 9J
13     IF (KP.EQ.1) GO TO 16
      DO 11 I=1,NSTRTUT
      IF (DELTA(I).GT.0) GO TO 12
11     CONTINUE
      CALL FLARE (ENTRY 2)
      CALL FLARE2 (IPR)
      CALL ENGINE FAILURE LOGIC
      CALL ENGFL
      GO TO PITCH AUTOPILOT
      GO TO 9J
12     KP=1
      TI=TIME
10     IF (NLRI.EQ.1) GO TO 16
      IF ((XRD1.LT.VS).OR.(XN.GT.XS).OR.
C      ((TIME-TI).GT.TS)) GO TO 16
      GO TO LANJING ROLL
      GO TO 8J
14     WRITE (6,15)
15     FORMAT (1X,16HEND OF GLIDE SLOPE)
      INSTE=J
      RETURN
16     WRITE (6,17)
17     FORMST (1X,21HAIRCRAFT HAS IMPACTED)
      INSTE=J
      RETURN

      G L I D E S L O P E

      INPUT REQUIRED FOR GLIDE SLOPE (FROM DIRCOM)
      VD - DESIRED INERTIAL VELOCITY DOWN THE GLIDE SLOPE
      DELVE - ALLOWED ERROR IN VE
      EPSGS - GLIDE SLOPE ELEVATION ANGLE
      ALPHDS - LOWER LIMIT ON ALPHA
      ALPHDL - UPPER LIMIT ON ALPHA
      TTD - DESIRED THRUST (INPUT ONLY IF IAP GREATER OR =3)
      HGC - DISTANCE BETWEEN WHEEL BOTTOM SURFACE AT 0 G.
      DELEPS - ALLOWED ANGULAR ERROR IN GLIDE SLOPE VERTICAL
      POSITION FROM ORIGIN
      RFH - RATE FEED BACK CONTRIBUTION TO HET
      PGS - PHNGOID CONTROL SENSITIVITY
      DELSIG - ALLOWED ANGULAR ERROR IN GLIDE SLOPE
      HORIZONTAL POSITION FROM ORIGIN
      RPY - RATE FEED BACK CONTRIBUTION TO HPT
      PHIC - CONSTANT EULER ROLL ANGLE FOR CROSS RANGE CONTROL

      INPUT FROM SDF2 (DIRCOM)
      VG77F, RHOAS, AMASS, GREFF, AREFF, XGW7F1, YGW7F1

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ZG77F1, YG77F1, XG77F1, YG77F1, ZG77F1  
 INPUT FROM SDF 2  
 XG77F1, YG77F1, ZG77F1

INPUT FROM LGEAR (DIRCOM)  
 RGP

OUTPUT GENERATED BY GLIDE SLOPE  
 VE - GLIDE SLOPE INITIAL VELOCITY ERROR  
 VAD - DESIRED AIRSPEED IN GLIDE SLOPE  
 IAP - PROBLEM PHASE INDICATOR  
 GAMMPR - FLIGHT PATH ANGLE FOR VAD  
 QR - DYNAMIC PRESSURE AT VAD  
 CLR - REQUIRED LIFT COEFFICIENT IN GLIDE SLOPE  
 CDR - DRAG COEFFICIENT ASSOCIATED WITH CLR  
 LQ - LIFT AT CLR AND QR  
 UR - DRAG AT CLR AND QR  
 THETAR - EULER ROLL ANGLE FOR REQUIRED GLIDE SLOPE CONDITIONS  
 TTD - DESIRED THRUST  
 HGS - DESIRED GLIDE SLOPE ALTITUDE  
 RR - DISTANCE TO GLIDE SLOPE ORIGIN  
 MEA - GLIDE SLOPE VERTICAL POSITION ERROR ALLOWED  
 ME - ACTUAL GLIDE SLOPE POSITION ERROR  
 MED1 - RELATIVE RATE LEAVING GLIDE SLOPE  
 MET - TOTAL GLIDE SLOPE POSITION ERROR  
 HPT - TOTAL GLIDE SLOPE HORIZONTAL POSITION ERROR  
 HPA - GLIDE SLOPE HORIZONTAL POSITION ERROR ALLOWED  
 P+UES - DESIRED EULER ROLL ANGLE

70 IAP=1  
 VE=VG77F-VU  
 TMP1=VE\*PI/180\*DEGRAD  
 IF (ABS(VE).LE.DELVL) GO TO 71  
 TMP2=VE\*COS(TMP1)-XG77F1  
 TMP3=VE\*SIN(TMP1)-YG77F1  
 VAD=SQRT(TMP2\*TMP2+YGM77F1\*YGM77F1+TMP3\*TMP3)  
 GAMMPR=ATAN(-TMP3/TMP2)  
 GAMPRU=GAMMPR\*RAUDLG  
 QR=.5\*RHQAS\*VAD\*VAD  
 CLR=AMASS\*GKEFF/(QR\*AREFF)  
 SWT2=.FALSE.  
 QJESR=.  
 76 DO 75 I=1,2  
 ALPD=ALPOL  
 CALL SAC1.  
 CLRR=CLR  
 CALL SAC2  
 ALPOL=ALPD  
 CDR=CDRR  
 75 CONTINUE  
 LR=CLR\*QR\*AREFF  
 DR=CDR\*QR\*AREFF  
 THETAR=GAMMPR+ALPOL\*DEGRAD  
 TTD=(LR\*SIN(GAMMPR)+DR\*COS(GAMMPR))/COS(THETAR)  
 IF (SWT2) GO TO 71  
 CLR=(AMASS\*GKEFF+DR\*SIN(GAMMPR)-TTD\*SIN(THETAR))/  
 (COS(GAMMPR)\*QR\*AREFF)  
 SWT2=.TRUE.  
 GO TO 70  
 71 HG1=AP5(XG77F-RGR)\*TAN(TMP1)+HGC  
 RR=SQRT((XG77F-RGR)\*\*2+ZG77F\*ZG77F)  
 MEA=RP\*DELEPS\*DEGRAD  
 ME=HGC7F-HGS  
 MED1=-ZG77F1+XG77F1\*TAN(TMP1)  
 MET=ME+RPH\*MED1

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O IF (ABS(HET) .GT. 1) GO HEAL ALPOES=ALPOES-PGS*HET
  IF (ALPOES.GT.1) ALPHOL ALPOES=ALPHOL
  IF (ALPOES.GT.ALPHOL) ALPOES=ALPHOL
  HPA=RR*DELSTG*DEGRAD
  HPT=YG77F+AFY*YG77F1
  IF (HPT.GT.HPA) GO TO 72
  IF (HPT.LT.(-HPA)) GO TO 73
  PHIOES=J.
  GO TO 74
72 PHIOES=-PHIC
  GO TO 74
73 PHIOES=PHIC

  CALL ENGINE FAILURE LOGIC

74 CALL ENGFL
  IF (IPR.EQ.1) CALL AUTPR2
  GO TO PITCH AUTOPILOT
  GO TO 9J

  TAKE OFF ROLL

  INPUT REQUIRED (FROM DIRCOM)
  VATO -AIRSPEED FOR TAKEOFF
  ALPHTO-ANGLE OF ATTACK FOR TAKEOFF
  HS -ALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF

  INPUT FROM SDF2 (DIRCOM)
  VA77F

  OUTPUT GENERATED
  ALPOL- DESIRED ANGLE OF ATTACK INPUT WHEN IAP GREATER OR =3J
  IAP -PROBLEM PHASE INDICATOR

20 IAP=5
  IF (VA77F.L1.VATO) GO TO 21
  IAP=6
  ALPOL=ALPHTO
21 IF (HR.GT.HS) GO TO 22
  CALL ENGINE FAILURE LOGIC
  CALL ENGFL
  GO TO PITCH AUTOPILOT
  QJESH=J.
  GO TO 9J
22 WRITE(6,23) HR,HS
  FORMAT(1H,5X,42) ALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF/
  *6X,5HHR = E15.8,10X,5HHS = E15.8)
  INDSIE=U
  RETURN

  LANDING P C L L

  INPUT REQUIRED FOR LANDING ROLL (FROM DIRCOM)
  TSP - TIME AFTER IMPACT TO STAGE SPOILERS
  TRV - TIME AFTER IMPACT TO REVERSE SIGNAL
  TCH - TIME AFTER IMPACT TO CHUTE SIGNAL
  TBK - TIME AFTER IMPACT TO BRAKE SIGNAL
  ISS = U, SPOILER SIGNAL INITIALIZATION
  ILR = U, REVERSE SIGNAL INITIALIZATION
  ICS = U, CHUTE SIGNAL INITIALIZATION
  IBS = U, BRAKE SIGNAL INITIALIZATION

  INPUT FROM SDF2 (DIRCOM)
  TIME

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O IF(IAP.EQ.4)GO TO 93
IF(IAP.EQ.5)GO TO 91
ALPD=ALPDES
CALL SACS
IF(IAP.LT.2)GO TO 97
RFALPH=RFALP2
PSH=PSH2
97 DELQC=DELQC2
ALPHAE=ALPHD-ALPDES
IF(DELTS.LE.1.E-6)GO TO 96
ALPOD1=(ALPDES-ADDIM1)/DELTS
96 IF(ABS(ALPOD1).GT.ALPOD)ALPOD1=0.
ADDIM1=ALPDES
ALPOD1=ALPOD1
ALPHRE=ALPHR1*RADEEG-ALPOD1
ALPHET=ALPHA1+RFALPH*ALPHRE
DELQDE=DELQN
SIGNN=SIGN(1.,ALPHAE)
IF(ABS(ALPHET).GE.DELALA)DELQDE=DELQN+PSH*ALPHET+SIGNN*DELQC
GO TO 92
93 IF(TH.LE.TST)GO TO 95
TMP1=DELQD1*(TA-TS1)
IF((DELQ1-DELQF).GE.0.)GO TO 94
DELQDL=DELQ1+TMP1
IF(DELQDE.GE.DELQF)DELQDE=DELQF
GO TO 92
95 DELQ1=DELQDE
GO TO 92
94 DELQDE=DELQ1-TMP1
IF(DELQDE.LE.DELQF)DELQDE=DELQF
GO TO 92
91 DELQDE=DELQTO
92 IF(DELQDE.LE.DELQL)DELQDE=DELQL
IF(DELQDE.GE.DELQU)DELQDE=DELQU
IF(IPR.EQ.0)CALL AUTPRS

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YAW AUTOPILOT

```

INPUT REQUIRED FOR YAW AUTOPILOT(DIRCOM)
RFB -RATE FEED BACK FOR SIDESLIP
DELBA -SIDE SLIP ERROR ALLOWED
PSR -PILOT SENSITIVITY IN SIDE SLIP OVER CONTROL
RFPST -RATE FEED BACK FOR PSIE
DPSIA -EULER YAW ERROR ALLOWED
PSPSI -PILOT SENSITIVITY IN EULER YAW CONTROL
DELRL -LOWER RUDDER LIMIT ON DELRDE
DELRU -UPPER RUDDER LIMIT ON DELRDE
IAP -PROBLEM PHASE INDICATOR

```

INPUT FROM SOF2(DIRCOM)  
BETAD,BETAR1,PSIPD

OUTPUT GENERATED BY YAW AUTOPILOT  
DELRN -NOMINAL RUDDER TRIM POSITION  
BETAE -SIDE SLIP POSITION ERROR  
BETAET-TOTAL SIDE SLIP ERROR  
DELRDE-DESIRED RUDDER POSITION  
PSIE -EULER YAW ANGLE POSITION ERROR  
PSIET -TOTAL EULER YAW POSITION ERROR

```

CALL SACS11
DELRN=DELRNN
IF(IAP.GT.2)GO TO 100
BETAE=BETAU
BETAET=BETAE+RFB*BETAR1*RADEEG

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```

DELRDE=DELRN
IF (ABS(BETAET),GE,DELHA) DELRDE=JELRN+PSR*BETAET
GO TO 100
PSIE=PSIAPJ
PSIET=PSIE+RFPST*PSIPQ*RADEG
DELRDE=DELRN
IF (ABS(PSIET),GE,OPSIAP) DELRDE=DELRN+PSPSI*PSIET
101 IF (DELRDE.LT,DELRLL) DELRDE=DELRLL
IF (DELRDE.GT,DELRUL) DELRDE=DELRUL
IF (IPR.EQ.1) CALL AUTPR6

      R O L L   A U T O P I L O T

      INPUT REQUIRED FOR ROLL AUTOPILOT(DIRCOM)
RFPHI -ROLL ANGLE RATE FEEDBACK
OPHIA -ROLL ANGLE ERROR ALLOWED
PSA -PILOT SENSITIVITY IN ROLL OVER CONTROL
DELPDE -LOWER AILERON LIMIT ON DELPDE
DELPDE -UPPER AILERON LIMIT ON DELPDE
IAP -PROBLEM PHASE INDICATOR

      INPUT FROM SDP2(DIRCOM)
PHIPD

      OUTPUT GENERATED BY ROLL AUTOPILOT
PHIE -ROLL ANGLE ERROR
PHIET -TOTAL ROLL ANGLE ERROR
DELPDE-DESIRED AILERON POSITION

IF (IAP.GT.3) GO TO 102
PHIE=PHIPD-PHICES
PHIET=PHIE+RFPHI*PHIPD*RADEG
IF (ABS(PHIET),LT,OPHIA) GO TO 102
DELPDE=PSA*PHIET
GO TO 103
102 DELPDE=J
103 IF (DELPDE.LT,DELPD) DELPDE=DELPD
IF (DELPDE.GT,DELPUL) DELPDE=DELPUL
IF (IPR.EQ.1) CALL AUTPR7

CALL THROTTLE AUTOPILOT
33 CALL THAUTS(IPR)

      B R A K E   A U T O P I L O T

      INPUT REQUIRED (FROM DIRCOM)
HBC(I) - BRAKING CONSTANT FOR STRUT I
PU - PER CENT SKID FOR CONTROLLED BRAKING
DELTA - PER CENT SPEED ERROR ALLOWED
OMEGR(I) - ACCELERATION TO OMEGR(I) DESIRED
HBL(I) - LOWER BRAKING MOMENT ALLOWED FOR STRUT I
HBU(I) - UPPER BRAKING MOMENT ALLOWED FOR STRUT I
MB(I) - BRAKING MOMENT INITIALLY READ IN
NSTRUT - NUMBER OF INDEPENDENT STRUTS(LGEAR MOD)
RZRO(I) - RADIUS OF TIRES ON EACH STRUT(LGEAR MOD)
NTIRES(I) - NUMBER OF TIRES ON EACH STRUT(LGEAR MOD)
MOMENT(I) - MOMENT OF INERTIA OF SINGLE ROTATING
WHEEL ON EACH STRUT(LGEAR MOD)
DELTA(I) - TIRE DEFLECTION FOR EACH GEAR(LGEAR MOD)

      OUTPUT GENERATED
OMEGTR(I) - DESIRED WHEEL SPEED FOR PD FOR STRUT I
OMTRD(I) - DESIRED WHEEL SPEED DECELLER FOR STRUT I
OMEGTE(I) - WHEEL SPEED ERROR FOR STRUT I

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MB(I) - BRAKING MOMENT FOR STRUT I
      OUTPUT GENERATED FOR LGEAR (IN DIRCOM)
      OMET(1,I),

      INPUT REQUIRED (FROM LGEAR)
      MA(I), OMET(1,I), VAXLE(I)

      INPUT REQUIRED SDF2(DIRCOM)
      AMASS, FX37P

DO 40 I=1,NSTRUT
  IF (INS.NE.1) GO TO 41
  IF (H(I)) 42,43,44
42  OMET(1,I)=0.
  GO TO 41
43  MB(I)=0.
  GO TO 41
44  IF (ID(I).GT.1) GO TO 45
  TMP1=-11.-PO)/(RZERO(I)-DELTA(I))
  OMEGTR(I)=VAXLE(I)*TMP1
  OMTRO1(I)=FX37P*TMP1/AMASS
  OMEGTE(I)=OMET(1,I)-OMEGTR(I)
  TMP1=0.
  IF (ABS(OMET(1,I)).LE.1.E-10) GO TO 48
  TMP1=ABS(OMET(1,I))/OMET(1,I)
48  IF (ABS(OMEGTE(I)).LT.ABS(DELTA*OMEGTR(I))) GO TO 46
  IF (OMEGTE(I).GT.0.) GO TO 47
  M3(I)=TMP1*(MA(I)-OMEGD1*MOMENT(I)*NTIRES(I))
  GO TO 41
45  MB(I)=MBC(I)
  GO TO 41
46  M4(I)=TMP1*(MA(I)-OMTRO1(I)*MOMENT(I)*NTIRES(I))
  GO TO 41
47  M4(I)=TMP1*(MA(I)+OMEGD1*MOMENT(I)*NTIRES(I))
41  IF (MB(I).LT.MBL(I)) MB(I)=MBL(I)
  IF (MB(I).GT.MBU(I)) MB(I)=MBU(I)
48  CONTINUE
  IF (IPR.EQ.1) CALL AUTPR9

      C O N T R O L   R E S P O N S E

      INPUT REQUIRED (FROM DIRCOM)
      DELPD - CONTROL SURFACE DEFLECTION (INPUT AND OUTPUT)
      DELQD - CONTROL SURFACE DEFLECTION (INPUT AND OUTPUT)
      DELRD - CONTROL SURFACE DEFLECTION (INPUT AND OUTPUT)
      DELHS - HORIZONTAL STABILIZER TIME RATE
      DELRRD - RUDDER TIME RATE
      DELA - AILERON TIME RATE
      NEO1 - ENGINE TIME RATE
      IN - NO. OF ENGINES
      DELTS - MAXIMUM INTEGRATION INTERVAL
      N(I) - THROTTLE POSITION FOR EACH ENGINE (INPUT AND OUTPUT)

      DELQD1=DELHS
      IF (DELQD.LT.DELQD) DELQD1=-DELHS
      DELRD1=DELRRD
      IF (DELRD.LT.DELRD) DELRD1=-DELRRD
      DELPD1=DELA
      IF (DELPD.LT.DELPD) DELPD1=-DELA
      DO 50 I=1,IN
      IF (ND(I).EQ.0.) GO TO 51
      IF (SMT(I)) GO TO 52
      IF (ND(I)) 56,58,58
      IF (PMDES(I)) 52,59,59

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```

29 IF (PNDES(I)) 59,52,52
30 N(I)=-N(I)
31 IF (ND(I)-N(I)) 53,54,54
32 ND(I)=-ND(I)
33 GO TO 55
34 NU1(I)=ND1
35 GO TO 55
36 N(I)=.
37 NU1(I)=0.
38 CONTINUE
39 SW1=.FALSE.
40 DO 55 I=1,IN
41 PNDES(I)=ND(I)
42 IF (ABS(DELQD1*DELTS).GE.ABS(DELQDE-DELQD)) GO TO 60
43 DELQD=DELQD+DELQD1*DELTS
44 GO TO 61
45 DELQD=DELQDE
46 IF (ABS(DELRD1*DELTS).GE.ABS(DELROE-DELRD)) GO TO 62
47 DELRD=DELRD+DELRD1*DELTS
48 GO TO 63
49 DELRD=DELROE
50 IF (ABS(DELPO1*DELTS).GE.ABS(DELPOE-DELPO)) GO TO 64
51 DELPO=DELPO+DELPO1*DELTS
52 GO TO 65
53 DELPO=DELPOE
54 DO 67 I=1,IN
55 IF (ABS(ND1(I)*DELTS).GE.ABS(ND(I)-N(I))) GO TO 66
56 N(I)=N(I)+NU1(I)*DELTS
57 GO TO 67
58 N(I)=ND(I)
59 CONTINUE
60 IF (IPR.EQ.1) CALL AUTP1
61 RETURN
62 END
63 SUBROUTINE FLARE1(IPR)
64 EXTERNAL ASIN

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#### FLARE

```

      INPUT REQUIRED(FROM DIRCOM)
XTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
HTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
VXTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
VHTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
IIR - IF=0, INITIALLY SET XRF, HRF, XRF01, HRF01 TO XTD,
      HTD, VXTD, VHTD
LD - SUSPECTED LANDING DISTANCE
JA - NUMBER OF INCREMENTS/DEG IN ALPHA SEARCH
YL - LOWER THRUST LIMIT ALLOWED IN FLARE
TU - UPPER THRUST LIMIT ALLOWED IN FLARE
PM - MAX. TAIL DOWN INTERFERENCE ANGLE AT TOUCHDOWN
ALPHDS - LOWER LIMIT ON ALPHA
ALPHDL - UPPER LIMIT ON ALPHA
HR

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      INPUT REQUIRED(FROM LGEAR-DIRCOM)
RLT - RUNWAY LENGTH(USED ALSO IN LGEAR)
ERDEG - RUNWAY ELEVATION ANGLE IN DEG(USED ALSO IN LGEAR)

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      INPUT REQUIRED(FROM SDF2-DIRCOM)
AMASS,DYNPP,AREFF,HTP7P
SGAMA,GAM7D,VG77F

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COMMON/DIRCOM/DM1(136),AMASS,DM2(25),AREFF,
*DM3(19),DYNPP,DM19(58),GAM7D,DM4(391),

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\*GAMA, DM13(13), VG77F, DM18(18), TR7P, DM5(165)  
 COMMON/DIRCOM/DA5(26), ERDEG, DM7(116), RLT, DM8(126)  
 COMMON/DIRCOM/DM9(36), XRF, HRF, DM12(110), ALPDES, IAP, DM16(3),  
 \*ALPHOS, ALPHOL, DM11(7), TTD, XTU, H10,  
 \*VXTD, VHTD, IIR, LD, DA, TL, TU, DM11(5), PH, DM12(169), HR, DM14(16),  
 \*XR, XRD1, HRD1, DM17(45), DM26(2068)

INPUT REQUIRED(FROM AUTS)  
 XR, XRD1, HRD1

OUTPUT GENERATED BY FLARE1  
 XRF - ACTUAL SELECTED TOUCHDOWN CONDITIONS(DIRCOM)  
 HRF - ACTUAL SELECTED TOUCHDOWN CONDITIONS(DIRCOM)  
 XRFD1 - ACTUAL SELECTED TOUCHDOWN CONDITIONS  
 HRFD1 - ACTUAL SELECTED TOUCHDOWN CONDITIONS  
 TX - TIME TO TOUCHDOWN X CONSTRAINT  
 TH - TIME TO TOUCHDOWN Y CONSTRAINT  
 DM - INCREASE OF TOUCHDOWN POINT PAST XTD.  
 RSR - TOUCHDOWN ALTITUDE RATE REQUIRED TO MEET TX=TH CONSTRAINT  
 AXR - REQUIRED ACCELERATION TO MEET TOUCHDOWN CONDITIONS  
 AHR - REQUIRED ACCELERATION TO MEET TOUCHDOWN CONDITIONS  
 GAMAFD - AIRSPEED FLIGHT PATH ANGLE RELATIVE TO RUNWAY  
 TTD - REQUIRED THRUST SATISFY AXR(DIRCOM)  
 IAP - PROBLEM PHASE INDICATOR (DIRCOM)  
 ALPDES - DESIRED ANGLE OF ATTACK (DIRCOM)

COMMON/AUTSC/TR, TC, TOX,  
 1TDA, TDB, TD(5), IRA, IRB, IRC, ICA, ICB,  
 2KA, KR, KEA, KEB, KT, NA, NNB, NC, ND(5), NRA, NRB, NRC,  
 3NLDA, NLRB, NLRC, NDA, NDB, NDC, NTOA, NTOB, NTOC

COMMON/AUTPRC/YR, ZR, YPD1, ZED1, PSIPD1, PHIPD1,  
 1VE, VAD, GAMPRD, GR, CLR, COR, LK, OR, IGS, RR, HEA, HE,  
 2HET, HPA, HPT, PHIES, TX, TH, XRFD1, HRFD1, AXR, AHR,  
 3ALPHA, ALPHD1, ALPHET, DELPH, BETAET, DELROE, DM,  
 4PHIE, PHIE, DELPDE, DELQD1, DELRQ1, DELPD1,  
 5ND1(5), CMGTR(5), DMTRD1(5), OMEGTE(5), PSIE, PSIET

COMMON/AUTSAC/ALPDR1, QDES, CL1, A1, CD1, DELRNN  
 LOGICAL SAT1  
 REAL LU, LI  
 DATA RADDEG, DEGRAD/57.2957795, .01745329/

IAP=2  
 IF (IIR.E7.1) GO TO 10  
 IIR=1  
 XRF=XTD  
 HRF=HTU  
 XRFD1=VXTD  
 HRFD1=VHTD  
 TMP1=XRF-XR  
 TMP2=XRD1+XRFD1  
 TMP3=HRF-HR  
 TMP4=HRFD1+HPD1  
 TMP5=TMP3\*TMP2/TMP4+XR-XTD  
 TX=2.\*TMP1/TMP2  
 TH=2.\*TMP3/TMP4  
 IF (TX-TH) 11, 30, 13  
 DM=TMP5  
 IF ((LD+DM).GT.RLT) GO TO 14  
 XRF=XTD+DM  
 TMP1=XRF-XR  
 GO TO 30  
 XRF=XTD+RLT-LD  
 TMP1=XRF-XR  
 HRFD1=TMP2\*TMP3/TMP1-HRD1

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Q GO TO 30
OH=TMP2
IF (OH.LT.1.) OH=1.
XRF=XTD+OH
TMP1=XRF-KR
TX=1.*TMP1/TMP2
IF (TX.LE.1.) GO TO 30
RSP=2.*TMP3/TX-HRD1
IF (RSP.GT.1.) GO TO 12
H(FD1)=RSP
GO TO 30
12 HRF01=1.
XRF01=HRD1*TMP1/TMP3-XRD1
30 TMP2=XRD1+XRF01
TMP4=HRF01+HRD1
AXR=(XRF01-XRD1)*TMP2/(2.*TMP1)
AHR=(HRF01-HRD1)*TMP4/(2.*TMP3)
GAMERR=(GAM/DEG-ERDEG)*DEGRAD
TMP1=SIN(GAMERR)
TMP2=COS(GAMERR)
QDESR=ALPHD1+(AHR*TMP2-AXR*TMP1)/VG77F
GAMMA0=ASIN(SGAMA)*RADDEG
GAMAP0=GAMMA0-ERDEG
GAMAP0=JEL-AU*GAMAP0
TMP1=SIN(GAMAP0)
TMP2=COS(GAMAP0)
ERRAD=ER)*C*DEGRAD
TMP1=WT*7P*SIN(ERRAD)
TMP4=WT*7P*COS(ERRAD)
TMP5=AMASS*AXR
SWT1=.FALSE.
ALPHD5
C CALL SACS TO FIND CL1 AND CO1 FOR ALPHA = A1
5 CALL SACS1
CALL SACS3
L1=CL1*OYNPP*AREFF
D1=CO1*OYNPP*AREFF
TMP6=DEGRAD*(A1+GAMAP0)
TTH=(TMP5+L1*TMP1+D1*TMP2+TMP3)/COS(TMP5)
IF (TTH.LT.TL) TTH=TL
IF (TTH.GT.TU) TTH=TU
IF (SWT1) GO TO 6
TTO=TTH
ALPOES=A1
6 AX=(TTH*COS(TMP6)-L1*TMP1-D1*TMP2-TMP3)/AMASS
AH=(TTH*SIN(TMP6)+L1*TMP2-D1*TMP1-TMP4)/AMASS
TAE=SQRT((AX-A1)**2+(AHR-AH)**2)
IF (SWT1) GO TO 7
AE=TAE
SWT1=.TRUE.
7 IF (TAE.GT.AE) GO TO 8
A=TAE
TTO=TTH
ALPOES=A1
8 A1=A1+DA
IF (A1.LE.ALPHD1) GO TO 5
PHIDES=1.
IF (IPR.EQ.1) CALL AUTPR3
RETURN
ENTRY FLARE2
GAMMA0=ASIN(SGAMA)*RADDEG
GAMAP0=GAMMA0-ERDEG
TAP=3
PHIDES=1.
O IF ((ALPOES+GAMAP0).GT.PM) ALPOES=PM-GAMAP0

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CALL STFL(2,2,PRT5)
CALL STOVAR(2,2,TT,TR,DU,DU,DU,DU,DU,DU)
CALL STFL(,1,DU)
RETURN

C
C
C ENTRY FOR PRINTING PITCH AUTOPILOT DATA
C
C ENTRY AUTPR5
C IF (PITCHP.EQ.) RETURN
C CALL LINES(1)
C WRITE(6,DU)
50 FORMAT(5X,15HPITCH AUTOPILOT)
C CALL STFL(2,6,PRT6)
C ALPHD1=ALPHR1*57.2957795
C CALL STOVAR(6,DELON,ALPHA,ALPHD1,ALPD01,ALPHET,DELQDE,
1 DU,DU)
C CALL STFL(,1,DU)
C RETURN

C
C
C ENTRY FOR PRINTING YAW AUTOPILOT DATA
C
C ENTRY AUTPR6
C IF (YAWAP.EQ.) RETURN
C CALL LINES(1)
C WRITE(6,DU)
60 FORMAT(5X,15HYAW AUTOPILOT)
C CALL STFL(2,7,PRT7)
C BETAD1=BETAR1*57.2957795
C CALL STOVAR(7,DELRN,BETAD,BETAD1,BETAET,DELRDE,
1 PSIE,PSIET,DU)
C CALL STFL(,1,DU)
C RETURN

C
C
C ENTRY FOR PRINTING ROLL AUTOPILOT
C
C ENTRY AUTPR7
C IF (ROLLAP.EQ.) RETURN
C CALL LINES(1)
C WRITE(6,DU)
70 FORMAT(5X,14HROLL AUTOPILOT)
C CALL STFL(2,3,PRT8)
C CALL STOVAR(3,PHIE,PHIET,DELPDE,DU,DU,DU,DU,DU)
C CALL STFL(,1,DU)
C RETURN

C
C
C ENTRY FOR PRINTING THROTTLE AUTOPILOT
C
C ENTRY AUTPR8
C IF (THROAP.EQ.) RETURN
C CALL LINES(3)
C WRITE(6,DU)
80 FORMAT(5X,18HTHROTTLE AUTOPILOT)
C WRITE(6,81) (ND(I),I=1,IN)
81 FORMAT(21X,9HNC(IN) = E15.8,4(5X,E15.8))
C WRITE(6,82) (TD(I),I=1,IN)
82 FORMAT(21X,9HTD(IN) = E15.8,4(5X,E15.8))
C RETURN

C
C
C ENTRY FOR PRINTING BRAKE AUTOPILOT
C
C ENTRY AUTPR9
C IF (BRAKAP.EQ.) RETURN
C CALL LINES(2)
C WRITE(6,DU) (MB(I),I=1,NSTRUT)
C FORMAT(5X,15HBRAKE AUTOPILOT/21X,9HMB(1) = E15.8,

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O C4(IX,E15.8))RETURN
  IF(105.NC.1)RETURN
  CALL LINE3(3)
  WRITE(6,11) (OMEGATR(I),I=1,NSTRUT)
91  FORMAT(17X,13HOMEGAT(I) = E15.8,4(5X,E15.8))
  WRITE(6,12) (OMTRUI(I),I=1,NSTRUI)
92  FORMAT(15X,15HOMEGATROI(I) = E15.8,4(5X,E15.8))
  WRITE(6,13) (OMEGTE(I),I=1,NSTRUT)
93  FORMAT(17X,13HOMEGATE(I) = E15.8,4(5X,E15.8))
  RETURN

C00 ENTRY FOR PRINTING CONTROL RESPONSE DATA

  ENTRY AUTOPILOT
  IF(CONTRP.EQ.1)GO TO 12
  CALL LINE3(1)
  WRITE(6,14)
100  FORMAT(18X,16HCONTROL RESPONSE)
  CALL STFL(2,6,PRT9)
  CALL STOVAR(6,DELQD1,DELQD1,DELQD1,DELQD,DELQD,
101  DELQD,DU,DU)
  CALL STFL(1,1,DU)
  CALL LINE3(2)
  WRITE(6,15) (ND1(I),I=1,IN)
101  FORMAT(24X,6HND1 = E15.8,4(5X,E15.8))
  WRITE(6,16) (M(I),I=1,IN)
102  FORMAT(24X,6HM = E15.8,4(5X,E15.8))

C00 WRITING OF INDICATORS

12  IF(INDICP.EQ.1)RETURN
  CALL LINE3(2)
  WRITE(6,11) IAP, (IC(I),I=1,4), (I(J),J=1,5)
11  FORMAT(61X,16HINDICATORS/33X,5HTAP = I2,10X,
  C7HIC(I) = I2,1H,,I2,1H,,I2,1H,,I2,1H,,I2,1H,,I2,
  C7HIB(I) = I2,1H,,I2,1H,,I2,1H,,I2,1H,,I2,1H,,I2)
  RETURN
  END
  SUBROUTINE THAUTS(IPR)

  THRITTLE AUTOPILOT

    INPUT REQUIRED (FROM DIPCOM)
    TF(I) - FIX ARRAY FOR ENGINE I
    NJF(I) - THROTTLE SETTING FOR TF(I)
    IR(I) - REVERSE CAPABILITY ARRAY FOR ENGINE I
    NR(I) - THROTTLE CONSTRAINT ARRAY FOR REVERSE FOR ENG. I
    NLR(I) - REVERSE THROTTLE SETTING FOR REVERSE SIGNAL ON LANDING
    NTO(I) - TAKE OFF THROTTLE SETTING FOR ENGINE I
    KE(I) - KILL ENGINE OPTION FOR ENG. I FOR HOLD MODE
    THE FOLLOWING ARE ENGINE LOAD CONSTANTS FOR VARIABLE
    ENGINE COMBINATIONS
    K2 - K(2)121
    K3(I) - K(3)131, K(3)232, K(3)121, K(3)1231, K(3)1232
    K4(I) - K(4)141, K(4)232, K(4)343, K(4)242, K(4)2342,
    K(4)2343, K(4)1341, K(4)1343, K(4)12341,
    K(4)12342, K(4)12343
    IN - NUMBER OF ENGINES
    ILR - REVERSE SIGNAL INITIALIZATION
    IAP - PROBLEM PHASE INDICATOR
    ITD - DESIRED THRUST

    INPUT FROM SDF2(DIRCOM)
    N(I)

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COMMON/DIRCON/DM1(58),IN,DM2(12),N(5),DM3(27),IAP,DM8(12),TTO,
*DM4(9),XC(5),DM5(6),ILR,DM9,IC(5),DM6(84),
*TF(5),NDF(2),IR(5),N3(5),
*NLP(5),NTU(5),K2,K3(5),K4(11),DM7(91),DM8(2066)

      INPUT FROM AUTS
      TD(1),TDA,TDB,IC(1),NOA,NDB,NDC

      OUTPUT GENERATED FOR AUTS
      TO(1),TC,TDX,IRA,IRB,IRC,NA,NC,ND(1),NBA,NBB,NBC,
      NLRA,NLRH,NLRC,NTOA,NTOB,NTOC,KA,KB,KT,KEA,
      KEB,ICA,ICB,NCB

      COMMON/AUTSC/TR,TC,TDX,
      1TDA,TDB,TU(5),IRA,IRB,IRC,ICA,ICB,
      2KA,KB,KEA,KEB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,
      3NLRA,NLRB,NLRC,NOA,NDB,NDC,NTOA,NTOB,NTOC

      REAL NDF,NU,N,NNB,NLR,NTU,K2,K3,K4,KA,KB,
      1NA,NC,ND,NBA,NBB,NBC,NLRA,NLRB,NLRC,
      2NTOA,NTOB,NTOC,NOA,NDB,NDC

      COMMON/AUTPRC/YR,ZR,YRD1,ZRD1,PSIP01,PHIPU1,
      1VE,VAQ,GAMPPD,QR,CLD,COR,LR,OR,HGS,RR,HEA,HE,
      2HEI,HPI,HPT,PHICES,TX,TM,XRF01,XRFU1,AXR,AHR,
      3ALPHA,ALPU01,ALPHET,DELNR,BETAET,DELROE,DM,
      4PHIE,PHIT,DELPOE,DELPO1,DELRO1,DELPO1,
      5NU(5),OMEGIR(5),OMTRO1(5),OMEGTE(5),PSIE,PSIET

      INTEGER TF
      CHECK ENGINE NO.
      DO 1 I=1,IN
      ND(I)=0.
      TO(I)=0.
      IF(IN-2)10,20,5
      IF(IN-4)30,40,4J

      SINGLE ENGINE LOGIC
10  IF(TF(1).EQ.1)GO TO 11
      IF(IC(1).EQ.1)GO TO 12
      SET UP DATA FOR COMMON ENGINE LOGIC
      TU(1)=TTO
      IRC=IR(1)
      NC=N(1)
      NBB=NB(1)
      NLRC=NLR(1)
      NTUC=NTU(1)
      TC=TD(1)
      KT=KE(1)
      CALL COMMON ENGINE LOGIC
      CALL CENGL
      ND(1)=NDC
      GO TO 4J
11  ND(1)=NDF(1)
      IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
      IF(IC(1).NE.0)GO TO 200
12  NU(1)=0.
      GO TO 200

      TWO ENGINE LOGIC
20  IF((TF(1).EQ.1).OR.(TF(2).EQ.1))GO TO 21
      TDX=TTO
      ICA=IC(1)

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O   IRA=IR(1)
    NA=NI(1)
    NHA=NI(1)
    NLRA=NLR(1)
    NTOA=NTO(1)
    KEA=KE(1)
    KA=K(1)
    ICD=IC(2)
    ICB=IC(2)
    NNB=NL(1)
    NNB=N(2)
    NLRB=NLR(2)
    NTOB=NTO(2)
    KEB=KE(2)
    KB=K(2)
C   CALL COMMON TWO ENGINE LOGIC
    CALL CTENL
    TJ(1)=TDA
    TJ(2)=TDJ
    NJ(1)=NDA
    NJ(2)=NDB
    GO TO 23J
21  ND(1)=NDF(1)
    ND(2)=NDF(2)
    IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
    IF(ILR.EQ.1)ND(2)=ENGREV(IR(2),N(2),NB(2),NLR(2))
    IF(IC(1).EQ.0)ND(1)=0.
    IF(IC(2).EQ.0)ND(2)=0.
    GO TO 23J
C   THREE ENGINE LOGIC
    NOTE( ONCE AN ENGINE IS STOPPED, IT STAYS FIXED
    EXCEPT TO FAIL
C   DO 31 I=1,3
    IF(TF(I).NE.1)GO TO 22
31  CONTINUE
    DO 23 I=1,3
    NJ(1)=NDF(1)
    IF(ILR.EQ.1)ND(I)=ENGREV(IR(I),N(I),NB(I),NLR(I))
    IF(IC(I).EQ.0)ND(I)=0.
23  CONTINUE
    GO TO 23J
22  IF((TF(1).EQ.1).AND.(TF(3).EQ.1))GO TO 24
    IF(TF(2).NE.1)GO TO 50
    ND(2)=NDF(2)
    IF(ILR.EQ.1)ND(2)=ENGREV(IR(2),N(2),NB(2),NLR(2))
    IF(IC(2).EQ.0)ND(2)=0.
    CALL TFFS(ND(2),TD(2))
26  TDX=TTD-TD(2)
    I1=1
    I2=3
    I3=0
27  ICA=IC(I1)
    ICB=IC(I2)
    IRA=IR(I1)
    IRB=IR(I2)
    NA=N(I1)
    NNB=N(I2)
    NBA=NB(I1)
    NBB=NB(I2)
    NLRA=NLR(I1)
    NLRB=NLR(I2)
    NTOA=NTO(I1)

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) NIOB=NTO(I2)
KEA=KE(I1)
KEB=KE(I2)
I4=I1+I3
KA=KJ(I4)
K3=1.-KJ(I4)
C CALL COMMON TWO ENGINE LOGIC
CALL CTENGL
T(I1)=TUA
T(I2)=TOJ
ND(I1)=NOA
ND(I2)=NOB
GO TO 24
24 ND(1)=NOF(1)
ND(3)=NOF(3)
IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
IF(ILR.EQ.1)ND(3)=ENGREV(IR(3),N(3),NB(3),NLR(3))
IF(IC(1).EQ.0)ND(1)=J.
IF(IC(3).EQ.0)ND(3)=J.
CALL TFFS9(NL(1),TU(1))
CALL TFFS9(ND(3),TO(3))
IF(IC(1).EQ.0)GO TO 51
TU(2)=TU-TD(1)-TO(3)
I1=2
I3=1
26 IRC=TR(I1)
NC=N(I1)
NGC=ND(I1)
NLRC=NLR(I1)
NTOC=NTO(I1)
TC=TO(I1)
C KT=KE(I1)
CALL COMMON ENGINE LOGIC
CALL CLNGL
ND(I1)=NOC
GO TO (24,56,57,29),I3
29 GO TO 200
51 ND(2)=J.
GO TO 27
50 IF(IC(1).EQ.0)GO TO 60
IF(IC(2).NE.0)GO TO 55
ND(2)=J.
CALL TFFS9(ND(2),TO(2))
GO TO 26
60 ND(1)=J.
CALL TFFS9(ND(1),TU(1))
TUX=TTU-TD(1)
I1=2
I2=3
I3=0
GO TO 27
55 IF(IC(3).EQ.0)GO TO 58
TO(1)=TTO*KJ(4)
I1=1
I3=2
GO TO 28
56 TO(2)=TTI*KJ(5)
I1=2
I3=3
GO TO 28
57 TO(3)=TTO-TD(1)-TO(2)
I1=3
I3=4
GO TO 28
ND(3)=0.

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      IF (IC(1).NE.0) GO TO 93
81  CONTINUE
      GO TO 92
82  DO 82 I=1,3
      IF (IC(I).NE.0) GO TO 91
      CONTINUE
      GO TO 97
91  IF ((IC(1).NE.0).OR.(IC(2).NE.0)) GO TO 100
      IF (IC(4).NE.0) GO TO 100
      NJ(1)=J.
      NJ(2)=J.
      NJ(4)=J.
      CALL TFF33(3.,TD(1))
      TD(2)=TD(1)
      TD(4)=TD(1)
      TD(3)=TTD-TD(1)-TD(2)-TD(4)
      I1=3
      I2=1
83  IRC=IR(I1)
      NC=N(I1)
      NDC=NB(I1)
      NLRC=NLR(I1)
      NTOC=NTD(I1)
      TC=TD(I1)
      KT=KE(I1)
      CALL GENGL
      NDC(I1)=NDC
      GO TO (84,101,102,103,111,121,131,141,151,152,161,162),I2
84  GO TO 230
95  DO 95 I=1,4
96  NJ(I)=J.
      GO TO 26.
97  DO 98 I=1,3
98  NJ(I)=J.
      CALL TFF33(0.,TD(1))
      TD(2)=TD(1)
      TD(3)=TD(1)
      TD(4)=TTD-TD(1)-TD(2)-TD(3)
      I1=4
      I2=1
      GO TO 83
100 IF ((IC(1).EQ.0).AND.(IC(2).EQ.0)) GO TO 110
      IF ((IC(1).EQ.0).AND.(IC(3).EQ.0)) GO TO 120
      IF ((IC(1).EQ.0).AND.(IC(4).EQ.0)) GO TO 130
      IF ((IC(2).EQ.0).AND.(IC(3).EQ.0)) GO TO 140
      IF (IC(1).EQ.0) GO TO 150
      IF (IC(2).EQ.0) GO TO 160
      I1=1
      I2=2
      TD(1)=TTD*K4(9)
      GO TO 83
101 TD(2)=TTD*K4(10)
      I1=2
      I2=3
      GO TO 83
102 TD(3)=TTD*K4(11)
      I1=3
      I2=4
      GO TO 83
103 TD(4)=TTD-TD(1)-TD(2)-TD(3)
      I1=4
      I2=1
      GO TO 83
110 NJ(1)=J.
      NJ(2)=J.

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C CALL TFFS3(0.,TD(1))
  TD(2)=TD(1)
  TD(3)=(TTO-TD(1)-TD(2))*K4(3)
  I1=3
  I2=5
  GO TO 83
111 TD(4)=(TTO-TD(1)-TD(2))*(1.-K4(3))
  I1=4
  I2=1
  GO TO 83
120 NO(1)=0.
  NO(3)=0.
  CALL TFFS3(0.,TD(1))
  TD(3)=TD(1)
  TD(2)=(TTO-TD(1)-TD(3))*K4(4)
  I1=2
  I2=6
  GO TO 83
121 TD(4)=(TTO-TD(1)-TD(3))*(1.-K4(4))
  I1=4
  I2=1
  GO TO 83
130 NO(1)=0.
  NO(4)=0.
  CALL TFFS3(0.,TD(1))
  TD(4)=TD(1)
  TD(2)=(TTO-TD(1)-TD(4))*K4(2)
  I1=2
  I2=7
  GO TO 83
131 TD(3)=(TTO-TD(1)-TD(4))*(1.-K4(2))
  I1=3
  I2=1
  GO TO 83
140 NO(2)=0.
  NO(3)=0.
  CALL TFFS3(0.,TD(2))
  TD(3)=TD(2)
  TD(1)=(TTO-TD(2)-TD(3))*K4(1)
  I1=1
  I2=8
  GO TO 83
141 TD(4)=(TTO-TD(2)-TD(3))*(1.-K4(1))
  I1=4
  I2=1
  GO TO 83
150 NO(1)=0.
  CALL TFFS3(0.,TD(1))
  TD(2)=(TTO-TD(1))*K4(5)
  I1=2
  I2=9
  GO TO 83
151 TD(3)=(TTO-TD(1))*K4(6)
  I1=3
  I2=10
  GO TO 83
152 TD(4)=(TTO-TD(1))*(1.-K4(5)-K4(6))
  I1=4
  I2=1
  GO TO 83
160 NO(2)=0.
  CALL TFFS3(0.,TD(2))
  TD(1)=(TTO-TD(2))*K4(7)
  I1=1
  I2=11
C

```



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161 GO TO 83
   TD(3)=(TD-TD(2))*K4(8)
   I1=3
   I2=12
   GO TO 83
162 TD(4)=(TD-TD(2))*(1.-K4(7)-K4(6))
   I1=4
   I2=1
   GO TO 83
260 IF(IIP.EQ.1)CALL AUTPR8
   RETURN
END
FUNCTION ENGREV(IRC,NC,NBC,NLRC)
REAL NC,NBC,NLRC
IF(IRC.EQ.1)GO TO 1
ENGREV=1.
RETURN
1 IF(NC.GT.NBC)GO TO 2
ENGREV=NLRC
RETURN
END
SUBROUTINE ENGFL
      INPUT REQUIRED (FROM DIRCOM)
XRF1 - FIRST RUNWAY POSITION TO STAGE ENGINE FAILURE
IT1(I)- ARRAY ASSOCIATED WITH XRF1
XRF2 - SECOND RUNWAY POSITION TO STAGE ENGINE FAILURE
IT2(I)- ARRAY ASSOCIATED WITH XRF2
H1 - FIRST ALT. TO STAGE ENGINE FAILURE IN GLIDE SLOPE
IH1(I)- ARRAY ASSOCIATED WITH H1
H2 - SECOND ALT. TO STAGE ENGINE FAILURE IN GLIDE SLOPE
IH2(I)- ARRAY ASSOCIATED WITH H2
HR1 - FIRST ALT. TO STAGE ENGINE FAILURE IN FLARE
IHR1(I) ARRAY ASSOCIATED WITH HR1
HR2 - SECOND ALT. TO STAGE ENGINE FAILURE IN FLARE
IHR2(I) ARRAY ASSOCIATED WITH HR2
TR1 - FIRST TIME AFTER IMPACT TO STAGE ENGINE FAILURE
ITR1(I) ARRAY ASSOCIATED WITH TR1
TR2 - SECOND TIME AFTER IMPACT TO STAGE ENGINE FAILURE
ITR2(I) ARRAY ASSOCIATED WITH TR2
IAP - PROBLEM PHASE INDICATOR

      INPUT FROM SDF (DIRCOM)
HGC7F
COMMON/DIRCOM/DM1(434),HGC7F,DM2(1193),IAP,DM3(35),
*IC(5),XRF1,IT1(5),XRF2,IT2(5),H1,IH1(5),H2,IH2(5),
*HR1,IHR1(5),HR2,IHR2(5),TR1,ITR1(5),TR2,ITR2(5),DM4(109),HR,
*DM5(16),XR,DM6(47),DM7(2068)

      INPUT FROM AUTS
XR, TR

      OUTPUT GENERATED
IC(I) - INITIALIZATION OF FAILURE INDICATOR OF ENGINE I
COMMON/AUTSC/TR,IC,TDX,
1TDA,TDB,TD(5),IRA,IRB,IRC,ICA,ICD,
2KA,KB,KCA,KCB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,
3NLRA,NLNB,NLNC,NDA,NDB,NDC,NTOA,NTOB,NTOC

ENGINE FAILURE LOGIC
(ONCE AN ENGINE FAILS-MUST REMAIN FAILED)
IF(IAP-2)1,2C,3J
IF(HGC7F.GT.H1)GO TO 11

```

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```

12 DO 12 I=1,4
11 IC(I)=IH1(I)
13 IF (HGC7F,GT,H2) RETURN
13 DO 13 I=1,4
13 IC(I)=IH2(I)
13 RETURN
20 IF (HR,GT,HR1) GO TO 21
22 DO 22 I=1,4
22 IC(I)=IH3(I)
21 IF (HR,GT,HR2) RETURN
23 DO 23 I=1,4
23 IC(I)=IH2(I)
23 RETURN
30 IF (IAP-4) 24,40,50
40 IF (TR,LT,TR1) GO TO 41
40 DO 40 I=1,4
42 IC(I)=ITR(I)
41 IF (TR,LT,TR2) RETURN
43 DO 43 I=1,4
43 IC(I)=IT2(I)
43 RETURN
50 IF (XR,LT,XRF1) GO TO 51
50 DO 50 I=1,4
52 IC(I)=IT1(I)
51 IF (XR,LT,XRF2) RETURN
53 DO 53 I=1,4
53 IC(I)=IT2(I)
53 RETURN
END
SUBROUTINE CENGL
COMMON ENGINE LOGIC
      INPUT FROM DIRCOM
      ILR, IAP
COMMON/DIRCOM/DM1(1628),IAP,DM2(33),ILR,DM3(228),DM4(2068)
      INPUT FROM AUTS
      TC, IRC, NC, NBC, KT, NTOC, NLRC
      OUTPUT GENERATED FOR AUTS
      NJC
COMMON/AUTSC/TR,TC,TOX,
1TDA,TDU,T(5),IRA,IRB,IRC,ICA,ICB,
2KA,KB,KEA,KEB,KT,NA,NNE,NC,NUIS,NOA,NBB,NBC,
3NLCA,NLRC,NLRC,NOA,NBB,NOC,NTOA,NTOB,NTOC
C
      REAL N,NC,NBC,NLRC,NTOC,NOC
      IF (ILR.EQ.1) GO TO 10
      IF (IAP-3) 11,12,13
      CALL TFFS8(I,C,N)
      IF (N,GT,.) GO TO 20
      IF (IRC,NE.1) GO TO 21
      IF (NC,GT,NOC) GO TO 21
      NJC=N
      RETURN
      NJC=1.
      RETURN
      IF (KT,NE.1) GO TO 11
      GO TO 21
      IF (IAP,LT,5) GO TO 12
      NJC=NTOC
      RETURN

```

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```

) IF (IRC.NE.1) GO TO 21
  IF (NC.GT.NBC) GO TO 21
  NDC=NLRC
  RETURN
END
SUBROUTINE CTENGL
COMMON TWO ENGINE LOGIC

      INPUT FROM AUTS
ICA, ICB, IRR, NNB, NUB, NLRU, NTOB, TOB, KEB, NDC, TOX,
IRA, NA, NUA, NLRA, NTOA, TDA, KEA, KA, KB
TOB
      OUTPUT GENERATED FOR AUTS
NUA, NDB, IRC, NC, NDC, NLRC, NTOC, TC, KT, NDB
TDA, TUB

COMMON/AUTS/TR,TC,TDX,
1 TUA,TUB,TD(5),IRA,IRR,IRC,ICA,ICB,
2 KA,KB,KEA,KEB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,
3 NLRA,NLRB,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC

C
  REAL KA,KB,NA,NNB,NC,NBA,NBB,NDC,NDA,NDB,NDC,NLRA,
1 NLRB,NLRC,NTOA,NTOB,NTOC
  IF ((ICA.EQ.0).AND.(ICB.EQ.0)) GO TO 30
  IF (ICA.EQ.0) GO TO 20
  IF (ICB.EQ.0) GO TO 10
  TDA=KA*TUX
  IRC=IRA
  NC=NA
  NDC=NBA
  NLRC=NLRA
  NTOC=NTOA
  TC=TDA
  KT=KEA
  CALL CTENGL
  NJA=NDC
  TOB=KB*TDX
5  IRC=IRU
  NC=NNB
  NDC=NBB
  NLRC=NLRB
  NTOC=NTOB
  TC=TUB
  KT=KEB
  CALL CTENGL
  NDB=NDC
  RETURN
10 NDB=0.
  CALL TFFS3(0.,TOB)
  TDA=TDX-TOB
  IRC=IRA
  NC=NA
  NDC=NBA
  NLRC=NLRA
  NTOC=NTOA
  TC=TDA
  KT=KEA
  CALL CTENGL
  NJA=NDC
  RETURN
20 NDA=0.
  CALL TFFS3(0.,TDA)
  TUB=TUX-TDA
  GO TO 5

O
O
  NDA=0.
  NDB=0.
  RETURN
END

```

## APPENDIX B

### DERIVATION OF AERODYNAMIC WEIGHTING FACTORS

## AERODYNAMIC WEIGHTING FACTORS

In the TOLA computer program, the aerodynamic effects are treated as concentrated loads in the form of total aerodynamic forces and moments acting at a reference point on the airframe. These quantities are calculated in the aerodynamics subprogram (SACS) and are defined as follows:

- a - axial force (body axis)
- y - side force (body axis)
- n<sub>f</sub> - normal force (body axis)
- l - moment about body X axis
- m - moment about body Y axis
- n - moment about body Z axis

To obtain realistic flexible body response to these aerodynamic loads, weighting effects or participation factors, PF(I), for the response of each normal mode are required.

An approach to determine the weighting effect for the Z translational degree of freedom is given below. A similar method can be used to determine the remaining participation factors.

In TOLA, the generalized aerodynamic force is calculated as the product of the total lift, the vertical modal deflection at the reference point, and a participation factor

$$Q_{AZ} = n_f \phi_{Z_R} PF$$

If the actual generalized force due to aerodynamics is obtained by integrating the product of the pressure distribution and modal deflection over the lifting area, the expression for this quantity would be given as

$$Q_{AZ} = \int_A \phi_Z(x,y) P(x,y) dA$$

Equating the two force expressions, an equation for the participation factor can be obtained.

$$PF = \frac{\int_A \phi_Z(x,y) P(x,y) dA}{n_f \phi_{Z_R}}$$

APPENDIX C

PROGRAM LISTING, PLTDAT COMPUTER PROGRAM

```

PROGRAM PLT0AT(INPUT,TAPE3,TAPE1,OUTPUT,TAPE4),
DIMENSION TITLE(15),BUF(400),NOIL(28),TBUF(400),
*AVL(4,6),
*BMM(2,400),CHMODS(5),DEPVAR(5),LINE(7),NOVA(5)
DATA CHMODS/4HPLOT,6HTITLE1,6HTITLE2,6HINOVAR,6HDEPVAR/
DATA NPUT/5LINPUT/
READ(NPUT,105)NPTS
105 FORMAT(I6)
READ(3) NHL
NW=C
NOL=
NHL=NHL-1
DO 10 N=1,NHL
READ(3) NI,ND,(TITLE(I),I=1,NI)
106 FORMAT(2I6,3A6)
IF (ND.GT.1) GO TO 7
NS=NW+1
NOL=NOL+1
NOIL(NOL)=NI
107 FORMAT(13A10)
ENCODE(13J,100,TBUF(NS))(TITLE(I),I=1,NI)
NW=NW+NI
GO TO 10
7 DO 8 J=1,ND
NS=NS+1
NOL=NOL+1
NOIL(NOL)=NI
IF (J.LE.9) GO TO 111
ENCODE(13J,11,TBUF(NS))(J,TITLE(I),I=1,NI)
111 FORMAT(13(12,A8))
GO TO 112
111 ENCODE(13J,113,TBUF(NS))(J,TITLE(I),I=1,NI)
113 FORMAT(13(*C*,11,A8))
112 NW=NW+NI
8 CONTINUE
10 CONTINUE
READ(3) IX
DO 15 I=1,NW
BMM(1,I)=1.E60
15 BMM(2,I)=-1.E60
K=
30 NOI=
DO 35 N=1,NOL
NIL=NOIL(N)
READ(3) (BUF(I+NOI),I=1,NIL)
IF (EOF(3)) GO TO 35
35 NOI=NOI+NIL
READ(3) ENDPNT
WRITE(4) (BUF(I),I=1,NW)
DO 36 I=1,NW
BMM(1,I)=AMIN1(BMM(1,I),BUF(I))
36 BMM(2,I)=AMAX1(BMM(2,I),BUF(I))
K=K+1
IF (K.GT.NPTS) GO TO 50
GO TO 30
50 DO 51 I=1,15
51 TITLE(I)=10H
NIV=
NOV=
KT1=
KT2=
CALL PLOTS(DUM,DUM,10)
CALL PLOT(.,1,-3)
60 READ(NPUT,90)CHMOD,LINE
90J FORMAT(10A10)

```



```

59 IF (EOF, NPUT) 9., 59
   DO 61 K=1,5
   IF (CMMD, EQ, CMMDS(K)) GO TO (80, 62, 63, 65, 66), K
61 CONTINUE
   PRINT 300, CMMD
300 FORMAT(* IMPROPER COMMAND=*, A10)
   STOP
62 CNCODE(40, 10., TITLE(1)) (LINE(I), I=1, 4)
   KT1=KT8(TITLE(1), 4.)
   GO TO 60
63 CNCODE(40, 10., TITLE(5)) (LINE(I), I=1, 4)
   KT2=KT8(TITLE(5), 4.)
   GO TO 60
65 CALL FIND(TBUF, NH, LINE(1), NIV)
   IF (NIV, NE, .) GO TO 70
   PRINT 31., LINE(1)
310 FORMAT(* IMPROPER INDEPENDENT VARIABLE=*, A10)
   STOP
70 AVAL(1, 1)=BMM(1, NIV)
   AVAL(2, 1)=BMM(2, NIV)
   GO TO 60
66 NDV=
   DO 69 N=1, 5
   IF (LINE(N), EQ, 1H ) GO TO 67
   CALL FIND(TBUF, NH, LINE(N), NOVA(N))
   IF (NOVA(N), NE, .) GO TO 68
   PRINT 320, LINE(N)
320 FORMAT(* IMPROPER DEPENDENT VARIABLE *, A10)
   STOP
67 NDV=N-1
   GO TO 60
68 NOX=NOVA(N)
   AVAL(1, N+1)=BMM(1, NOX)
   AVAL(2, N+1)=BMM(2, NOX)
   CALL SCALE(AVAL(1, N+1), 6., 2, 1)
69 CONTINUE
   NDV=5
   GO TO 60
80 IF (NIV, NE, .) GO TO 81
   PRINT 330
330 FORMAT(* NO INDEPENDENT VARIABLE*)
   STOP
81 IF (NDV, NE, .) GO TO 82
   PRINT 340
340 FORMAT(* NO DEPENDENT VARIABLES*)
   STOP
82 IF (KT1, NE, .) CALL LABEL(1., 6.5, 10., 6.5, TITLE(1), KT1,
   * 3, 2, 0., 0., 0.)
   IF (KT2, NE, .) CALL LABEL(1., 6.1, 10., 6.1, TITLE(5), KT2,
   * 2, 2, 0., 0., 0.)
   CALL PLOT(NDV*.6+.5, ., -3)
   AXLEN=10.-NDV*.6
   CALL SCALE(AVAL(1, 1), AXLEN, 2, 1)
   CALL AXIS(0., 0., TBUF(NIV), -10, AXLEN, 0., AVAL(3, 1), AVAL(4, 1))
   DO 89 J=1, NDV
   JD=NOVA(J)
   REWIND 4
   IP=3
83 NLAD(4) (BUF(I), I=1, NH)
   IF (EOF, 4) 85, 84
84 VARIND=(BUF(NIV)-AVAL(3, 1))/AVAL(4, 1)
   VARDEP=(BUF(JD)-AVAL(3, J+1))/AVAL(4, J+1)
   IF (IP, EQ, 3) CALL SYMBOL(VARIND, VARDEP, .1, J, 0., -1)
   IF (IP, NE, 3) CALL PLOT(VARIND, VARDEP, 2)
   IP=2

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85 GO TO 84
   NSUB=NDVA(J)
   CALL AXIS(-(J-1)*.6,.1,TBUF(NSUB),10,6.,90.,AVAL(3,J+1),
   *AVAL(4,J+1))
   CALL SYMBOL(-(J-1)*.6-.4,1.,.14,J,90.,-1)
89 CONTINUE
   CALL PLOT(AXLEN+1.,0.,-3)
   GO TO 6C
93 CALL PLOT(.,0.,999)
   STOP
END
FUNCTION KTB(ISTRG,IST)
  DIMENSION ISTRG(1)
  DO 2 I=1,IST
    KTB=ISTRG(I)-1
    NWJ=(KTB+3)/11
    NBITS=8*MOD(KTB,10)
    ITST=ISHIFT(ISTRG(NWJ),NBITS).AND.778
    IF(ITST.NE.558) RETURN
2  CONTINUE
  KTB=-1
  RETURN
END
SUBROUTINE FIND(TBUF,NW,COMP,N)
  DIMENSION TBUF(1)
  DO 1 I=N+1,NW
    IF(TBUF(I).EQ.COMP) RETURN
1  CONTINUE
  N=-1
  RETURN
END

```

## APPENDIX D

### RIGID BODY EXAMPLE



D-3

2148  
2149  
2150  
2151  
2152  
2153  
2154  
2155  
2156

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Variable	Value	Unit
1.00	1	
NSMAIN	2	
CTAB.1	1.0667, 1.0667, 3.	
CTAB.1	130.701, 130.701, 443.92, 443.92, 443.92, 443.92, 443.92	6
CTAB.1	4+3.32	13
INDUC.2	1	
CTAB.2	1.0667, 1.0667, 3.	
CTAB.2	130.701, 130.701, 4.23E+4, 4.23E+4, 4.23E+4, 4.23E+4	6
CTAB.2	4.23E+4, 4.23E+4	12
MUS	1.0667, 1.0667, 1.0667, 1.0667	
ES	1.0667, 1.0667, 1.0667, 1.0667	
SU	1.0667, 1.0667, 1.0667	
REM	BCD 4FLEXIBLE WIRFRAME DATA	
INDFLX	0	
REM	BCD 3AUTPILOT DATA	
REM	BCD 3A. ENGINE DATA	
INDAUT	1	
IN	2	
ZN	-1.0667, -1.0667	
YN	-1.0667, 1.0667	
N	1.0667	
REM	BCD 3B. DRAG CHUTE DATA	
ICS	0	
CUCH	1.0667	
SSH	1.0667	
XCH	-9.025	
YCH	1.0667	
ZCH	-1.0667	
REM	BCD 5C. PHASE BEGIN-TERMINATE	
ITO	0	
IF	1.0667	
NF	0	
XRF	0	
HRF	8.796	
JELTAM	3.	
NLKI	0	
T1	0	
KP	0	
VS	1.0667	
XS	3.0667	
TS	1.0667	
HS	0	
REM	BCD 4D. HOLD MANEUVER DATA	
ALPDES	1.0667	
TTO	0	
KE	INT 1.1	
PM	1.0667	
REM	BCD 5H. LANDING ROLL MANEUVER DATA	
TSP	0	
TRV	0	
TCH	7.	
IBK	0	
ISS	0	
ILK	0	
IUS	0	
REM	BCD 5I. ENGINE FAILURE STAGE DATA	
IC	INT 0.0	
XRF1	INT 0.0	
IT1	INT 0.0	
XRF2	INT 0.0	
IT2	INT 0.0	
H1	0	
IM1	INT 0.0	
1	0	

T 2	INT	0.0
5.1	INT	0.0
IHR1	INT	0.0
IR2	INT	0.0
IHR2	INT	0.0
TR1	INT	0.0
ITR1	INT	0.0
TR2	INT	0.0
ITR2	INT	0.0
REM	BCD	5J. BRAKE COND. STAGE DATA
IB	INT	0.0
IBK1	INT	1.0
IBK1	INT	0.0
IBK2	INT	1.0
IBK2	INT	0.0
REM	BCD	4K. PITCH AUTOPILOT DATA
IST	INT	0.0
ALPOL	INT	2.0
RFALPH	INT	0.0
DELALA	INT	0.0
PSH	INT	0.0
PSH2	INT	0.0
RFALP2	INT	0.0
DELQF	INT	8.0
DELJTO	INT	0.0
DELQI	INT	-1.0
DELQU	INT	+2.5
DELFD1	INT	5.25
REM	BCD	4L. YAW AUTOPILOT DATA
RFB	INT	0.0
DELJA	INT	0.5
PSRIA	INT	1.0
DPRIA	INT	0.5
RFPRI	INT	0.0
PSPRI	INT	0.0
DELRL	INT	-1.0
DELRLU	INT	+2.0
REM	BCD	4M. ROLL AUTOPILOT DATA
RPHI	INT	0.0
OPHIA	INT	0.5
PSA	INT	-1.0
DELPL	INT	-1.2
DELPU	INT	+1.2
REM	BCD	5N. THROTTLE AUTOPILOT DATA
TF	INT	0.0
NDF	INT	0.0
IR	INT	0.0
NR	INT	1.0
NLR	INT	0.0
NTU	INT	0.0
K2	INT	1.0
REM	BCD	4O. BRAKE AUTOPILOT DATA
MBC	INT	0.0
PD	INT	0.0
DELTAH	INT	0.0
OMEC01	INT	2.0
MBL	INT	0.0
MBU	INT	0.0
REM	BCD	5P. CONTROL RESPONSE DATA
DELAS	INT	5.25
DELRRD	INT	31.5
DELA	INT	1.0
NEU1	INT	1.0
REM	BCD	4Q. INITIALIZATION
J	INT	3

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L-LQD      * 4.56478
DELQDE     4.56478
DELQN      4.56478
DELPD      ..
DELRD      ..
MANLOG     1
PITCHP     1
REM        BCD 30ATA PLOT TAPE
IPLT       BCD 2STAGING DATA
REM        BCD 4A.GEARS INTO PROGRAM
INJLG      ..
ISTAGE     ..
DECR.S     BCD 1HR
STESTD     11..

TRA
INJLG      -1
REM        BCD 40.SMOOTH IMPACT STAGE
AINCRS     BCD 30DEL110DEL20DEL3
STEST      -.., -.15, -.55

TRA
PRINT      ..2
DELTS      ..55
AMAXER     ..55
PRIMIN     ..
AINCRS     BCD 11IMES
STEST      .9

TRA
ATAB51     7.35-6484E-3, 1.7-27972E-3
ATAB52     -5.2147852E-4, 1.-238928E-3
ATAB53     -3.1358631E-4, 1.8-65268E-3
ATAB56     ..55
ATAB57     ..55
REM        BCD 50. EFFICIENT AMAXER STAGE
AINCRS     BCD 40DELTA10DELTA20DELTA3
STEST      ..1, ..1

TRA
PRINT      ..5
AMAXER     ..1
DELTS      ..1
REM        BCD 40.SMOOTH IMPACT STAGE
AINCRS     BCD 100DEL1
STEST      -..5

TRA
PRINT      ..4
DELTS      ..55
AMAXER     ..55
REM        BCD 50. EFFICIENT AMAXER STAGE
AINCRS     BCD 10DELTA1
STEST      ..1

TRA
PRINT      ..5
AMAXER     ..1
DELTS      ..1
INDSTF     1

TRA

```

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 8

ZSDF

0.	0.	0.	0.	10.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	57.7454851E-01	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	0.	0.	-31.6515539E+00	12.4671000E+04	0.	10.3393988E+00

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0.

T(I)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0. 0. 15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

TTO

11.5000000E+00 0. 0.

FITCH AUTOPILOT

DELQN

ALPHA

ALPH01

ALP001

ALPHET

DELODE

26.8544760E-01-14.0024531E-07 0. 0. -14.0024531E-07 26.8544760E-01

INTEG RTN. HT = 1.0000000E-03

ZSDF

0.	0.	0.	0.	10.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	90.1422933E-02	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	0.	0.	-26.3312709E+00	12.4671000E+04	0.	10.3393988E+00

VPCS

38.7489900E+02

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
 GENERALIZED COMPUTER PROGRAM  
 INDSOF 2 CASE LROLL STAGE 1 PAGE 9

TFFS  
 0. 0.  
 0. 0.  
 T(I)  
 SAC1  
 29.7745819E-03-20.0749533E-03 60.9750569E-02 0. 0. 15.3281670E-03 0.  
 FLARE  
 AUTS  
 ALPDES PHIDES TTD  
 11.5000000E+00 0. 0.  
 PITCH AUTOPILOT  
 DELON ALPHAE ALPH01 ALPDD1 ALPHET DELODE  
 27.5617208E-01-14.0324531E-07 0. 0. -14.0024531E-07 27.5607208E-01  
 STAGE 04--DECR. HR

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 10

INDLG -1  
REM BCD 48 SMOOTH IMPACT STAGE  
AINCRS BCD 300 ELT10JELT20DELTA  
STEST TRA -0.5,-0.5,-0.5

2SDF

0. 0. 0. 0. 10.0001000E+0. 29.0276042E+01 0. 59.0569125E+00  
59.9992201E-01 11.4999986E+00 26.5337670E-02 29.6220760E+01 10.4252977E+01 29.6159990E+01 0.  
0. 0. 0. 0. -26.3302709E+00 12.4671000E+01 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+00 0. 0. 31.9713313E-01 38.9543765E+01 78.8552277E+01 0.  
0. 40.3200000E+00 0. 0. 54.9315281E-01 10.7799996E+01 49.6083699E+01 0.  
0. 40.3200000E+00 0. 0. 54.9315281E-01 10.7799996E+01 49.6083699E+01 0.

MUVP

VCPT

FTRX

FTRY

FTRZ

HA

HB

DOELTA

33.6000000E+00 29.6159990E+01 0. 0. -0. 0. 0. 78.8552277E+01  
33.6000000E+00 29.6159990E+01 0. 0. -0. 0. 0. 10.7799996E+01  
33.6000000E+00 29.6159990E+01 0. 0. -0. 0. 0. 49.6083699E+01

SD2

SD1

S

S2D2

S2D1

S2

OMETD1

OMET

0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXM

FYM

0. 0. 0. 0. 0. 0. 0. 0.

FZM

LM

NM

NM

0. 0. 0. 0. 0. 0. 0. 0.

VPCS

38.7409900E+02

TFFS

0. 0. 0. 0. 0. 0. 0. 0.

D-9

ORIGINAL PAGE IS  
OF POOR QUALITY

## INOSDF 2 CASE LROLL STAGE 1 PAGE 11

T(1)

**SAC1**

29.7745819E-03-20.8749533E-03 61.9750569E-02 0.

0.

15.3281670E-03 0.

FLARE

AUTS

ALPDES

## PHIDES

TTO

11.5333500E+03 G.

6.

### PITCH AUTOPILOT

DE LGN

ALPHAE

ALPHD1

ALP001

ALPHET

DELQDE

27.5333224E-01-14.0124531E-07 L.

Q.

-14.0024531E-07 27.5339224E-01

[illegible]



[illegible]



[illegible]

11.000000E-02	11.000000E-02	29.596673E+00	0.	93.7100927E-C1	28.9775565E+01	0.	59.6180378E+00
48.198445E-C4	0.	26.5003399E-02	29.5844872E+01	10.399476E+01	29.5772046E+01	0.	0.
65.6333767E-01	11.6257361E+00	12.9189599E-01	0.	-12.713308E-01	0.	13.3544858E+00	0.
0.	0.	99.5793199E-C2	0.	-27.2803123E+03	12.467100E+14	0.	0.

[illegible]

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

MUVP		VGPT	INC/SDF	2	CASE LROLL	STAGE 1	PAGE	15		
			FTRX		FTRY	FTRZ	MA		MB	DELTA
33.627000E+02	29.5776739E+01	L.	0.		-0.	0.		0.		-73.4934807E-01
33.627000E+02	29.5776739E+01	L.	0.		-0.	0.		0.		-46.1891723E-02
33.627000E+02	29.5776739E+01	L.	0.		-0.	0.		0.		-46.1891723E-02
SD2	SD1	S		S202	S201	S2		OMET01		OMET
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
FTRA	FTRB	FTRC	0.	MTX	MTY	MTZ	0.	FXM		FYM
0.	0.	0.	0.	0.	0.	0.	0.	0.		0.
FZM	LH	MH	0.	NH						
0.	0.	0.	0.							
VPCS										
38.7489900E+02										
TFFS										
0.	0.									
SAC1		J.			T(I)					
30.2764715E-03	23.1185661E-03	63.3346129E-02	0.		0.		90.5470527E-04	0.		
					FLARE					
AUTS										
ALPOES	PHIDES	TTO								
11.503300E+03	0.	L.								
DELON	ALPHA	ALPH01			PITCH AUTOPILOT					
29.1245546E-11	12.573666E-02	12.9189599E-01	0.		ALPH01	ALPHET	DELQDE			
					12.573666E-02	29.1245546E-11				

APPENDIX E

FLEXIBLE BODY EXAMPLE





136

6  
12

7  
7  
13  
19  
7  
13  
19

13  
25  
37  
7

E-4

REM	BCD	4G.	HOLD MANEUVER DATA
ALPOES		11.5	
TTD		11.1	
KE	INT	11.5	
PH			
REM	BCD	5H.	LANDING ROLL MANEUVER DATA
TSP		7.	
TRV		7.	
ICH		7.	
IBK		7.	
ISS		7.	
ILR		7.	
IBS		7.	
REM	BCD	5I.	ENGINE FAILURE STAGE DATA
IC	INT	0.0	
XRF1		2.0	
IT1	INT	2.0	
XRF2		2.0	
IT2	INT	2.0	
H1		2.0	
IH1	INT	2.0	
H2		2.0	
IH2	INT	2.0	
HR1		2.0	
IHR1	INT	2.0	
HR2		2.0	
IHR2	INT	2.0	
TR1		2.0	
ITR1	INT	2.0	
TR2		2.0	
ITR2	INT	2.0	
REM	BCD	5J.	BRAKE COND.STAGE DATA
IB	INT	0.0	
IBK1		1.0	
IBK1	INT	1.0	
IBK2		1.0	
IBK2	INT	1.0	
REM	BCD	4X.	PITCH AUTOPILOT DATA
TST		2.0	
ALPOL		2.0	
RFALPH		2.0	
DELALA		2.0	
PSH		2.0	
PSH2		2.0	
RFALP2		2.0	
DELQF		2.0	
DELQTO		2.0	
DELQOL		2.0	
DELQOU		2.0	
DELFD1		2.0	
REM	BCD	4L.	YAW AUTOPILOT DATA
REB		2.0	
DELDA		2.0	
PSR		2.0	
OPSIA		2.0	
RFPSI		2.0	
PSPSI		2.0	
DELRL		2.0	
DELRLU		2.0	
REM	BCD	4H.	ROLL AUTOPILOT DATA
RFPHI		2.0	
OPHIA		2.0	
PSA		2.0	
DELP		2.0	
DELP		2.0	

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```

REM      BCD 5N THROTTLE AUTOPILOT DATA
TF      INT 0.0
NOF      0.0
IR      INT 0.0
NB      0.0
NLR      0.0
NTO      0.0
K2      1.0
REM      BCD 40. BRAKE AUTOPILOT DATA
MBC      0.0
PD      0.0
DELTAW   0.0
OHECD1   2.0

MBL      0.0
MBU      0.0
REM      BCD 5P. CONTROL RESPONSE DATA
DELS     5.25
DELRPD   31.5
DELA     1.0
NEO1     1.0
REM      BCD 40. INITIALIZATION
IAP      3.0
HR      1.0
DELOD    4.55478
DELODE   4.55478
DELOD    4.55478
DELPD    0.0
DELPD    0.0
MANLOG   1.0
PITCHP   1.0
REM      BCD 2 STAGING DATA
REM      BCD 4A. GEARS INTO PROGRAM
INDLG     0.0
ISTAGE    0.0
DECRESE  BCD 1HR
STESTD    11.0
TRA      -1.0
INDLG     -1.0
REM      BCD 4B. SMOOTH IMPACT STAGE
AINCRS   BCD 30DELTA1DELTA2DELTA3
STEST    -0.5,-0.5,-0.5
TRA      -1.0
PRINT     0.0
DELS      0.0
AMAXR     0.0
PRIMIN    0.0
AINCRS   BCD 1TIMES
STEST     0.9
TRA      7.3516484E-3,1.727972E-3
ATAS51    -5.2147852E-4,1.238928E-3
ATAS52    -3.1368631E-4,1.869268E-5
ATAS53    0.0
ATAS54    0.0
ATAS55    0.0
REM      BCD 5C. EFFICIENT AMAXER STAGE
AINCRS   BCD 40DELTA1DELTA2DELTA3
STEST     1.0,1.0,1.0
TRA      0.5
PRINT     0.5
AMAXER    0.5
DELS      0.5
REM      BCD 40. SMOOTH IMPACT STAGE
AINCRS   BCD 10DELTA1
STEST     -0.5
TRA      -1.0

```

```

PRINT
DELTS      : 2
AMAXER     : 0.5
REM        : 0.05
BCD        : 0.05 EFFICIENT AMAXER STAGE
AINCRS     : 10 DELTA1
STEST      : 1
TRA        : 1

PRINT
AMAXER     : 0.5
DELTS      : 0.1
INDSTF     : 1
TRA        : 1

```

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 7

A. GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VPCS

8. XCGRF AREFF DIRFF D2RFF  
16.0500000E+02 17.7000000E+00 16.7000000E+00

PRINT CODES IDENTIFYING TIME HISTORY

250F	TIMES	XG77F	YG77F	HGC7F	U777F	V777F	W777F
TIME	Q177R	RI77R	AMACH	V177F	DYNPP	XG77F1	YG77F1
PI77R	ALPH0	BETAD	ALPH01	BE1AD1	GA47D	SIG7D	THTPD
ZG77F1	PH1FD	AX77F	AY77F	AZ77F	NTR7P	FOC	FCX
FSIPD	FCZ						
FCY							
VPCS							
AMASS							
TFFS							
MT	NT						
SAC1							
CAVAM	CA	CN	CY	CL	CM	CNN	

77  
1  
00

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 8

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	57.7454851E-01	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.			-31.6515539E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(I)

SAC1

29.7745819E-03-20.0749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

AUTS

FLARE

ALFDES

PHIDES

TTD

11.5000049E+00 0. 0.

PITCH AUTOPILOT

DELOH

ALPHA

ALFHD1

ALPDD1

ALPHET

DELODE

28.8544760E-01-14.0024531E-07 0.

0.

-14.0024531E-07 26.8544760E-01

INTEG RTN. MT = 1.00000000E-03

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	90.1422983E-02	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.			-26.3302709E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

E-10

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 9

TFFS

0.

0.

0.

0.

T(II)

SAC1

29.7745819E-03-20.8749533E-03 60.9750269E-02 0.

0.

15.3281678E-03 0.

AUTS

FLARE

ALPDES

PHIDES

TTD

11.5000000E+00 0.

0.

DELOW

ALPMAE

ALFMD1

PITCH AUTOPILOT

ALPDD1

ALPHET

DELODE

27.5607208E-01-14.8024531E-07 0.

0.

-14.8024531E-07 27.5607208E-01

STAGE ON--DECR. HR

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INCHOF 2 CASE LROLL STAGE 1 PAGE 10

INDLG -1  
REM BCD 49, SMOOTH IMPACT STAGE  
ATNCRS BCD 30DEL1100ELT20DEL13  
STEST TRA -.05, -.05, -.05

ZSOF

0. 0. 0. 0. 10.0000000E+00 29.0274847E+01 0. 59.0569126E+00  
59.9992281E-01 11.4999986E+00 0. 26.5337670E-02 29.6220760E+01 10.4252977E+01 29.6199990E+01 10.3393988E+00  
0. 0. 90.1422983E-02 0. -26.3102705E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

F:

SR

SF

AA

FC2

0. 35.2330000E+03 0. 0. 31.9713310E-01 -38.9549765E+02 -78.8562277E+01 0.  
0. 40.3200000E+03 0. 0. 54.9315280E-01 -10.7799396E+01 -34.6383699E+01 0.  
0. 40.3200000E+03 0. 0. 54.9315280E-01 -10.7799396E+01 -34.6383699E+01 0.

MUVP

VGPT

FTRX

FTRY

FTRZ

MA

MR

ODELTA

33.6000000E-02 29.6159990E+01 0. 0. -0. 0. 0. -79.8895154E-01  
33.6000000E-02 29.6154990E+01 0. 0. -0. 0. 0. -10.904626E-01  
33.6000000E-02 29.6159990E+01 0. 0. -0. 0. 0. -10.904626E-01

S02

S01

S

S202

S201

S2

OMETD1

OMET

0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXM

FYM

0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.

FZM

LM

MM

NM

0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.

VPCS

38.7489900E+02

TFFS

0. 0. 0. 0. 0. 0. 0. 0.

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E-11

INOSOF 2      CASE LROLL      STAGE 1      PAGE      11

T(1)

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

15.3281670E-03 0.

POINT  
XDIT

X02F  
Y01F

X02T  
Y01T

Y02F  
Z01F

VOZT  
ZOLT

ZD2F  
XDDF

2021  
Y00F

KDIF  
ZODF

10.0300000E-01	0.
29.0274042E+01	0.
20.0000000E-01	0.
29.0274042E+01	0.
30.0000000E-01	0.
29.0274042E+01	0.
40.0000000E-01	0.
29.0274042E+01	0.

91.2652002E-02	0.
0.	0.
10.2398015E-01	0.
0.	0.
92.5024062E-02	0.
0.	0.
91.5277229E-02	0.
0.	0.

0.	0.
59.0569126E+00	0.
0.	0.
59.0569126E+00	0.
0.	0.
59.0569126E+00	0.
0.	0.
59.0569126E+00	0.

-28.9135646E+00	0.	18.5462913E-02
-28.4544208E+00	0.	18.7604868E-02
-28.1584011E+00	0.	-11.9775242E-02
-24.3726223E+00	0.	22.8822210E-02

## AUTS

FLARE

ALPOES

## PHIDES

110

11.50000000E+00 0.

9.

### PITCH AUTOPILOT

DE LON

ALPHA

AL FND1

ALPDS1

ALPNET

DEL COE

27.5339, 14E-01-14.0024531E-07 0.

9.

-14.0024531E-07 27.5339224E-01

[illegible]



INOSDF 2 CASE LROLL STAGE 1 PAGE 12

[illegible]

250F

50.0000000E-03	50.0000000E-03	14.8031850E+00	0.	96.9255346E-01	29.0027333E+01	0.	59.3321982E+00
0.	27.2691345E-04	0.	26.5179136E-02	29.6034039E+01	10.4122524E+01	29.5957121E+01	0.
62.9408593E-01	11.5617249E+00	0.	12.6599115E-01	0.	-12.1627675E-01	0.	10.3434516E+00
0.	0.	94.7837143E-02	0.	-26.7864184E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

0.

6.

MUY P

P

35.20000000E+03

40.32000000E+03  
40.32000000E+03

VGPI

92

ETRY

57

**STUDY**

50

5101

22

459

5583

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LRUL STAGE 1 PAGE 13

33.38888888E-02 29.5973017E+01 0. 0. -0. 0. 0. -25.578419E-03  
33.60000000E-02 29.5965279E+01 0. 0. -0. 0. 0. -30.100733E-03  
33.60000000E-02 29.5965279E+01 0. 0. -0. 0. 0. -30.100733E-03

S02 S01 S S202 S201 S2 OMETD1 OMET  
0. 0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0. 0.  
FTRA FTRB FTRC MTX MTY MTZ FXM FYM  
0. 0. 0. 0. 0. 0. 0. 0.  
FZM LM MM NM  
26.4566471E+00 0. 17.8487823E+01 0.

VPCS  
38.7489900E+02  
TFFS  
0. 0.

0. 0.

SAC1  
38.8142517E-03-21.9773025E-03 62.1249652E-02 0. 0. 12.2575620E-03 0.  
FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
18.0000000E-01 0.	95.6591171E-02 0.	13.1314487E-03 0.	59.2289816E+00 0.	51.4324685E-02-28.3488744E+00 0.	18.5681969E-02 0.		
29.0027819E+51 0.	10.4579527E-01 0.	16.3322030E-03 0.	59.2528812E+00 0.	55.1828791E-02-27.5350303E+00 0.	18.7952610E-02 0.		
29.0000000E-01 0.	96.6655688E-02 0.	-15.2076542E-03 0.	59.3247313E+00 0.	-53.6546557E-02-27.1853834E+00 0.	-12.8042899E-02 0.		
29.0032434E+01 0.	95.9324761E-02 0.	24.8658597E-03 0.	59.4452341E+00 0.	87.3915752E-02-24.3453439E+00 0.	22.9254624E-02 0.		
30.0000000E-01 0.							
29.0024375E+01 0.							
40.0000000E-01 0.							
29.0027938E+01 0.							

AUTS

PLANE

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INDSO# 2      CASE LROLL      STAGE 1      PAGE 14

ALPDES	PHIDES	TTO
11.5000000E+00	0.	0.

### PITCH AUTOPILOT

DELON	ALPHA E	ALPHO1	ALPCO1	ALPHET	DELODE
28.2700935E-01	61.7294630E-03	12.6599115E-01	0.	51.7294630E-03	28.2700935E-01

[illegible]

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 15

INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03
INTEG	RTN.	HT	=	1.600000000	-03

250F

10.0000000E-02	10.0000000E-02	29.966769E+00	0.	93.7098797E-01	28.9775545E+01	0.	39.6186786E+00
0.	43.2450607E-04	0.	25.5008497E-02	28.5844982E+01	10.9906531E+01	0.	0.
65.646534E-01	11.6258534E+00	0.	12.9349867E-01	0.	-12.7143277E-01	20.5772144E+01	10.3544256E+00
0.	0.	99.5833827E-02	0.	-27.2744387E+00	12.6718000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
-------	---	----	----	----	----	----	-----

0.	35.2800000E+03	0.	0.	34.9155442E-01	38.9549765E+02	78.8562277E+01	0.
0.	40.3200000E+03	0.	0.	39.9547989E-01	10.7799996E+03	39.6383699E+01	0.
0.	40.3200000E+03	0.	0.	39.9547989E-01	10.7799996E+03	39.6383699E+01	0.

MUVP	VGPT	FTRX	FTRY	FTRZ	MA	MB	DOELTA
------	------	------	------	------	----	----	--------

33.6000000E-01	29.5784944E+01	0.	0.	-0.	0.	0.	-72.4166619E-01
33.6000000E-01	29.5501112E+01	0.	0.	-0.	0.	0.	-5.0510413E-01
33.6000000E-01	29.5501112E+01	0.	0.	-0.	0.	0.	-5.0510413E-01

S02	S01	S	S202	S201	S2	OMET01	OMET
-----	-----	---	------	------	----	--------	------

0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXH	FYM
------	------	------	-----	-----	-----	-----	-----

0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

FZM	LM	NM	NM
-----	----	----	----

24.3554817E+00	0.	13.85E7145E+01	0.
----------------	----	----------------	----

VPCS

38.7489900E+02

TFFS

E-16

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INOSOF 2 CASE LROLL STAGE 1 PAGE 16

0. 0.

**0**

Y (I) 2

**SAC1**

38.2764807E-03-23.1194946E-03 63.3356138E-02 0.

9.

90.5418689E-04 0.

**FLEX**

[illegible]

FLAME

AUTS

ALPDES

PHIOES

110

11.50000000E+00 0.

9.

### PITCH AUTOPILOT

DE LON

ALPHA E

ALFMD1

ALP 001

ALPHET

DELCOE

29.0985706E-01 12.5858422E-02 12.9349867E-01 0.

12.5658422E-02 29.0985706E-01

[illegible]

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSCF 2

CASE LROLL

## STAGE 1

PAGE

17

[illegible]

250F

15.0000000E-02	15.0000000E-02	44.3003500E+00	0.	29.3552141E-01	28.9570435E+01	0.	59.9059780E+00
0.	62.9675929E-04	0.	26.4828395E-02	24.5653189E+01	10.3657782E+01	29.5574749E+01	0.
64.1000511E-01	11.6903561E+00	0.	12.8113987E-01	0.	-13.1985314E-01	0.	10.3705021E+00
0.	0.	10.4422113E-01	0.	-27.7778787E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

P

P2

51

59

55

22

FC2

11.

35.28000000E+03	0.
40.32000000E+03	0.

9.

31.4902661E-01-38.9549765E+02-78.8562277E+01 0:  
37.5811505E-01-10.7749996E+03-34.6383699E+01 0:

C-3

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY  
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 10

0. 40.3280000E+03 0. 0. 37.5811505E-01-10.7799995E+03-39.6383699E+01 0.

MUVP VGPT FTRX FTRY FTRZ HA HB ODELTA

33.0000000E-02 29.5590914E+01 0. 0. -0. 0. 0. -69.1497722E-01

33.0000000E-02 29.5612156E+01 0. 0. -0. 0. 0. -24.8322627E-02

33.0000000E-02 29.5612166E+01 0. 0. -0. 0. 0. -24.8322627E-02

SD2 SD1 S S202 S201 S2 OMETO1 OMET

0. 0. 0. 0. 0. 0. 0. 0.

0. 0. 0. 0. 0. 0. 0. 0.

FTRA FTRB FTRC HTX HTY MTZ FXH FYH

0. 0. 0. 0. 0. 0. 0. 0.

FZH LM MM NM

92.4689028E-01 0. 40.7864789E+00 0.

VPCS

38.7429900E+02

TFFS

0. 0.

0. 0.

T(II)

SAC1

38.5566271E-03-24.2740905E-03 64.5784391E-02 0. 0. 57.0052216E-04 0.

FLEX

POINT X02F X02T Y02F Y02T Z02F Z02T X01F

X01T Y01F Y01F Z01F Z01T Z01F Y01F Z01F

10.4805005E-01 0. 93.9243789E-03 50.7316675E+00 86.1109423E-02-27.8883618E+00 0. 0. 0. 0. 0. 0. 0. 0.

10.8958562E-01 0. 52.2496503E-03 50.7377182E+00 77.4745869E-03-28.4993856E+00 10.0731982E-02

10.5236131E-01 0. 50.5538950E-03 50.3642718E+00 -17.7023431E-02-27.6902810E+00 11.1680385E-02

10.5231357E-01 0. 11.3863919E-02 60.2231144E+00 74.2456941E-02-26.2991382E+00 -12.415096E-02

0. 0. 0. 0. 0. 0. 23.6383140E-02

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END  
DATE

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